Monthly Webinar Series



WOODWORKS

Kendeda Building for Innovataive Sustainable Design, The Miller Hull Partnership with Lord Aeck Sargent, photo Jonathan Hillyer



1430 Q, The HR Group Architects, Buehler Engineering, Greg Folkins Photography

T3 Minneapolis, MGA, DLR Group, Magnusson Klemencic Associates, StructureCraft, photo Ema Poter

RESOURCES & UPCOMING EVENTS

New WOOD SOLUTION PAPER

Taking the Guesswork out of Mixed-Use Building Requirements



where are present whet remain in the property of allow a couple to organ, and provider, fair proposal of we in some that where no of same support and the tracting and the court passes strategy to presented the local sector in the sector in the sector with the sector of the sect the rest is here there are seen buying one a name in case in a second part of the or of specific processors. Note an implicate had Canada Institute Statistications in Space of and the contradito exchange tales and appropriderivation and the interaction of the local lines. statistic southline with from one printers when submitting being on any record to any records

of settinguitaria advangtures surt regroups names in Planet areas, "read on" the subscription of the last of the local of a second of a state of these that are interedial and distants a loss that the base of the loss of the loss of the

and plant much share below straight and an entry lines a interest in site interest of in the board will part of the loss being and because have second partners at the statent, and a high rise during and conception, or where beauty out And Address of the Ad

Para and Life Exhibit -Building Stee, Chicapetery mini Comptraction Types

the summaries building their WO I - Galler Ini Tea printpert surging to be on the story. Inguiters. But including the Agenty the states of the start is not start to start the start to start the start to start the start to s

the state of the property of particular distribution of the state of the particular distribution of the state science, benand reard environme, where we is not

Applications for targets parts at the BD. Management of the subscription in Frank (in Frank) Castly of Dispace, and its parameters and project of approaching write approach to a single size where he party from a lot of the second In which cards of the division of the state science. The computation of these functions, and its special arraying of the last strike to requerry service to excitence to survive to had the Reserve balance of the second states strand to the stated comparing with the registering and the barbarra Par propriety in turnel by Par in york to first is more which is of carrier clarge particular of which we cannot weating many practic process of the finance plant of manual ships beinging

Providence and project and another Including a present and many property in careful second Internet desires the factors of time in respect the first



January 12 | ONLINE – 1 Hour The World's Tallest Mass Timber Tower: A Behind the Scenes Look at Ascent



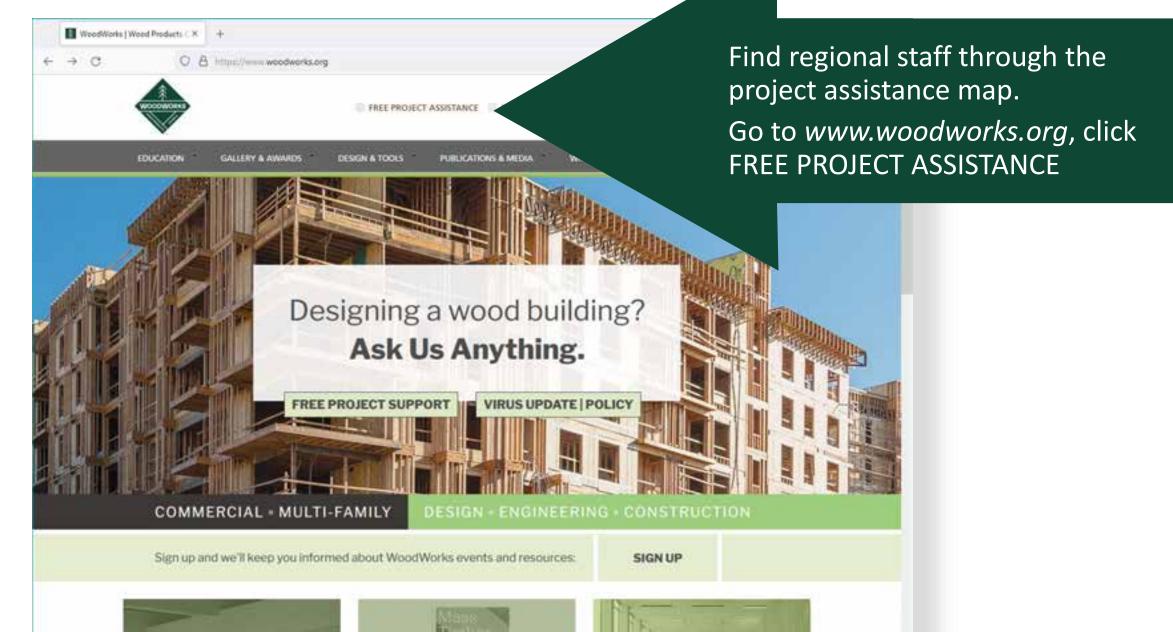
New for GCs and installers: U.S. Mass Timber Construction Manual





Download free at woodworks.org

WoodWorks: Project Assistance Map



Design Professionals: **One-on-One Support & Assistance**

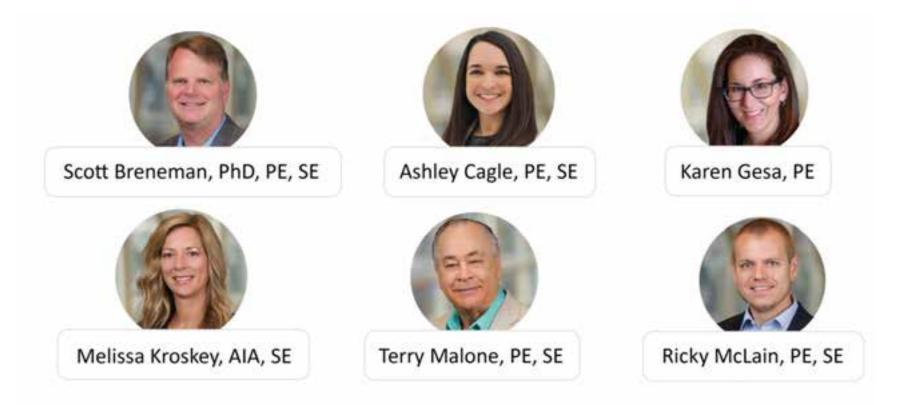


PROJECT SUPPORT FIELD DIVISION



Meet the Help Desk

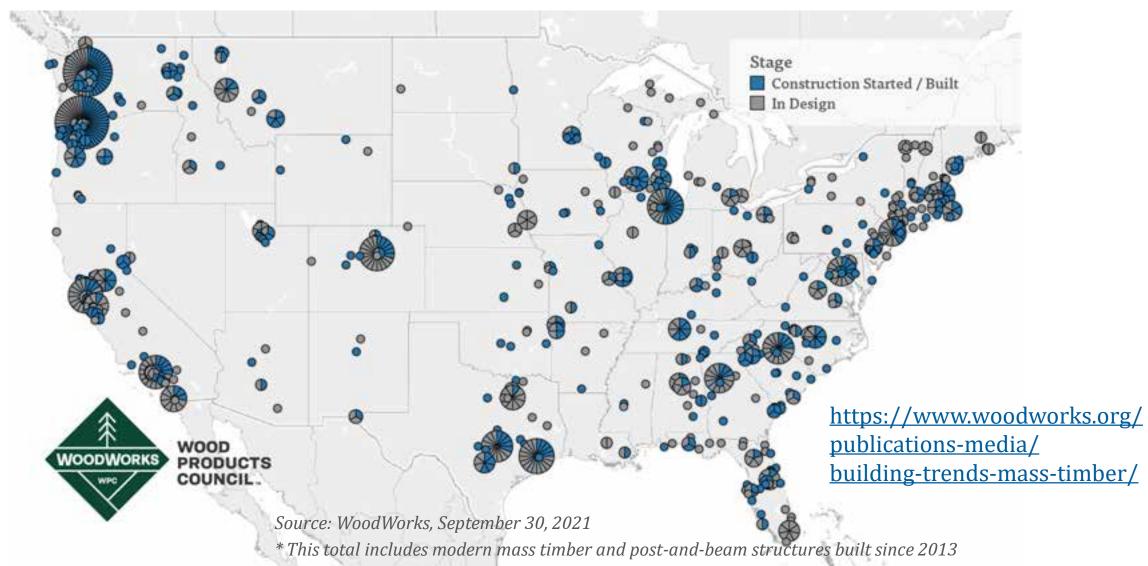




Need technical assistance on a project? Email: help@woodworks.org

Current State of Mass Timber Projects

As of September 2021, in the US, **1,241** multi-family, commercial, or institutional projects have been constructed with, or are in design with, mass timber.





Continuing Education Credits

- Participants will receive a certificate of completion via email
- AIA credits will be processed by WoodWorks

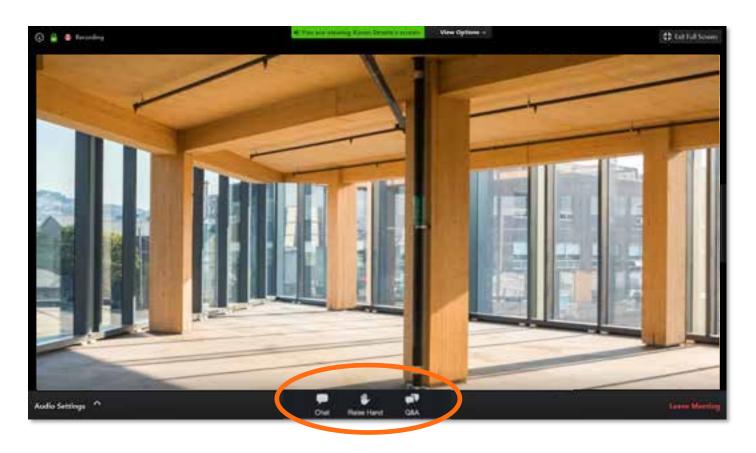
Go to woodworks.org/webinar

- 1. To download the group sign in form
- 2. To download the presentation pdf

Ask Questions through the Q&A Box



Submit questions in the Q&A box at the bottom of your screen as they come up in the presentations. We will get to as many questions as possible.



Interior Wall and Floor Assemblies in Mid-Rise Multi-Family: Designing for Fire, Acoustics & Structure

Presented by Karen Gesa, Ricky McLain & Ashley Cagle



"The Wood Products Council" is a Registered Provider with The American Institute of Architects Continuing Education Systems (AIA/CES), Provider #G516.

Credit(s) earned on completion of this course will be reported to AIA CES for AIA members. Certificates of Completion for both AIA members and non-AIA members are available upon request. This course is registered with AIA CES for continuing professional education. As such, it does not include content that may be deemed or construed to be an approval or endorsement by the AIA of any material of construction or any method or manner of handling, using, distributing, or dealing in any material or product.



Questions related to specific materials, methods, and services will be addressed at the conclusion of this presentation.

Course Description

What are the pros and cons of using a single stud wall vs. a staggered stud wall for dwelling unit separation? Do you need sprinklers or fireblocking in the floor cavity of your wood joist floor assembly? How can you meet code requirements for fire-resistance continuity of corridor walls while also having numerous mechanical elements puncturing those walls? If you have questions like this, you won't want to miss this webinar focused on practical solutions for commonly asked multi-family design questions. Join us for this third session in our 2021 series of deep dives into this topic as we take a step-by-step approach to the design and selection of interior walls (unit demising, corridor, shafts and firewalls) and floor/ceiling assemblies and discuss how the fire-resistance, acoustical performance and structural load resolution of these assemblies can be simultaneously achieved. We'll analyze example details and assemblies, contrast different assembly options, learn how to make modifications to tested wall assemblies, answer questions that arose during the first two sessions in this series, and look at tools you can use to evaluate your options.

