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Questions related to specific materials, methods, and services will be addressed at the conclusion of this presentation.



Course Description

In January 2019, the International Code Council (ICC) approved a set of proposals to allow tall wood buildings as part of the 2021 International Building Code (IBC). Based on these proposals, the 2021 IBC will include three new construction types—Type IV-A, IV-B and IV-C—allowing the use of mass timber or noncombustible materials. These new types are based on the previous Heavy Timber construction type (renamed Type IV-HT) but with additional fireresistance ratings and levels of required noncombustible protection. This presentation will take a detailed look at the new code provisions and methods of addressing the new requirements. Topics will include tall-wood specific high rise and sprinkler requirements, methods of demonstrating fire-resistance ratings, fire design for penetrations, connections and abutting panels, allowances for exposed timber, exterior walls, concealed spaces and more.



Learning Objectives

- 1. Explore the three new tall wood construction types and discuss related code provisions such as allowable heights and fire-resistance ratings.
- 2. Discuss code-compliant options for exposing mass timber, where up to 2-hour fire-resistance ratings are required, and demonstrate design methodologies for achieving these ratings.
- 3. Review code requirements unique to tall wood buildings, focusing on items such as sprinklers, shaft construction and concealed spaces.
- 4. Highlight design options for addressing topics such as fire stops at penetrations through mass timber assemblies and exterior walls fire-resistance in tall timber structures.



NEW CONSTRUCTION TYPES IN 2021 IBC

Type IV-A – Maximum 18 stories, with gypsum wallboard on all mass timber.

Type IV-B – Maximum 12 stories, limitedarea of exposed mass timber walls and ceilings allowed.

Type IV-C – Maximum 9 stories, all exposed mass timber designed for a 2-hour fire resistance.



New Building Types



18 STORIES
BUILDING HEIGHT 270'
ALLOWABLE BUILDING AREA 972,000 SF
AVERAGE AREA PER STORY 54,000SF

TYPE IV-A

12 STORIES
BUILDING HEIGHT 180 FT
ALLOWABLE BUILDING AREA
AVERAGE AREA PER STORY 54,000SF

TYPE IV-B

IBC 2021



9 STORIES
BUILDING HEIGHT 85'
ALLOWABLE BUILDING AREA 405,000 SF
AVERAGE AREA PER STORY 45,000 SF

TYPE IV-C



BUSINESS OCCUPANCY [GROUP B]

*BUILDING FLOOR-TO-FLOOR HEIGHTS ARE SHOWN AT 12'-0" FOR ALL EXAMPLES FOR CLARITY IN COMPARISON BETWEEN 2015 TO 2021 IBC CODES.

Credit: Susan Jones, atelierjones



Tall Wood Building Size Limits

		Co	nstruction T	ype (All <u>Spri</u>	nklered Valu	ies)	
	I-A	I-B	<u>IV-A</u>	<u>IV-B</u>	<u>IV-C</u>	IV-HT	III-A
Occupancies	Allo	wable Build	ing Height al	bove Grade l	Plane, Feet ()	IBC Table 50	4.3)
A, B, R	Unlimited	180	<u>270</u>	<u>180</u>	<u>85</u>	85	85
	Al	lowable Nun	nber of Stori	es above Gra	de Plane (IB	C Table 505	.4)
A-2, A-3, A-4	Unlimited	12	<u>18</u>	<u>12</u>	<u>6</u>	4	4
В	Unlimited	12	<u>18</u>	<u>12</u>	9	6	6
R-2	Unlimited	12	<u>18</u>	12	8	5	5
		Allowable A	Area Factor (At) for SM,	Feet ² (IBC 7	Table 506.2)	
A-2, A-3, A-4	Unlimited	Unlimited	135,000	90,000	<u>56,250</u>	45,000	42,000
В	Unlimited	Unlimited	324,000	216,000	135,000	108,000	85,500
R-2	Unlimited	Unlimited	184,500	123,000	<u>76,875</u>	61,500	72,000