3-Part Series on Light-Frame Interior Detailing

July 2021 Workshop Fire, Acoustics, and Structural Detailing of Light-Frame Interior Walls <u>https://www.woodinstitute.org/enrol/index.php?id=207</u>

November 2021 Symposium Fire, Acoustics, and Structural Detailing of Light-Frame Horizontal Assemblies <u>https://www.woodinstitute.org/enrol/index.php?id=212</u>

<u>December 8 Webinar</u> Wrap up on interior floor and wall assemblies Answering follow-up questions, commonly asked questions <u>https://www.woodinstitute.org/enrol/index.php?id=218</u>

February 2022 Symposium Exterior walls: Assemblies, Fire Resistance Ratings, Claddings and Details <u>https://www.woodinstitute.org/course/view.php?id=228</u>

Today's Agenda: Light-Frame Interior Detailing

Fire-resistance and acoustics of interior walls | Impacts of:

- Stud size and spacing
- Addition of sheathing layers
- Addition of insulation

Shaftliner Panel Systems

- Assembly options
- Detailing at floor supports
- Mass timber floor to shaft wall interface

Firewalls

- Floor sheathing continuity
- Seismic joints
- Material allowances

How do I determine fire rating and STC?

What if I need to alter the tested wall assembly?

703.3 Methods for determining fire resistance. The application of any of the methods listed in this section shall be based on the fire exposure and acceptance criteria specified in ASTM E119 or UL 263. The required *fire resistance* of a building element, component or assembly shall be permitted to be established by any of the following methods or procedures:

- 1. *Fire-resistance* designs documented in approved sources.
- 2. Prescriptive designs of fire-resistance-rated building elements, components or assemblies as prescribed in Section 721.
- 3. Calculations in accordance with Section 722.
- 4. Engineering analysis based on a comparison of building element, component or assemblies designs having *fire-resistance ratings* as determined by the test procedures set forth in ASTM E119 or UL 263.
- 5. Alternative protection methods as allowed by Section 104.11.
- 6. *Fire-resistance* designs certified by an approved agency.

Common methods for determining fire rating

- 1. Tested assemblies published by:
 - a. Underwriters Laboratories (UL)
 - b. Gypsum Association (GA)
 - c. US Gypsum Corporation (USG)
 - d. National Gypsum
 - e. American Wood Council (AWC) DCA-3
 - f. Proprietary sheathing/insulation manuf
- 2. IBC prescriptive assemblies per section 721
- 3. IBC calculated method per section 722
 - a. Component Additive Method (CAM)

UL-rated wall assemblies

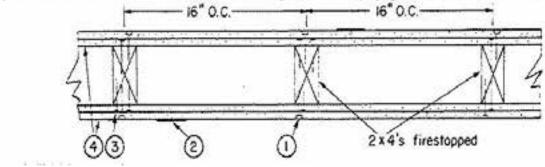
Design No. U301 May 28, 2021

Bearing Wall Rating - 2 Hr.

Finish Rating - 66 Min.

This design was evaluated using a load design method other than the Limit States Design Method (e.g., Working Stress Design Method). For jurisdictions employing the Limit States Design Method, such as Canada, a load restriction factor shall be used — See Guide BXUV7 or BXUV7

* Indicates such products shall bear the UL or cUL Certification Mark for jurisdictions employing the UL or cUL Certification (such as Canada), respectively.



https://iq.ulprospector.com/en/ ?tt=1002

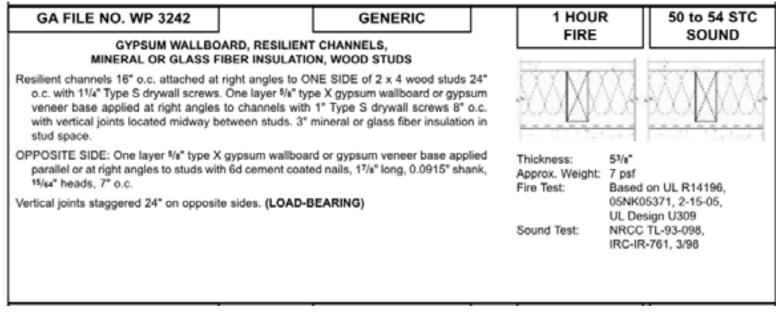
Challenge:

- Not typically an STC listed
- Fixed stud size/spacing

GA-600 wall assemblies

Territory Pro-	\sim
FIRE	GYPSUM ASSOCIAT
RESISTANCE	
DESIGN	
MANUAL	
SOUND CONTROL	

GYPSUM SYSTEMS



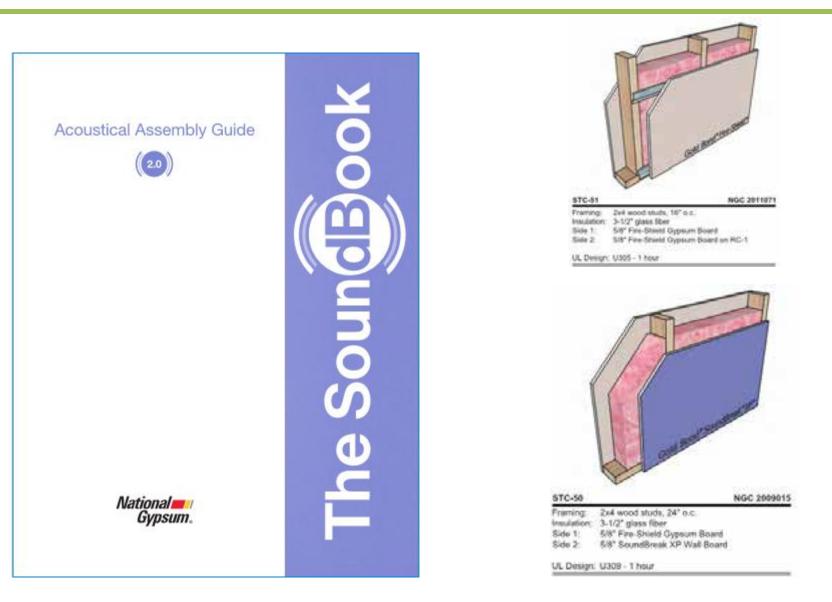
Has several wall assemblies with stud spacing at 24"

USG wall assemblies



1 Hour Fire-Rated Construction	Dimensional Lumber	Acou	Reference				
Construction Detail	Description Test Numbe		er STC IIC		Test Number	Index	
dg. wt. 3	5/8" Svernox Frecox Core gypsum panels, celling - 1" nominal wood sub and finished floor - 2 x 10 wood joist 16" o.c.	UL Des L501	38	32	CK-6412-7 Based on 1-1/4" nominal wood floor	8-52	
Χ	 joints finished optional Leveuxox floor underlayment optional SRM-25 or SRB sound mat optional veneer plaster 		39	56	CK-6412-8 Based on 1-1/4" nominal wood foor, 44 oz carpet and 40 oz pad atop flooring		

National Gypsum Wall assemblies

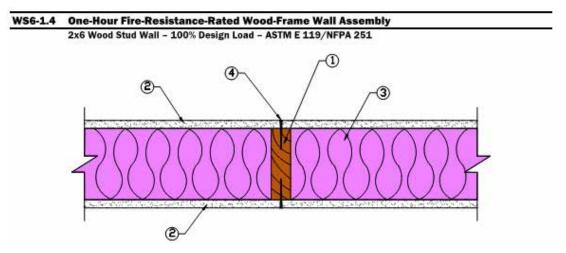


AWC wall assemblies

American Wood Council publication DCA-3 that has 1- and 2-hour rated assemblies, many with STC and IIC information:



Fire-Resistance-Rated Wood-Frame Wall and Floor/Ceiling Assemblies



Proprietary wall sheathing or insulation

REFERENCE.	FIRE RATING	TEST NO.	STC	OC ASSEMBLY NO.	CONSTRUCTION DESCRIPTION
NBC-W5c (16° o.c.) NBC-W5c (16° o.c.) NBC-W5d (24° o.c.) NBC-W5d (24° o.c.)	45 min, L.B. 1 h, N.L.B. 45 min, L.B. 1 h, N.L.B.	NBC-W5c (16° o.c.) NBC-W5d (24° o.c.) *W0669 (16° o.c.)	49 53 52	UWSR037	Single 38 mm x 89 mm (1-1/2" x 3-1/2") wood studs spaced 400 mm (16") or 600 mm (24") o.c.; resilient channels spaced 400 mm (16") or 600 mm (24") o.c.; single layer 12.7 mm (1/2") type "x" gypsum board one side; double layer other side, one thickness, 89 mm (3-1/2") thick EcoTouch® QuietZone® PINK® FIBERGLAS® Acoustic Batt Insulation.

1 Hour Design #		(entropy)	GA File #	STC - 35		
FIRE	UL U	305	05 WP 3605		NGC - 2403	
	D.PDF file	Board app 16" o.c. wi 7" o.c. at e	mm) Fire-Shield Gypsu lied horizontally or ve ith 6d coated nails, 1-7 edges. Joints of squar bard may be left expos	ertically to each si 7/8" long, 0.0915 e edge, bevel edg	de of 2x4 wood studs " shank, 1/4" heads, ge or predecorated	

Prescriptive through IBC

IBC Section 721 has pages of prescriptive assemblies based on testing using ASTM E 119 or UL 263:

MATERIAL	ITEM NUMBER	CONSTRUCTION			MINIMUM FINISHED THICKNESS FACE-TO- FACE ^b (inches)				
	NOMBER		4 hours	3 hours	2 hours	1 hour			
	14-1.1 ^{h. m}	2" × 4" wood studs 16" on center with two layers of $\frac{3}{8}$ " regular gypsum wallboard ^e each side, 4d cooler ⁿ or wallboard ⁿ nails at 8" on center first layer, 5d cooler ⁿ or wallboard ⁿ nails at 8" on center second layer with laminating compound between layers, joints staggered. First layer applied full length vertically, second layer applied horizontally or vertically.	Ι	_	_	5			
	14-1.2 ^{l, m}	2" × 4" wood studs 16" on center with two layers $\frac{1}{2}$ " regular gypsum wallboard ^e applied vertically or horizontally each side ^k , joints staggered. Nail base layer with 5d cooler ⁿ or wallboard ⁿ nails at 8" on center face layer with 8d cooler ⁿ or wallboard ⁿ nails at 8" on center.	_		_	51/2			
14. Wood studs-interior par-	14-1.3 ^{l, m}	2" × 4" wood studs 24" on center with $\frac{5}{8}$ " Type X gypsum wallboard ^e applied vertically or horizontally nailed with 6d cooler ⁿ or wallboard ⁿ nails at 7" on center with end joints on nailing members. Stagger joints each side.	_			4 ³ / ₄			
tition with gyp- sum wallboard each side	14-1.4 ¹	2" × 4" fire-retardant-treated wood studs spaced 24" on center with one layer of $\frac{5}{8}$ " Type X gypsum wallboard ^e applied with face paper grain (long dimension) parallel to studs. Wallboard attached with 6d cooler ⁿ or wallboard ⁿ nails at 7" on center.	—	—	_	4 ³ / ₄ ^d			
1		2" x 4" wood stude 16" on contar with two lowers 5/ " Type V gyngym wellbaarde							

TABLE 721.1(2)—continued RATED FIRE-RESISTANCE PERIODS FOR VARIOUS WALLS AND PARTITIONS ^{a, o, p}

Calculated method through IBC 722/DCA 4

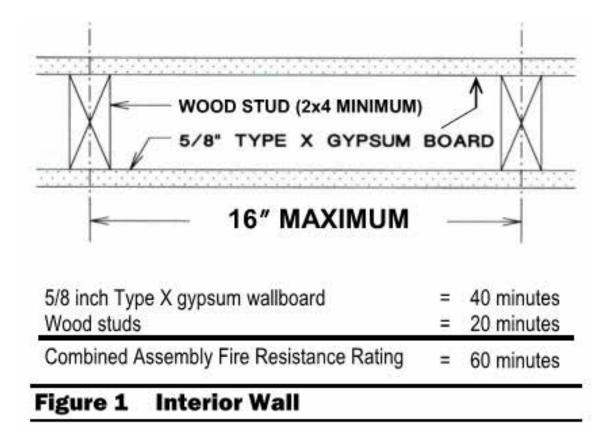
TABLE 722.6.2(1) TIME ASSIGNED TO WALLBOARD MEMBRANES^{a, b, c, d}

DESCRIPTION OF FINISH	TIME ^e (minutes)
³ / ₈ -inch wood structural panel bonded with exterior glue	5
¹⁵ / ₃₂ -inch wood structural panel bonded with exterior glue	10
¹⁹ / ₃₂ -inch wood structural panel bonded with exterior glue	15
³ / ₈ -inch gypsum wallboard	10
¹ / inch gynsum wallhoard	15



Component Additive Method (CAM) for Calculating and Demonstrating Assembly Fire Resistance

Calculated method through IBC 722/DCA 4



Calculated method through IBC 722/NDS Ch 16

Exposed Framing Fire Resistance

Table 16.2.1A	Char Depth and Effective Cha			
	Depth (for β_n = 1.5 in./hr.)			

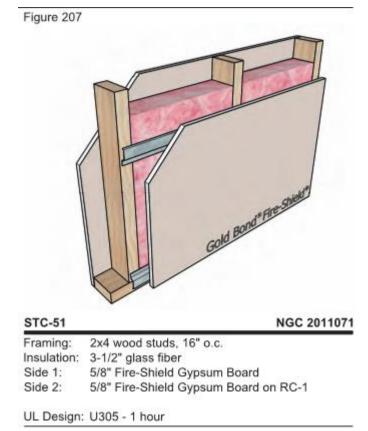
Required Fire Resistance (hr.)	Char Depth, a _{char} (in.)	Effective Char Depth, a _{eff} (in.)
1-Hour	1.5	1.8
1 ¹ / ₂ -Hour	2.1	2.5
2-Hour	2.6	3.2



Cold wood Heated zone Char layer Heated zone B Heated zone Char layer Heated zone Char layer Char layer



Let's say we need a 1-hour corridor wall with STC >=50 and choose this assembly:



Then the engineer needs to increase the stud size or decrease the spacing. Or perhaps he/she needs a layer of wood sheathing for shear resistance.

Typically having more or larger studs shouldn't affect the fire-rating chosen.

There are a couple of references that confirm this: Notes 15 & 16 of the Gypsum Association Fire Resistance Design Manual state that studs can be larger than noted in the assembly and that stud spacings noted are max:

- 15. Greater stud sizes (depths) shall be permitted to be used in metal- or wood-stud systems. Metal studs of heavier gage than those tested shall be permitted. The assigned rating of any load-bearing system shall also apply to the same system when used as a nonload-bearing system. Indicated stud spacings are maximums.
- 16. Specified floor-ceiling and roof-ceiling framing sizes or truss dimensions are minimums. Greater joist or truss sizes (depths) shall be permitted to be used in metal- or wood-framed systems. Indicated joist and truss spacings are maximums.

Section VI of the <u>UL Fire Design Information</u> essentially notes the same:

If your stud/joist size is <u>smaller</u> or spacing is <u>larger</u> than the tested assembly, you'll generally need to show conformance to fire resistance with another method.



What options exist for 1-hour rated floor and roof assemblies where floor joists less than 2×10 in depth are desired?

In many building applications, including multi-family housing and offices, it is common for designers to go to great lengths to minimize Boor depth in order to maximize plate height, specifically in considers (although this could be relevant at any floor location). As corridors are commonly less than 10 feet wide, solid sawn floor joints can be used in lies; of parallel chood trumen or Ejoints used at the longer span adjacent bays. However, most fire-tested floor and roof assembles utilizing solid sawn structural members require a minimum 2x10 depth. And yet, a depth of less than 2x10 can often be accomplehed structurally while providing cost advantages and allowing more room for MEP items.

For designers seeking shallower floor and roof depths, the following



options exist IIIC Section 703 permits multiple ways of determining fire-resistance.

ratings. One method is to use calculations in accordance with IBC Section 722. IBC section 722.6 could be used to calculate up to a 1-hour rating for a wood-frame wall, floor or roof assembly. IBC Table 722.6.3(2) allows 10 minutes for wood floor or roof joints at 16" o.c. (so minimum joint size is given except that it needs to be adaption for structural leads) BY Table 711.6 W1 allows 35 minutes for a laser of 117 measure term Y. Adding these treather an

https://www.woodworks.org/experttip/what-options-exist-for-1-hour-rated-floorand-roof-assemblies-where-floor-joists-less-than-2x10-in-depth-are-desired/

Acoustically, more studs or larger studs can reduce the STC.

Fewer studs increases the STC.



Home - All Expert Tips

What is the impact of wood stud size and spacing on the fire-resistance and acoustical performance of a wall assembly? Can stud sizes and spacing be altered from those in tested wall systems?

Interior wall partitions in a wood-frame building—such as unit demising and corridor walls in a multi-family project—must meet several design objectives simultaneously. Two primary functions are fire resistance and acoustical separation. Having to cite two tested wall assemblies, one for fire-resistance endurance results and another for acoustic results, is common. However, matching components between the two tested systems can be challenging, and the architect may want to slightly alter the wall stud size and/or spacing of one of the systems to meet specific project needs.

For example, a corridor wall that requires a 1-hour fire resistance rating and STC 50 acoustical rating will be constructed of 2x6 studs at 16" o.c. with resilient channels on one side, and one layer of 58" gypsum wallboard on each side. Is it permissible to demonstrate the fire-resistance rating (FI0) of this wall assembly with a tested assembly that included 2x4 studs instead of 2x6 studs? If the acoustical test being cited also included 2x4 studs, what is the acoustical impact of constructing the wall with 2x6 studs?

Similarly, a unit demising wall will be constructed of a staggered stud wall system, each row having 2x4 studs at 24° o.c. alternating on each side of 2x6 top and bottom plates. However, to meet structural demands, each row must have 2x4 studs at 16° o.c.. What impact does this reduction in stud spacing have on the fire resistance and acoustical performance of the wall?

It is generally accepted that stud adves can be increased beyond those in a wall fire test, and stud spacings can be decreased relative to those in a wall fire test, without reducing the fire-resistance endurance of the wall assembly.

Item 16 of the Gypsum Association Fire Resistance Design Manual notes.

Greater stud sizes (depths) shall be permitted to be used in metal- or wood-stud systems. Metal studs of heavier gauge than those tested shall be permitted. The assigned rating of any load bearing system shall also apply to the same system when used as a nonload bearing system. Indicated stud spacings are maximums.

Similarly Section VI of the UILFine Design Information notes:

So here is the challenge:

More studs or larger studs – fire rating ok, acoustics may not be

Fewer studs or smaller studs – acoustics ok, fire rating may not be

Possible solutions:

- 1. Choose assembly for acoustics first, then calculate the fire-rating if needed
- Alternate Method of determining STC/IIC: IBC 1206.2 & 1206.3 Both STC and IIC may be "established by engineering analysis based on a comparison of floor-ceiling assemblies having [STC/IIC] ratings as determined by the test procedures."

What if you need to add a layer of wood sheathing?

What if you add a layer of wood sheathing?

Adding sheathing will not negatively affect the fire rating of a wall.

Home > All Expert Tips

Adding Wood Structural Panels to a Fire-Tested Wall Assembly

Q: Can I add wood structural panels to a fire-tested wall assembly that doesn't already include them? I need the exterior walls on a project to be shear walls but the UL assembly I'm specifying doesn't show sheathing panels.

A: Yes, wood structural panels can be added to a fire resistance-rated wall assembly that was tested without them. Several references permit this, as outlined below:

The Underwriter Labs' General Information for Fire-resistance Ratings – ANSI/UL 263, Section VI item 6, allows the addition of wood structural panels in fire-rated gypsum board wall assemblies and provides relevant construction details.

The Gypsum Association's Fire Resistance Design Manual permits this per Item 23 in Section 1 of the General Explanatory Notes. This is shown in the following text:

"When not specified as a component of a fire resistance-rated wall or partition system, wood structural panels shall be permitted to be added to one or both sides. Such panels shall be permitted to be applied either as a base layer directly to the framing (under the gypsum board), as a face layer (over the face layer of gypsum board), or between layers of gypsum board in multi-layer systems. When such panels are applied under the gypsum board or between layers of gypsum board the length of the fasteners specified for the attachment of the gypsum board applied over the wood structural panels shall be increased by not less than the thickness of the wood structural panels. Fastener spacing for the gypsum board and the number of layers of gypsum board shall be as specified in the system description."

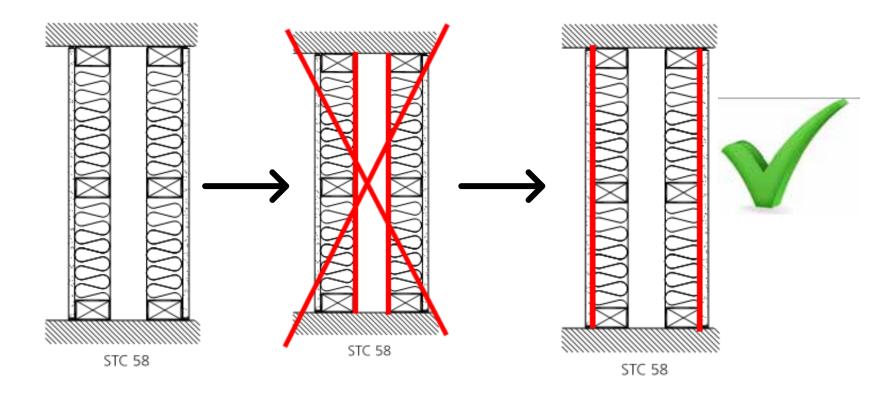
Additionally, ESR 2586, Performance Standards and Qualification Policy for Structural-Use Panels, and Performance Standard for 202 Siding, states the following in certical 4.7 Eine Periotike Constantion:

https://www.woodworks.org/experttip/adding-wood-structuralpanels-to-a-fire-tested-wall-assembly/

What if you add a layer of wood sheathing?