Tall Wood Building Size Limits

		Constr	uction Type (<u>U</u>	nsprinklered	Values)	
	I-A	I-B	<u>IV-A</u>	<u>IV-B</u>	<u>IV-C</u>	IV-HT
Occupancies	Allowa	ble Building H	Height above C	Frade Plane, F	eet (IBC Table	504.3)
A, B, R	Unlimited	160	<u>65</u>	<u>65</u>	<u>65</u>	65
	Allov	vable Number	of Stories abo	ve Grade Plan	e (IBC Table 5	505.4)
A-2, A-3, A-4	Unlimited	11	<u>3</u>	<u>3</u>	<u>3</u>	3
В	Unlimited	11	<u>5</u>	<u>5</u>	<u>5</u>	5
R-2	Unlimited	11	4	4	4	4
	A	llowable Area	Factor (At) for	r SM, Feet ² (I	BC Table 506.	2)
A-2, A-3, A-4	Unlimited	Unlimited	45,000	30,000	18,750	15,000
В	Unlimited	Unlimited	108,000	72,000	45,000	36,000
R-2	Unlimited	Unlimited	61,500	41,000	25,625	20,500



Tall Wood Building Size Limits

		Constr	uction Type (L	nsprinklered	Values)						
	I-A	I-B	<u>IV-A</u>	<u>IV-B</u>	<u>IV-C</u>	IV-HT					
Occupancies	Allowa	ble Building I	Height above G	Frade Plane, Fo	eet (IBC Table	504.3)					
A, B, R	Unlimited	160	<u>65</u>	<u>65</u>	<u>65</u>	65					
	Allo	Unlimited 160 65 65 65 65 Allow Nie author OS traino Gase Sane (IBC Table 505.4)									
A-2, A-3, A-4	Unlimited.	aklarc	will be	<u>3</u>	$\mathbf{rod}^{\underline{3}}$	3					
В	Unan Red	ıkıçıs	wiii be	regun		5					
R-2	Unlimited	11	4	4	4	4					
	A	llowable Area	Factor (At) for	r SM, Feet ² (I	BC Table 506.	2)					
A-2, A-3, A-4	Unlimited	Unlimited	45,000	30,000	18,750	15,000					
В	Unlimited	Unlimited	108,000	72,000	45,000	36,000					
R-2	Unlimited	Unlimited	61,500	41,000	25,625	20,500					



Non-Tall Opportunities – Large Area

		Co	nstruction T	ype (All <u>Spri</u>	nklered Valu	<u>es</u>)	
	I-A	I-B	<u>IV-A</u>	<u>IV-B</u>	<u>IV-C</u>	IV-HT	III-A
Occupancies	Allo	wable Build	ing Height al	bove Grade]	Plane, Feet (I	BC Table 50	4.3)
A, B, R	Unlimited	180	<u>270</u>	<u>180</u>	<u>85</u>	85	85
	Al	lowable Nun	nber of Stori	es above Gra	de Plane (IB	C Table 505	.4)
A-2, A-3, A-4	Unlimited	12	<u>18</u>	<u>12</u>	<u>6</u>	4	4
В	Unlimited	12	<u>18</u>	<u>12</u>	9	6	6
R-2	Unlimited	12	18	12	8	5	5
		Allowable A	Area Factor (At) for SM,	Feet ² (IBC 7	Table 506.2)	L
A-2, A-3, A- 4	Unlimited	Unlimited	135,000	90,000	<u>56,250</u>	45,000	42,000
В	Unlimited	Unlimited	324,000	216,000	135,000	108,000	85,500
R-2	Unlimited	Unlimited	184,500	123,000	<u>76,875</u>	61,500	72,000