Adding sheathing will not negatively affect the STC of a wall provided:

- 1. It does not impede the performance of a resilient channel
- 2. It does not change the depth of an air space.



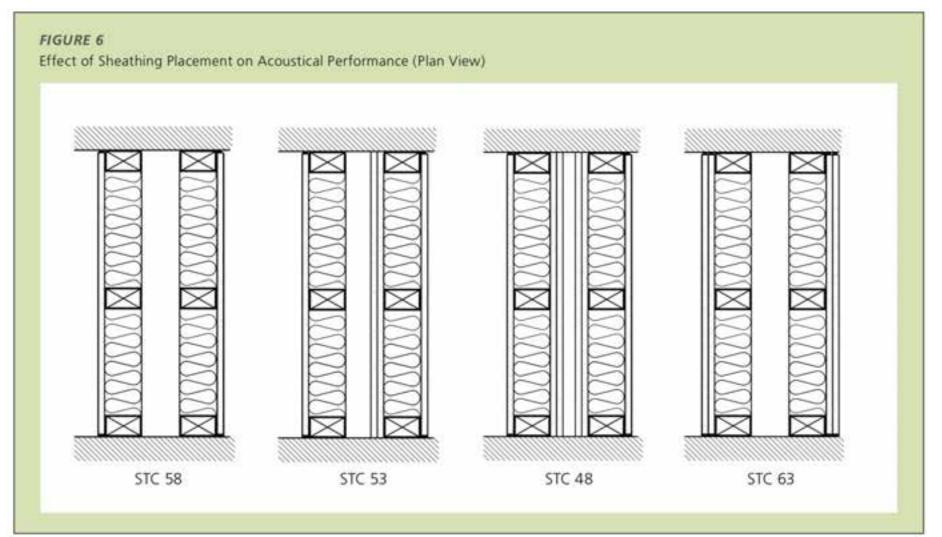
What if you add a layer of wood sheathing?

- For walls with resilient channels, put WSP on opposite side of wall
- For highly loaded shear walls, can use double layer of sheathing on same side of wall



What if you add a layer of wood sheathing?

WSP placement in double stud walls – big impact on STC



What if you add a layer of wood sheathing?

Can wood structural panels be added to an acoustically-tested wall assembly?

In many multi-family structures, interior demising walls that separate dwelling units from other units or from public spaces are required to have a minimum level of acoustical performance (IBC Section 1207). In some cases, these interior walls are also used as shear walls, utilizing plywood or OSB on one or both sides of the wall. Appropriate STC performance for walls are typically justified through the use of a tested assembly; however, most tested assemblies do not include wood structural panels (WSPs). This post contains information to help justify its inclusion in these cases.

In the WoodWorks technical paper, Acoustical Considerations for Mixed-Use Wood Frame Buildings, author Steve Thorburn discusses the impact that WSPs can have on acoustical performance of walls. Adding shear wall sheathing to a wall assembly can actually increase its acoustical performance in certain circumstances because it adds mass to the assembly. As Thorburn notes, "In the past, using multiple



layers of gypsum sheathing to increase the mass of the system has been the most common solution to raising the STC rating of the system. "He goes on, "In the case of shear wall sheathing, mass can be traded out for mass." However, designers should be careful where they place WSPs within the wall assembly.

With respect to placement, two conditions that could negatively affect the STC performance of a wall are 1) if the WSPs impede the performance of resilient channels, and 2) if the WSPs alter the depth of the air cavity.

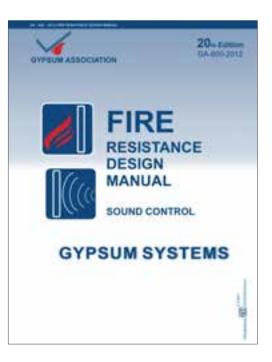
Resilient channels are a common component of many high-performing, acoustically-tested wall assemblies. If the assembly includes resilient channels on one side, the best practice is to put WSPs on the other (non-resilient channel) side of the wall, between the

https://www.woodworks.org/experttip/can-wood-structural-panels-addedacoustically-tested-wall-assembly/

What if you need to add insulation?

Fire Resistance – Insulation Effects

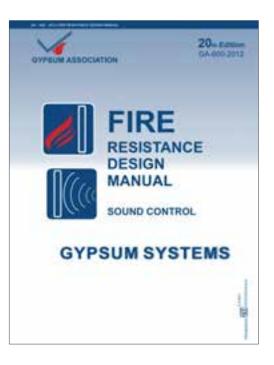
"<u>When not specified as a component of a</u> <u>fire tested wall or partition system,</u> <u>mineral fiber, glass fiber, or cellulose</u> <u>fiber insulation of a thickness not</u> <u>exceeding that of the stud depth shall be</u> <u>permitted to be added within the stud</u> <u>cavity."</u>



Fire Resistance – Insulation Effects

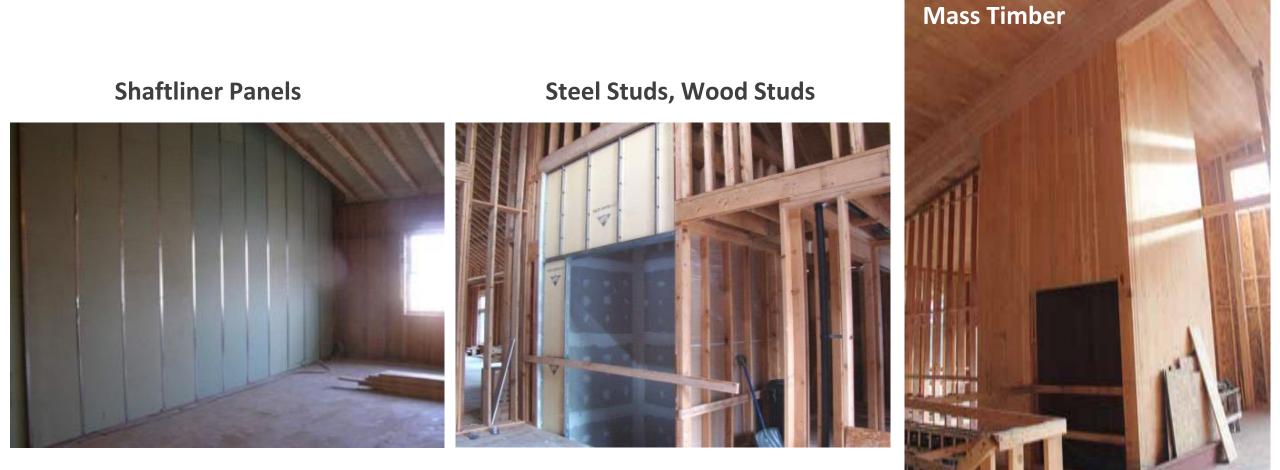
"<u>The addition of up to 16-3/4 inches of 0.5 pcf</u> <u>glass fiber insulation (R-40), either batt or loose-</u> <u>fill, to any 1- or 2-hour fire resistance rated floor-</u> <u>ceiling or roof-ceiling system</u> having a cavity deep enough to accept the insulation is permitted provided that <u>one additional layer of</u> <u>either 1/2 inch or 5/8 inch type X gypsum board is</u> <u>applied to the ceiling</u>. The additional layer of gypsum board shall be applied as described for the face layer of the tested system except that the fastener length shall be increased by not less than the thickness of the additional layer of gypsum board."

> Section 1.12 Gypsum Association's Fire Resistance Design Manual



Why would I use a shaftliner panel system as a shaft wall?

Shaft Walls – Material Options and Detailing Impacts



Shaftliner Systems - Benefits & Limitations

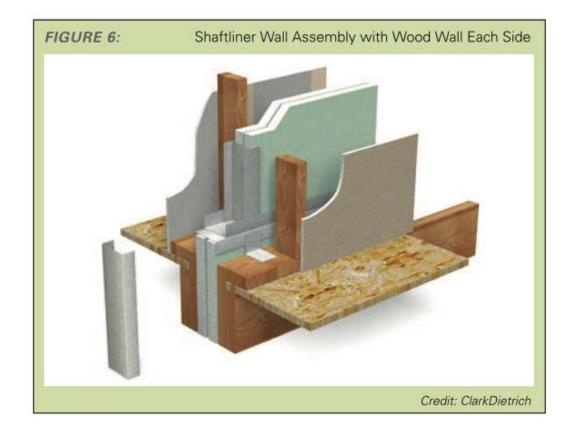
Benefits

Allows installation from one side only

 useful in small MEP shafts where
 finishing from inside isn't possible

Limitations

- Some have height limitations, both per story and overall system
- Not structural, requires back-up wood wall



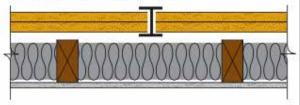


Source: Clark Dietrich

H-Stud Option

2-Hour Fire Rating

Design Reference: UL U373, ULC W312, WHI GP/WA 120-03, cUL U373

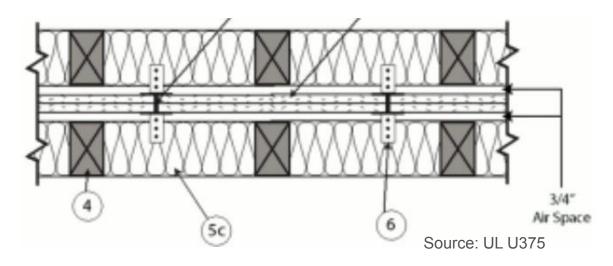


59 STC Sound Trans.

Test Reference: RAL TL 10-290

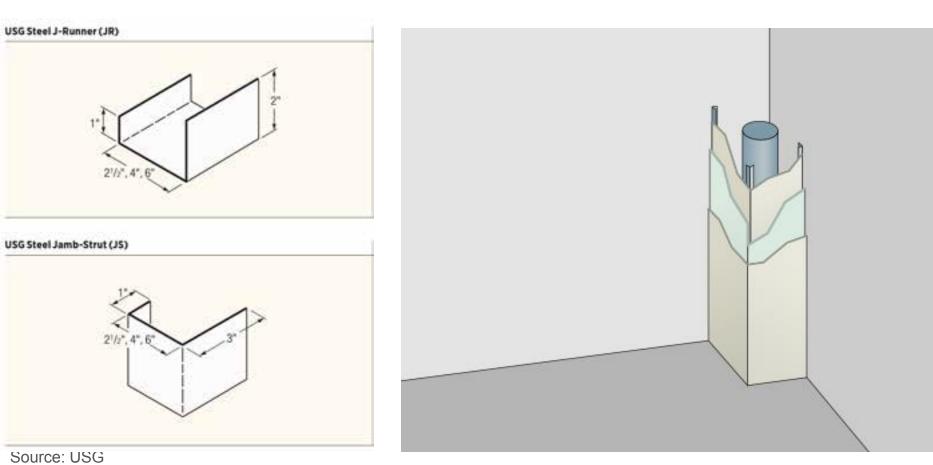
Two layers 1" (25.4 mm) DensGlass Shaftliner inserted in H-Studs 24" (610 mm) o.c. Min. 3/4" (19 mm) air space between liner panels and adjacent wood or metal framing.

Sound Tested with 2"x 4" stud wall with 1/2" (12.7 mm) ToughRock[®] wallboard or DensArmor Plus[®] interior panels and 3-1/2" (89 mm) fiberglass insulation in stud space. Source: Georgia Pacific



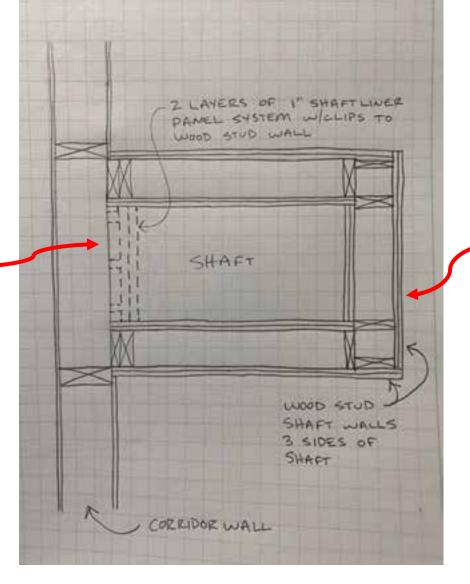
H-Stud Option







H-stud shaftliner with wood stud wall backup



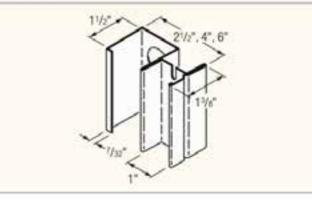
3 sides of wood shaft walls installed first. If shaft is small enough, might suggest shaftliner system on more than one side



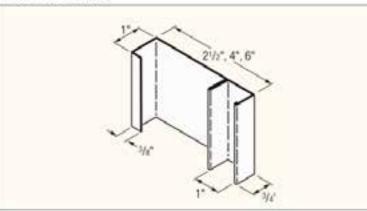
Source: Clark Dietrich

CH-Stud Option

USG Steel C-H Stud (CH)

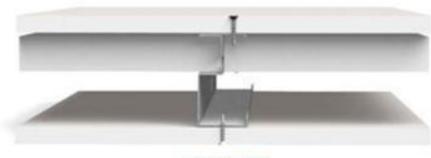


USG Steel E-Stud (ES)



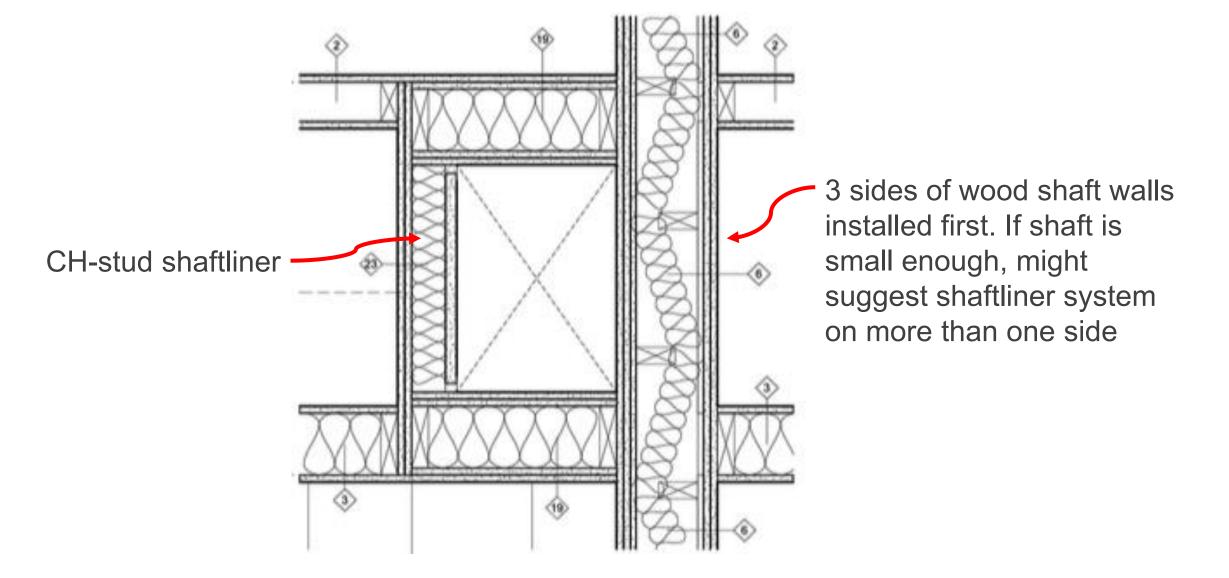
No wood backup wall





Stairwall Source: Clark Dietrich

Source: USG



Why do shaftliner panel height limits exist and how can I meet them in a 5+ story building?

Shaftliner Systems – Height Limits

Why do you need to support shaftliner panels?

- H-studs are non-structural
- Can only resist nominal horizontal pressures and self weight (but limited on self weight capacity)

PERFORMANCE SELECTOR

WALL SYSTEMS-LIMITING HEIGHTS TABLE

Stud Type and Size	Designation	Allowable Deflection	One-Hour Shaft Wall / Stairwell (U415 System A)*				Two-Hour Shaft Wall (U415 System C)*			
			5	7.5	10	15	5	7.5	10	15
2-1/2* С-н Studs	212CH-18	L/120	11'5*	10'0*	9'1" 4	7' 11" d	-	-	-	a S araan
		L/240	10' 7"	9'3"	8' 4" "	7' 4" *	-	-	-	=
		L/360	9' 4"	8'2"	7'5"	6'6"	-	-	-	-
	212CH-34	L/120	13' 5"	11'8"	10'8"	9'3"	-	-	-	-
		L/240	12" 3"	10'9"	9.9.	8'6"	-	-	-	-
		L/360	10'10*	9'6"	8' 7"	7'6"	-	-	-	-
4" C-H Studs	400CH-18	L/120	15' 2*	12' 5"	10.844	8'9**	15" 2"	12' 5"	10'9""	8' 9" #
		L/240	14'5"	12' 5"	10° 9° ±	8'9*¢	14'5"	12' 5"	10'9"=	8' 9" ±
		L/360	12"9"	11'2"	10° 1° d	8'9"d	12'9"	11' 2*	10' 1" d	8° 9° d
<u>_</u>	400CH-34	L/120	20'5"	17'10"	16' 2" "	13'4" =	20'5"	17'10"	16' 2* «	13' 4" *
		L/240	17' 6"	15' 3*	13'10"	12'1" #	17' 6"	15' 3"	13'10"	12'1" 4
		L/360	15' 3"	13' 4"	12'1*	10"7" «	15' 3"	13' 4"	12'1"	10'7**

Shaftliner Systems – Height Limits

Can also perform a structural analysis of the walls, especially when stacking multiple stories, to verify adequacy

		Allowable	e Momen	t, Shear a	and Effec	tive Sect	ion Prop	erties		
	Web	Flange	Stiffener	Design	Radius	Fy = 33 ksi, Fu = 45 ksi				
Section	A	В	C	Т	R	May	Vax	Iye	Sye	Ae
	in	in	in	in	in	kip-in	kips	in⁴	in ³	in ²
Web Depth 2.50"	Lip 1.00"									
250 J100-18	2.622	2.25	1.00	0.0188	0.0843	0.8999	0.247	0.0679	0.0455	0.0366
250 J100-27	2.636	2.25	1.00	0.0283	0.0796	1.5439	0.685	0.1123	0.0781	0.0754
250 J100-30	2.641	2.25	1.00	0.0312	0.0782	1.7646	0.832	0.1270	0.0893	0.0896
250 J100-33	2.646	2.25	1.00	0.0346	0.0764	2.0359	1.023	0.1448	0.1030	0.1073
Web Depth 2.50"	Lip 2.00"									
250 J200-18	2.622	2.25	2.00	0.0188	0.0843	0.8674	0.247	0.0792	0.0439	0.0369
250 J200-27	2.636	2.25	2.00	0.0283	0.0796	1.7070	0.685	0.1442	0.0864	0.0765
250 J200-30	2.641	2.25	2.00	0.0312	0.0782	1.9498	0.832	0.1634	0.0987	0.0910
250 J200-33	2.646	2.25	2.00	0.0346	0.0764	2.2482	1.023	0.1866	0.1138	0.1092
Web Depth 4.00"	Lip 1.00"									
400 J100-18	4.122	2.25	1.00	0.0188	0.0843	1.4271	0.152	0.1807	0.0722	0.0373
400 J100-27	4.136	2.25	1.00	0.0283	0.0796	3.0404	0.518	0.3395	0.1539	0.0780
400 J100-30	4.141	2.25	1.00	0.0312	0.0782	3.4461	0.695	0.3818	0.1744	0.0930
400 J100-33	4.146	2.25	1.00	0.0346	0.0764	3.9409	0.948	0.4326	0.1994	0.1121

Shaftliner Systems – Height Limits

Example Shaftliner Clip Attachment Schedule per UL U375						
System No.	System Height Limitation	Attachment Clip Schedule				
1	23 ft	10 ft o.c.				
2	44 ft	Base to 20 ft: 5 ft o.c. 20 ft to 44 ft: 10 ft o.c.				
3	66 ft	Base to 22 ft: 3'-4" o.c. 22 ft to 42 ft: 5 ft o.c. 42 ft to 66 ft: 10 ft o.c.				

H-Stud

Source: Clarkdietrich

Doesn't the shaftliner system need to bypass the floor?

Code requirements for shaft enclosures contained in IBC Section 713

SECTION 713 SHAFT ENCLOSURES

713.1 General. The provisions of this section shall apply to shafts required to protect openings and penetrations through floor/ceiling and roof/ceiling assemblies. *Interior exit stairways* and *ramps* shall be enclosed in accordance with Section 1023.

- IBC 713.2: Shaft Walls shall be constructed as Fire Barriers
- Many shaft wall provisions contained in IBC Section 707 Fire Barriers

SECTION 713 SHAFT ENCLOSURES

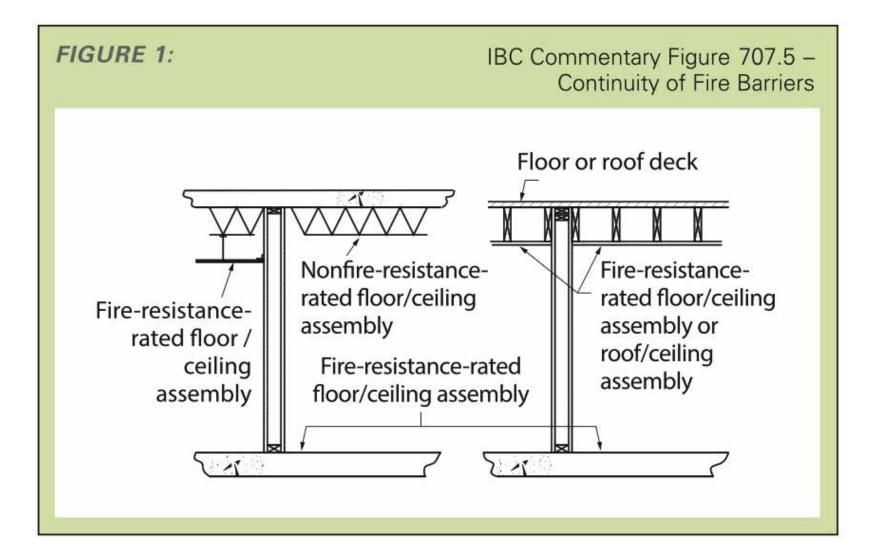
713.5 Continuity.