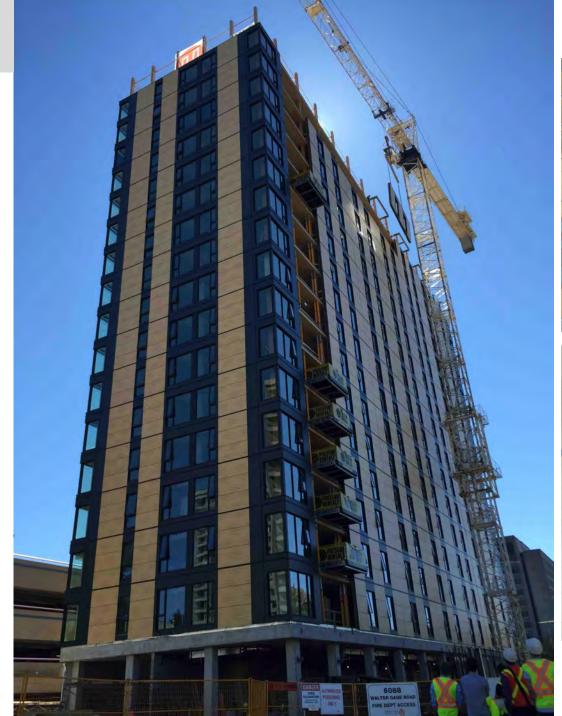
Type IV-A



18 STORIES
BUILDING HEIGHT 270'
ALLOWABLE BUILDING AREA 972,000 SF
AVERAGE AREA PER STORY 54,000SF

TYPE IV-A

Credit: Susan Jones, atelierjones







Photos: Structurlam, naturally:wood, Fast + Epp

18 STORIES
BUILDING HEIGHT 270'
ALLOWABLE BUILDING AREA 972,000 SF
AVERAGE AREA PER STORY 54,000SF

TYPE IV-A

Credit: Susan Jones, atelierjones

Type IV-A Height and Area Limits

Occupancy	# of Stories	Height	Area per Story	Building Area
A-2	18	270 ft	135,000 SF	405,000 SF
В	18	270 ft	324,000 SF	972,000 SF
M	12	270 ft	184,500 SF	553,500 SF
R-2	18	270 ft	184,500 SF	553,500 SF

Areas exclude potential frontage increase

In most cases, Type IV-A height & story allowances = 1.5 * Type I-B height & story allowances

Type IV-A area = 3 * Type IV-HT area

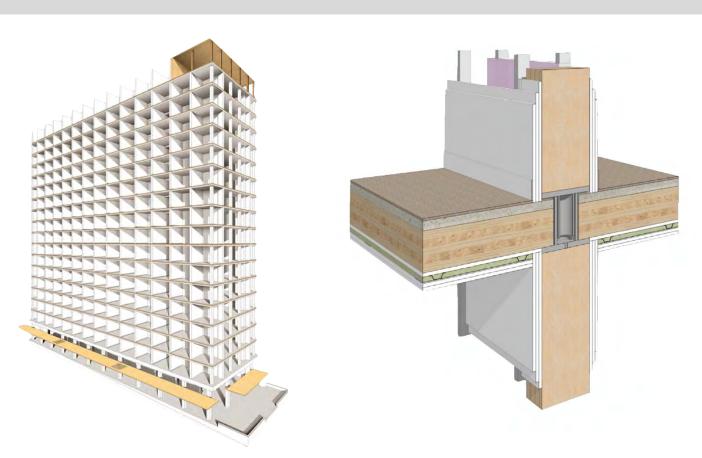


18 STORIES BUILDING HEIGHT 270' ALLOWABLE BUILDING AREA 972,000 SF AVERAGE AREA PER STORY 54,000SF

TYPE IV-A

Credit: Susan Jones, atelierjones

Type IV-A Protection vs. Exposed



100% NC protection on all surfaces of Mass Timber



Type IV-A Fire Resistance Ratings (FRR)







Primary Frame FRR

Ext or Int Bearing Wall FRR

Floor Construction FRR

Roof Construction FRR

3 HR (2 HR at Roof)

3 HR

2 HR

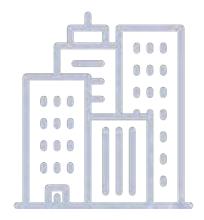
1.5 HR



Type IV-A Fire Resistance Ratings (FRR)







Primary Frame FRR

Ext or Int Bearing Wall FRR

Floor Construction FRR

Roof Construction FRR

½" Type X Gypsum = 25 min

FRR	Min. NC Protection
3 HR (2 HR at	120 min (80 min
Roof)	at Roof)
3 HR	120 min
2 HR	80 min
1.5 HR	80 min

5/8" Type X Gypsum = 40 min



Noncombustible Protection (NC)

TABLE 722.7.1(a) PROTECTION REQUIRED FROM NONCOMBUSTIBLE COVERING MATERIAL

Required Fire Resistance Rating of Building Element per Tables 601 and 602 (hours)	Minimum Protection R Noncombustible Protec	
1	<u>40</u>	1 layer 5/8 Type X
2	<u>80</u>	2 layers 5/8 Type X
3 or more	<u>120</u>	3 layers 5/8 Type X

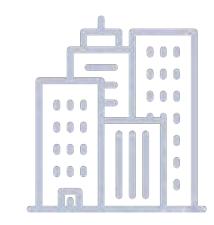
TABLE 722.7.1(b) PROTECTION PROVIDED BY NONCOMBUSTIBLE COVERING MATERIAL

Noncombustible Protection	<u>Protection Contribution</u> (minutes)
1/2 inch Type X Gypsum Board	<u>25</u>
5/8 inch Type X Gypsum Board	<u>40</u>



Noncombustible Protection (NC)





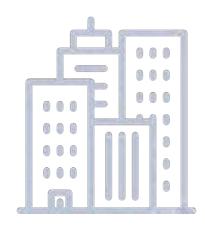
The definition of "Noncombustible Protection (For Mass Timber)" is created to address the passive fire protection of mass

timber.