Shaft enclosures shall have continuity in accordance with 707.5 for fire barriers.

SECION 707 FIRE BARRIERS

707.5 Continuity.

Fire barriers <u>shall extend from the top of the foundation or floor/ceiling assembly</u> <u>below to the underside of the floor or roof sheathing, slab or deck above and shall be</u> <u>securely attached thereto.</u> Such fire barriers shall be <u>continuous though concealed</u> <u>space</u> such as the space above a suspended ceiling. Joints and voids at intersections shall comply with Sections 707.8 and 707.9.

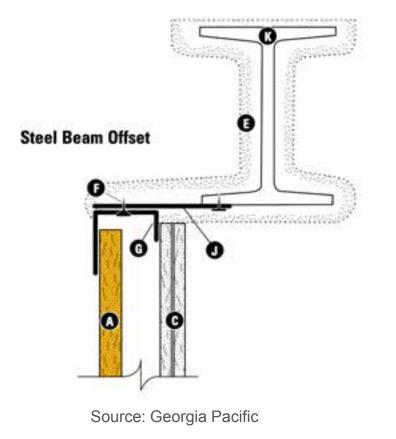


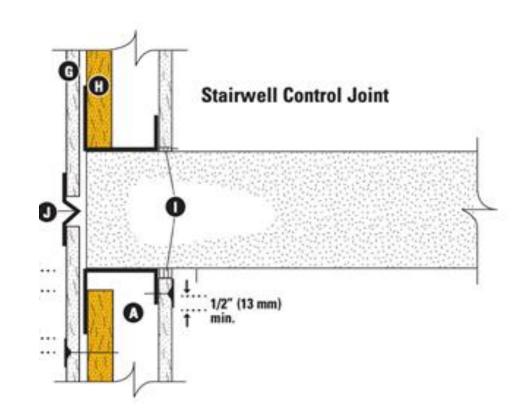


The continuity of the fire barrier's fire protection can be maintained even if the wall framing does not extend to the underside of the decking above



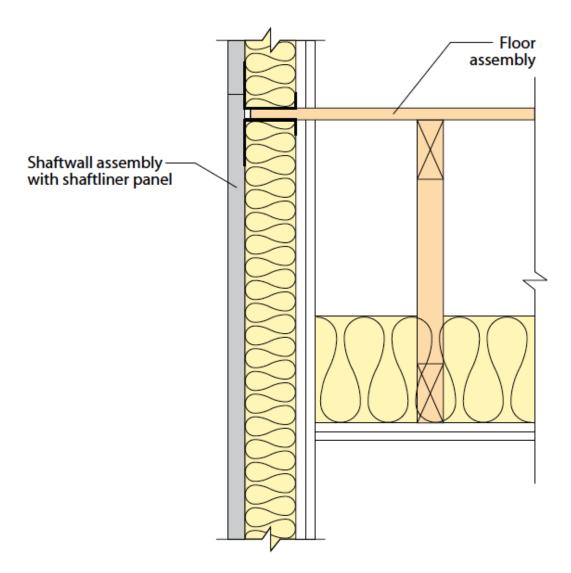
Non-bypassing details with noncombustible construction





How do I support a shaftliner panel system on a wood floor assembly?

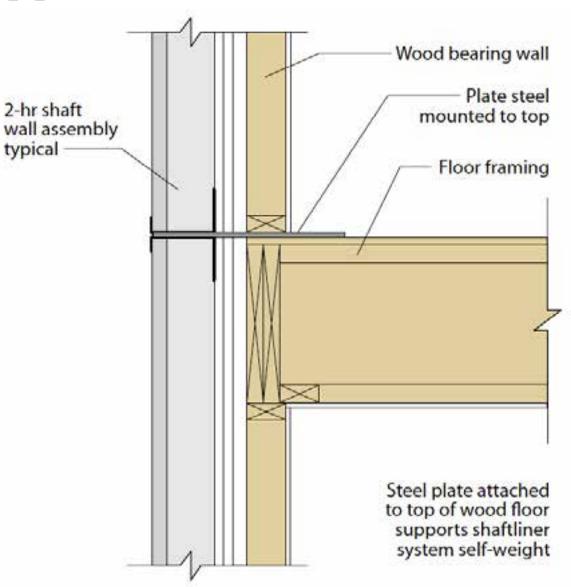
Floor sheathing cantilevers out to support shaftliner system self-weight



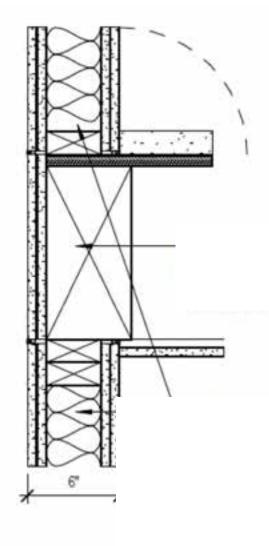
Wood bearing wall Floor framing Shaft wall assembly Continuous steel angle Steel angle attached to wood rim joist supports shaftliner system self-weight

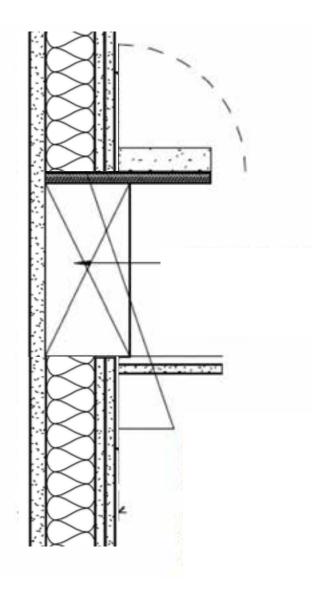
Steel angle attached to wood rim joist supports shaftliner system self-weight

Steel plate attached to top of wood floor supports shaftliner system self-weight

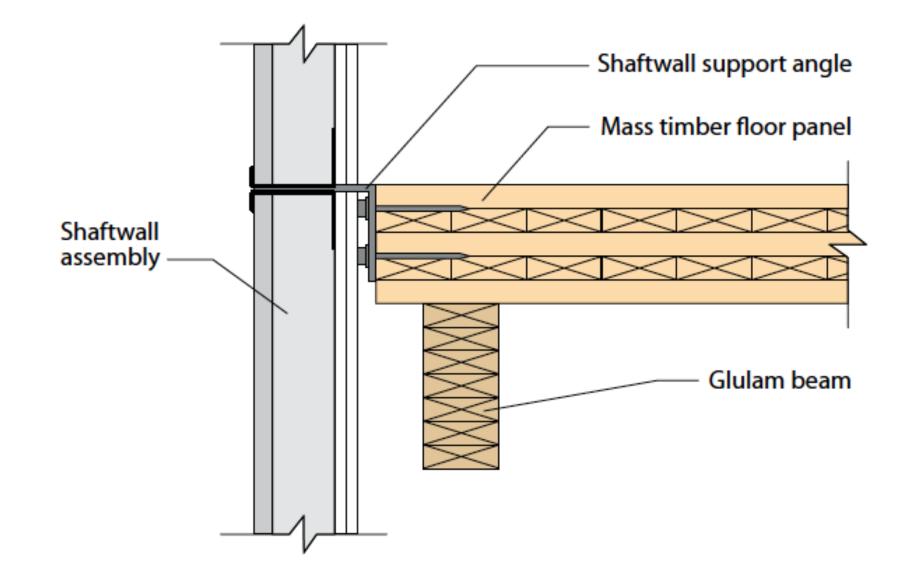


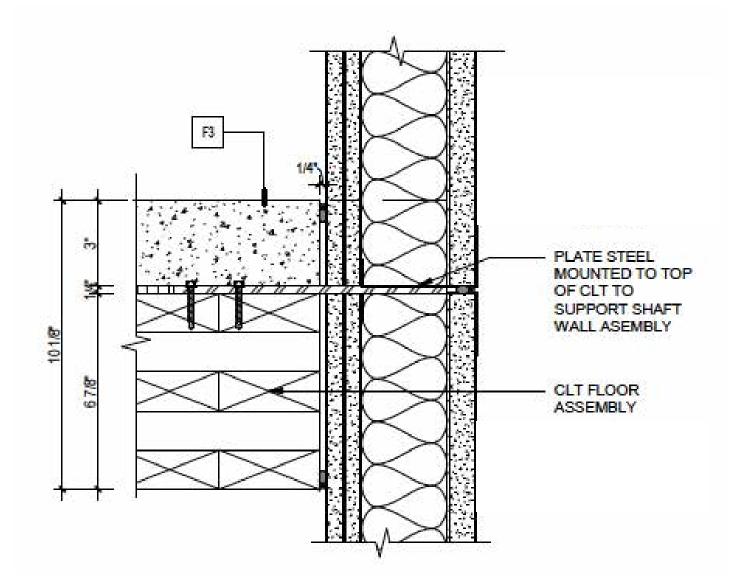
Shaftliner system self-weight supported on wood floor in platform framed condition





What about shaftliner systems combined with mass timber floors?

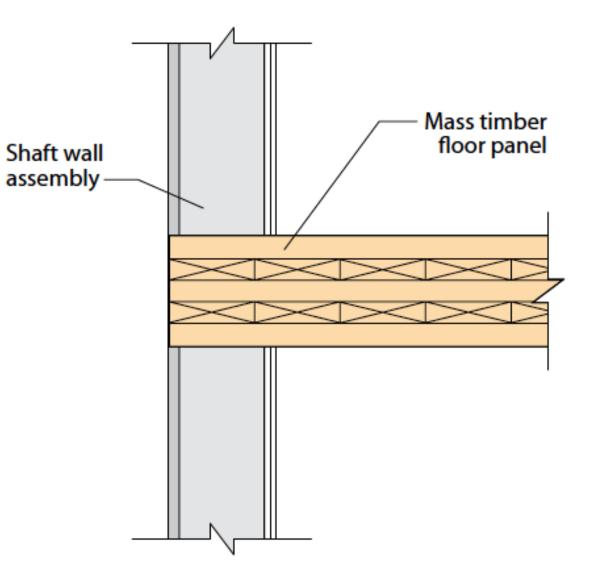


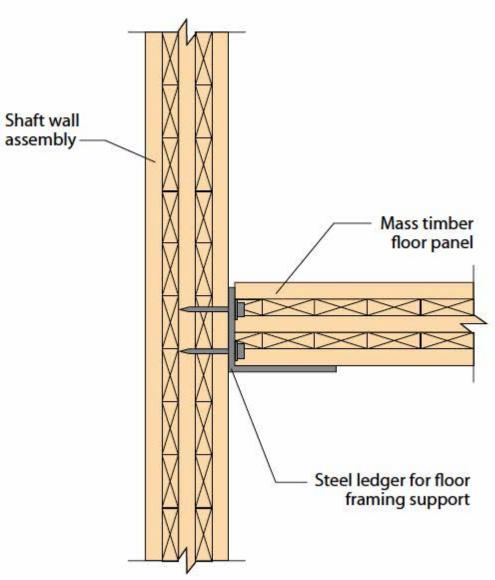


Recall fire barrier continuity definition:

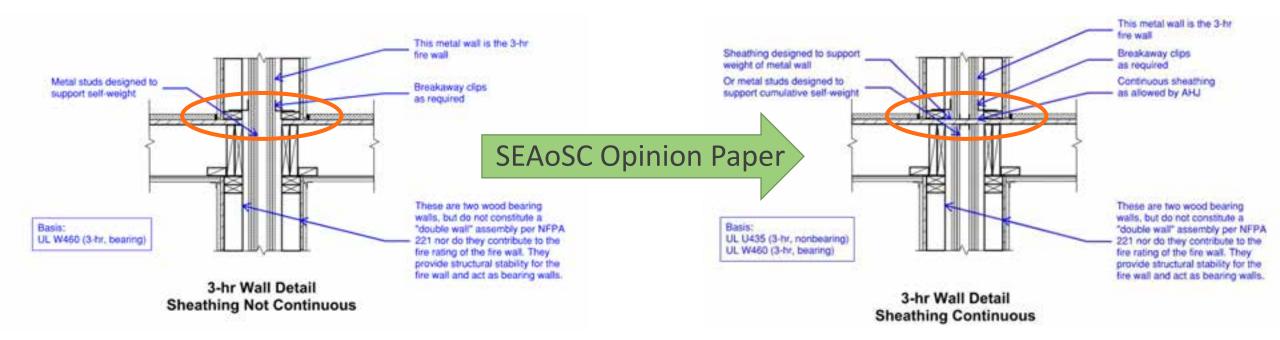
shall extend ... to the underside of the floor or roof sheathing, slab or deck above and shall be securely attached thereto

CLT is the "slab" and it is not disrupting the continuity of the shaft wall





Seismic Considerations for Fire Walls



2018 IBC:

706.2 Structural stability.

Fire walls shall be designed and constructed to allow collapse of the structure on either side without collapse of the wall under fire conditions. Fire walls designed and constructed in accordance with NFPA 221 shall be deemed to comply with this section.

Exception: In Seismic Design Categories D through F, where double five walls are used in accordance with NFPA 221, floor and roof sheathing not exceeding ³/₄ inch (19.05 mm) thickness shall be permitted to be continuous through the wall assemblies of light frame construction.

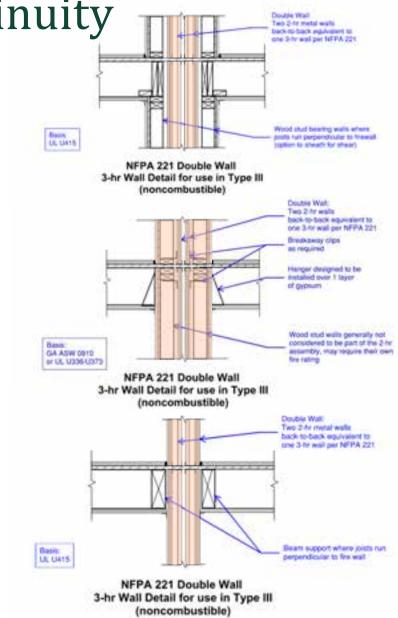
s

NFPA 221:

4.5* Double Wall Assemblies. Where either wall of a double wall is laterally supported by a building frame with a fire resistance rating less than that required for the wall, double wall assemblies shall be considered to have a combined assembly fire resistance rating as specified in Table 4.5.

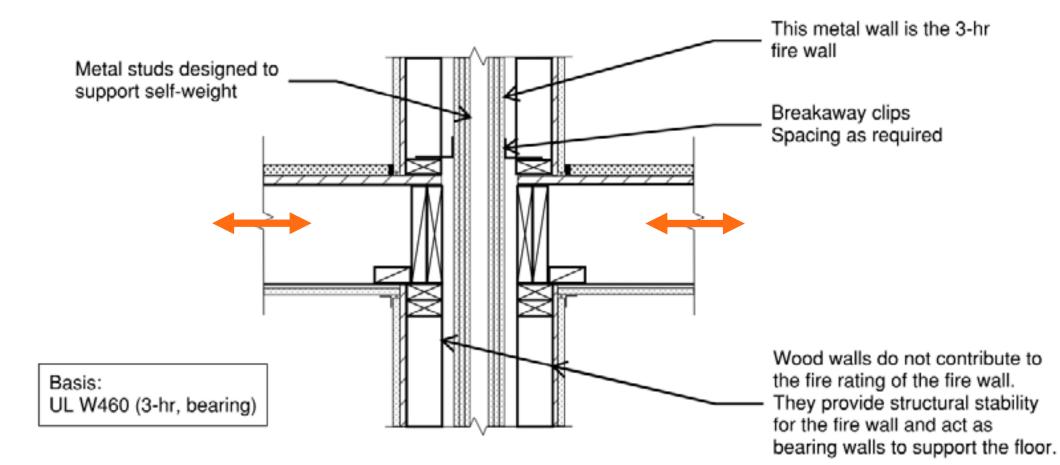
Table 4.5 Fire Resistance Ratings for Double Wall Assemblies

Fire Resistance Rating of Each Wall (hr)	Equivalent to Single Wall (hr)
3	4
2	3
1	2

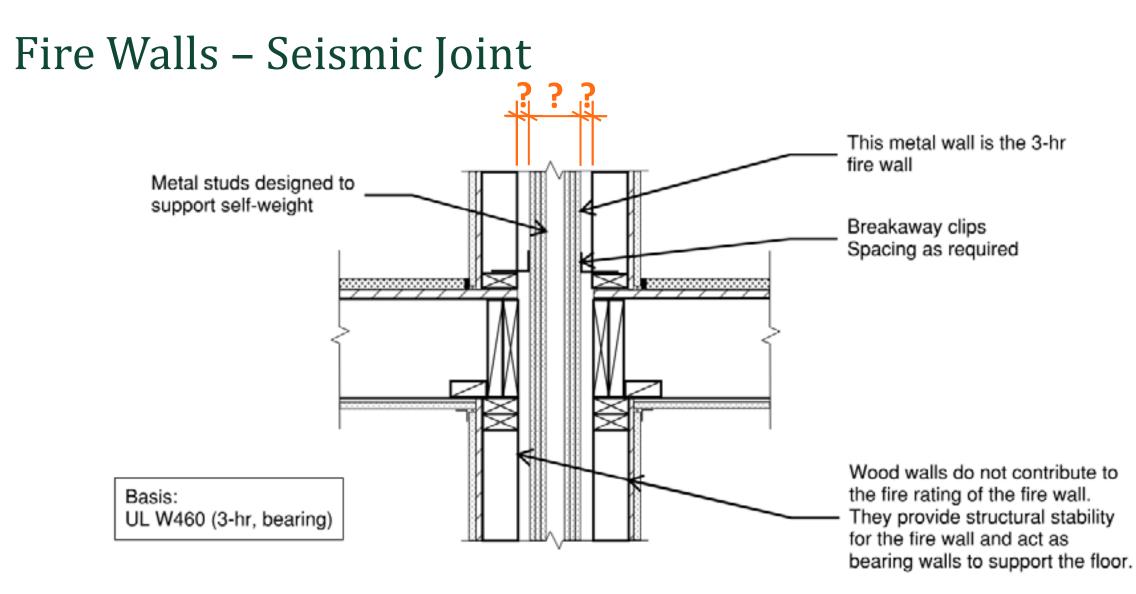


But what if we <u>want</u> a seismic separation?

Fire Walls – Seismic Joint

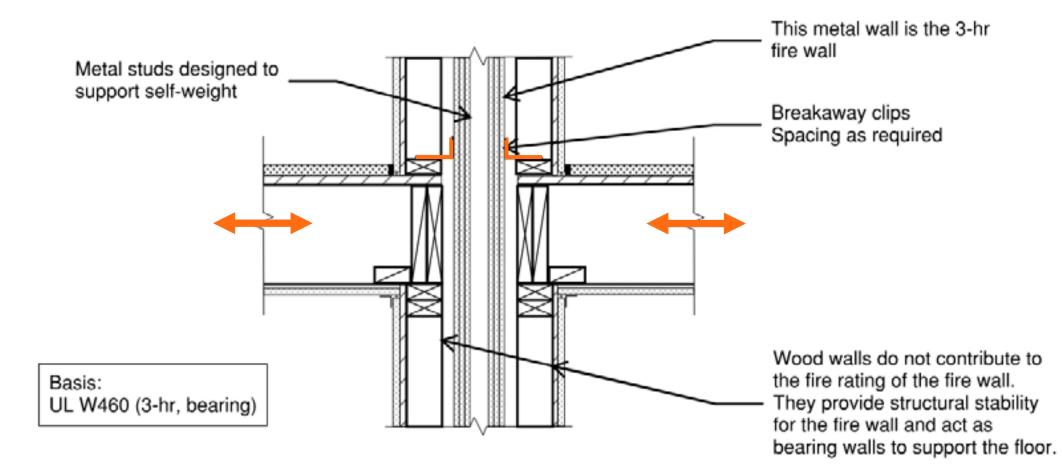


3-hr Wall Detail Sheathing Not Continuous



3-hr Wall Detail Sheathing Not Continuous

Fire Walls – Seismic Joint



3-hr Wall Detail Sheathing Not Continuous

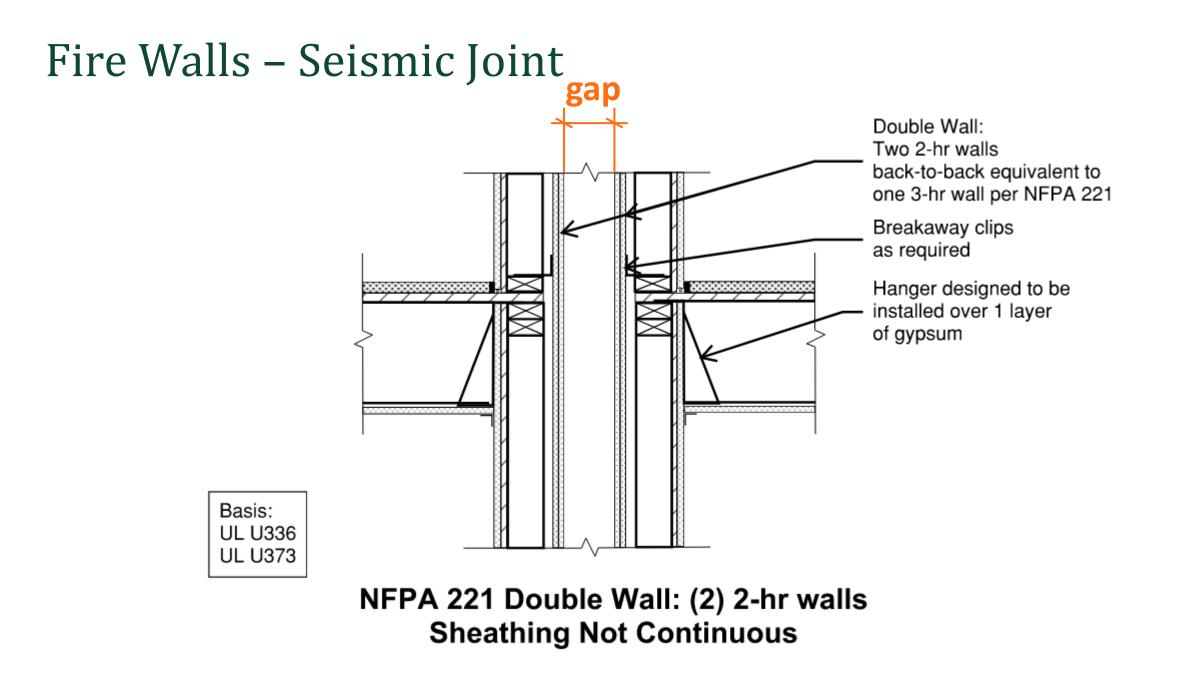
Fire Walls – Seismic Joint

2018 IBC Provisions for Structural Stability

706.2 Structural stability.

Fire walls shall be designed and constructed to allow collapse of the structure on either side without collapse of the wall under fire conditions. Fire walls designed and constructed in accordance with NFPA 221 shall be deemed to comply with this section.