Mass timber is permitted to have its own fire-resistance rating (e.g., Mass Timber only) or have a fire resistance rating based on the fire resistance through a combination of the mass timber fire-resistance plus protection by non-combustible materials as defined in Section 703.5 (e.g., additional materials that delay the combustion of mass timber, such as gypsum board).







IBC 722.7

The fire resistance rating of the mass timber elements shall consist of the fire resistance of the unprotected element (MT) added to the protection time of the noncombustible (NC) protection.



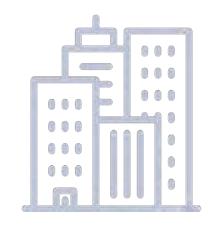












However, FRR Doesn't always need to be from a combination of MT + NC. In some cases, just NC can be used, in other cases, just MT can be used:



IBC 602.4

Mass timber elements shall meet the fire resistance rating requirements of this section based on either the fire resistance rating of the noncombustible protection, the mass timber, or a combination of both.

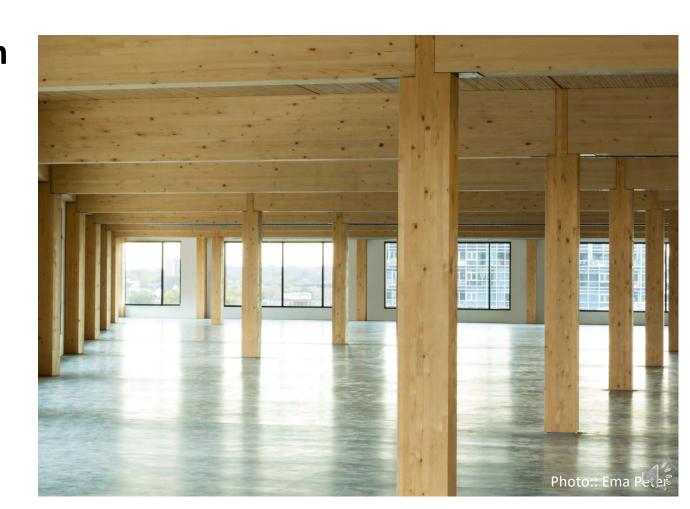


MT Type IV Minimum Sizes

In addition to meeting FRR, all MT elements must also meet minimum sizes

These minimum sizes have been in place for old type IV (current type IV-HT) construction and the same minimums sizes also apply to MT used in new types IV-A, IV-B and IV-C

Contained in IBC 2304.11

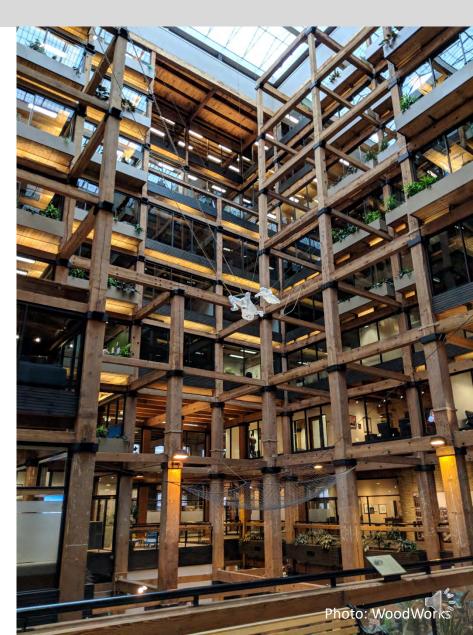


Type IV Minimum Sizes - Framing

F	Framing Solid Sawn (nominal)		Glulam (actual)	SCL (actual)
or	Columns	8 x 8	$6^3/_4 \times 8\frac{1}{4}$	7 x 7½
Floor	Beams	6 x 10	5 x 10½	5¼ x 9½
of	Columns	6 x 8	5 x 8¼	5¼ x 7½
Roof	Beams*	4 x 6	3 X 6 ⁷ / ₈	3½ X 5½

Minimum Width by Depth in Inches
See IBC 2018 2304.11 or IBC 2015 602.4 for Details

*3" nominal width allowed where sprinklered



Type IV Minimum Sizes – Floor/Roof Panels

Floor Panels/Decking:

- 4" thick CLT (actual thickness)
- 4" NLT/DLT/GLT (nominal thickness)
- 3" thick (nominal) decking covered with:
 1" decking or 15/32" WSP or ½"
 particleboard

Roof Panels/Decking:

- 3" thick CLT (nominal thickness)
- 3" NLT/DLT/GLT (nominal thickness)
- 2" decking (nominal thickness)
- 1-1/8" WSP







MT Type IV Minimum Sizes – Walls

Exterior Walls for Type IV-A B C

CLT or Non-combustible

Exterior Walls for Type IV-HT

- CLT or FRTW or Non-combustible
- IBC 2018 6" Thick Wall (FTW or CLT)
- IBC 2021 4" Thick <u>CLT</u>





MT Type IV Minimum Sizes – Walls

MT Interior Walls in all Type IV:

- Laminated construction 4" thick
- Solid wood construction min. 2 layers of 1" matched boards

Other Interior Walls in Type IV A,B,C

Non-combustible (0 hr for nonbearing)

Other Interior Walls in Type IV HT

- Non-combustible (1 hr min)
- Wood stud wall (1 hr min)

Verify other code requirements for FRR (eg. interior bearing wall; occupancy separation)





Type IV-A Fire Resistance Ratings (FRR)

IV-A

FRR Examples:

Primary Structural Frame (Beam, Column, Bearing Wall):

3 HR Required

NC protection = at least 120 min

Use 3 layers of 5/8" type X Gypsum = 120 min (2 HR)
 Mass Timber FRR req'd = 3 HR - 2 HR = 1 HR





Type IV-A Fire Resistance Ratings (FRR)

IV-A

FRR Examples:

Floor Panels:

2 HR Required

NC Protection = at least 80 min

- Use 2 layers of 5/8" type X Gypsum = 80 min (1.33 HR), plus:
 - Mass Timber FRR req'd = 2 HR 1.33 HR = 0.67 HR,
 or
- Use 3 layers of 5/8" Type X Gypsum = 120 min (2 HR) and no FRR from MT req'd





Type IV-A Protection







Floor Surface Protection

Roof Construction Protection

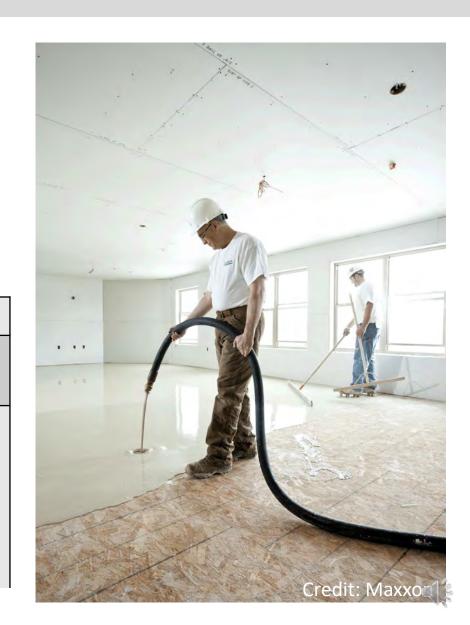
Ext Wall Protection

Min. 1 inch of NC protection

Min. 2 layers 5/8" type X gyp on inside face

Min. 1 layer 5/8" type X gyp on outside face

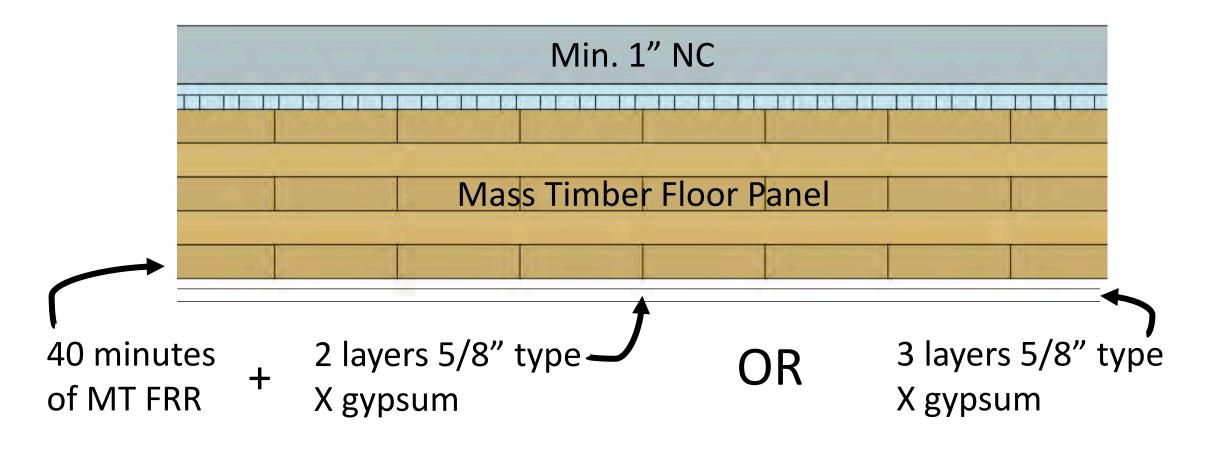
Min. 2 layers 5/8" type X gyp on inside face (non-brng) Min. 3 layers 5/8" type X gyp on inside face (brng)