Exception: In Seismic Design Categories D through F, where double *fire walls* are used in accordance with NFPA 221, floor and roof sheathing not exceeding ³/₄ inch (19.05 mm) thickness shall be permitted to be continuous through the wall assemblies of light frame construction.



What if we want diaphragm continuity but we're in a lower SDC?

2018 IBC Provisions allow floor sheathing through firewall under certain conditions

706.2 Structural stability.

Fire walls shall be designed and constructed to allow collapse of the structure on either side without collapse of the wall under fire conditions. *Fire walls* designed and constructed in accordance with NFPA 221 shall be deemed to comply with this section.

Exception: In Seismic Design Categories D through F, where double *fire walls* are used in accordance with NFPA 221, floor and roof sheathing not exceeding ³/₄ inch (19.05 mm) thickness shall be permitted to be continuous through the wall assemblies of light frame construction.



SEAoSC LIGHT-FRAMING CONSTRUCTION COMMITTEE STRUCTURAL ENGINEERS ASSOCIATION OF SOUTHERN CALIFORNIA SEISMOLOGY OPINION

DATE: March 21, 2008

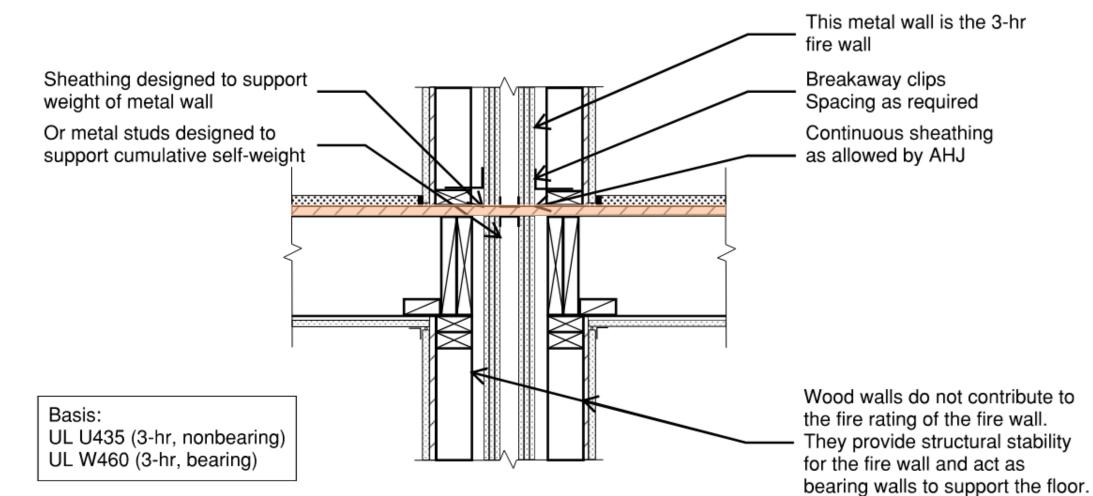
Continuity of Plywood Diaphragm Sheathing in 2 hr and 3hr Fire Walls:

Opinion: The continuity of plywood diaphragm sheathing should be maintained across the air gap commonly encountered in double stud Firewalls of 2 or 3 hour construction. The intent is to ensure that structural continuity is not significantly reduced in the roof and floor diaphragms.

Commentary:

This opinion is prepared to address the issue of diaphragm continuity as it relates to recent changes in 2007 CBC and 2006 IBC model code. Specifically the outgoing UBC provisions for Area-Separation walls have more or less been replaced by the Fire wall provisions of the IBC. Such walls are encountered in light-frame multifamily or mixed-use construction and are often constructed as a double studwall when occurring at partywall locations. The double stud walls are typically separated by an airspace of a one to four inches.

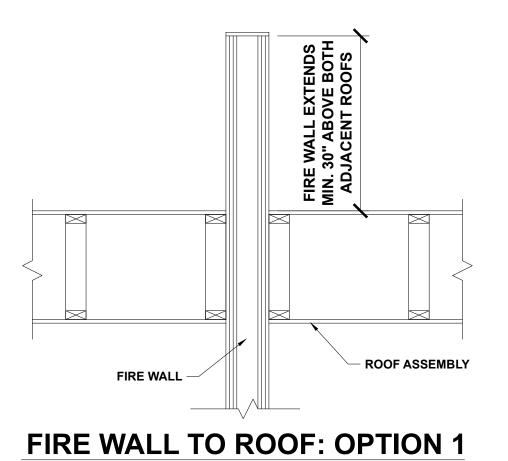
The IBC has introduced language [IBC 705.4] that states fire walls must have "sufficient structural stability" under fire conditions to allow collapse of either side. Previous commentary to the UBC topic of Area Separation



3-hr Wall Detail Sheathing Continuous

Fire Walls – Vertical Continuity

• Fire walls are required to be continuous from foundation to roof

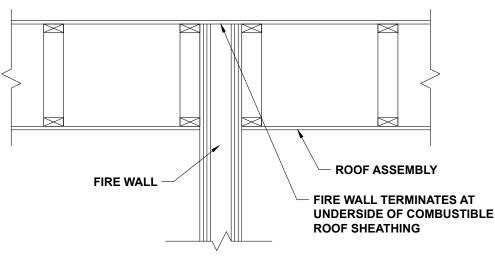


Fire Walls – Vertical Continuity

IN CONSTRUCTION TYPES III, IV OR V

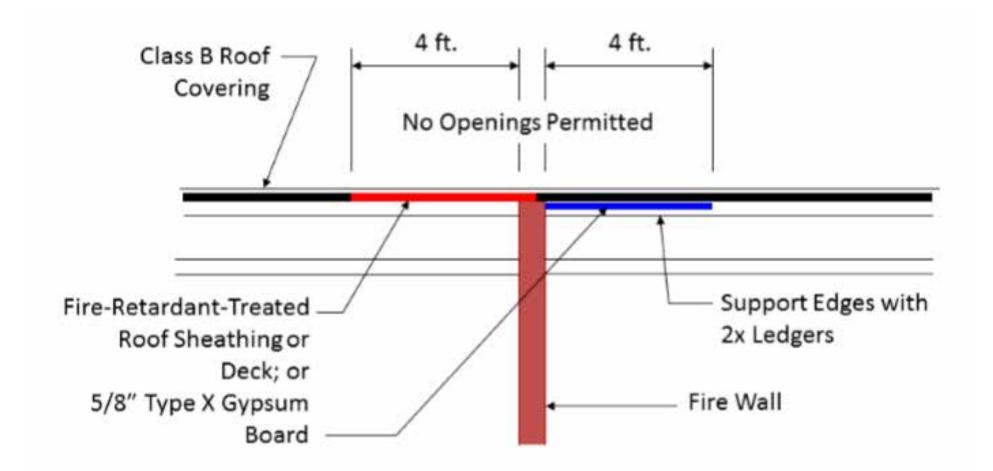
- NO OPENINGS IN ROOF WITHIN 4FT OF FIRE WALL
- MIN. CLASS B ROOF COVERING
- ROOF SHEATHING/DECK MIN. 4FT EACH SIDE OF WALL IS FRT

OR UNDERSIDE OF SHEATHING IS COVERED WITH $\frac{5}{8}$ " TYPE X GYPSUM



FIRE WALL TO ROOF: OPTION 2

Fire Walls – Vertical Continuity



Are the studs required to be FRT?

No!

Could we use FRT in lieu of noncombustible?

Exterior Walls – Materials

602.3 Type III.

Type III construction is that type of construction in which the exterior walls are of noncombustible materials and the interior building elements are of any material permitted by this code. Fire-retardant-treated wood framing and sheathing complying with Section 2303.2 shall be permitted within exterior wall assemblies of a 2-hour rating or less.

Commentary:

Although fire-retardant-treated wood (FRTW) does not meet the specifications of the code as a noncombustible material, it is permitted as a substitute for noncombustible materials for framing and sheathing within exterior wall assemblies of Type III construction. ...the required fire-resistance rating of the exterior wall must not be greater than 2 hours.

Fire Walls – Materials

706.3 Materials.

Fire walls shall be of any approved noncombustible materials.

Exception: Buildings of Type V construction.

Commentary:

This section requires that fire walls be constructed of noncombustible materials unless both buildings are of Type V (combustible) construction. This is consistent with the provisions of Section 602, which require exterior walls of buildings of Type I, II, III and IV to be built of noncombustible construction, while buildings of Type V construction are permitted to be built of combustible exterior walls.

Fire Walls – Ratings

TABLE 706.4 FIRE WALL FIRE-RESISTANCE RATINGS

F-1, H-3 ^b , H-5, M, S-1 3 H-1, H-2 4 ^b	GROUP	FIRE-RESISTANCE RATING (hours)
H-1, H-2 4 ^b	A, B, E, H-4, I, R-1, R-2, U	3ª
	F-1, H-3 ^b , H-5, M, S-1	3
F-2 S-2 R-3 R-4 2	H-1, H-2	4 ^b
	F-2, S-2, R-3, R-4	2

 In Type II or V construction, walls shall be permitted to have a 2-hour fire-resistance rating.

b. For Group H-1, H-2 or H-3 buildings, also see Sections 415.6 and 415.7.

QUESTIONS?

This concludes The American Institute of Architects Continuing Education Systems Course



Karen Gesa, PE WoodWorks – Wood Products Council <u>Karen.Gesa@woodworks.org</u> 703.789.6096 Ricky McLain, PE, SE WoodWorks – Wood Products Council Ricky.McLain@woodworks.org 802.498.3310 Ashley Cagle, PE, SE WoodWorks – Wood Products Council Ashley.cagle@woodworks.org 703.201.3910

Copyright Materials

This presentation is protected by US and International Copyright laws. Reproduction, distribution, display and use of the presentation without written permission of the speaker is prohibited.

© The Wood Products Council 2021

Disclaimer: The information in this presentation, including, without limitation, references to information contained in other publications or made available by other sources (collectively "information") should not be used or relied upon for any application without competent professional examination and verification of its accuracy, suitability, code compliance and applicability by a licensed engineer, architect or other professional. Neither the Wood Products Council nor its employees, consultants, nor any other individuals or entities who contributed to the information make any warranty, representative or guarantee, expressed or implied, that the information is suitable for any general or particular use, that it is compliant with applicable law, codes or ordinances, or that it is free from infringement of any patent(s), nor do they assume any legal liability or responsibility for the use, application of and/or reference to the information. Anyone making use of the information in any manner assumes all liability arising from such use.