Type IV-A Fire Resistance Ratings (FRR)



FRR & NC Floor Panel Example: 2 HR

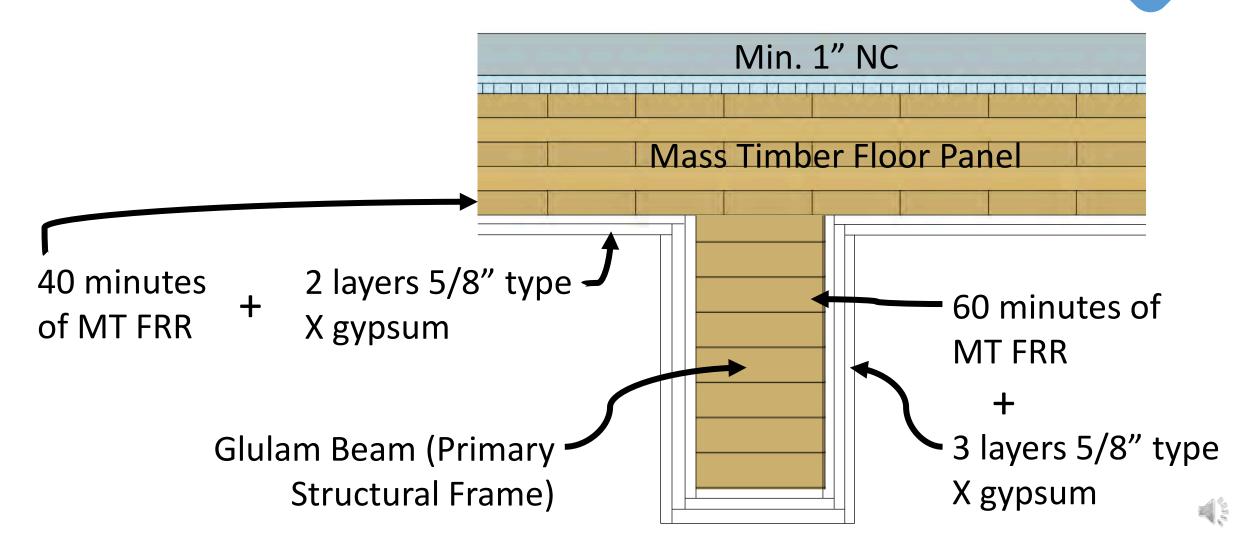




Type IV-A Fire Resistance Ratings (FRR)

IV-A

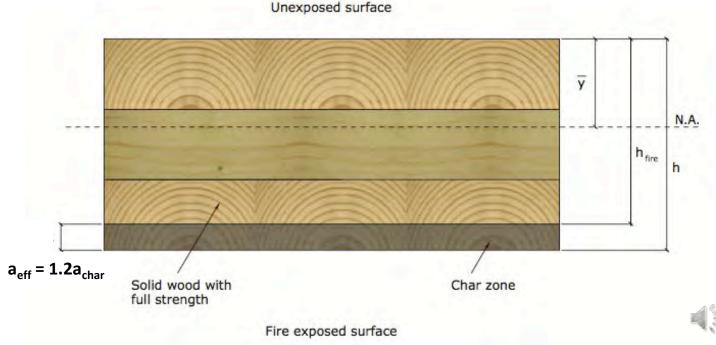
Primary Frame (3 HR) + Floor Panel Example (2 HR):



How do you determine FRR of MT?

- 2 Options:
- 1. Calculations in Accordance with IBC 722 → NDS Chapter 16
- 2. Tests in Accordance with ASTM E119





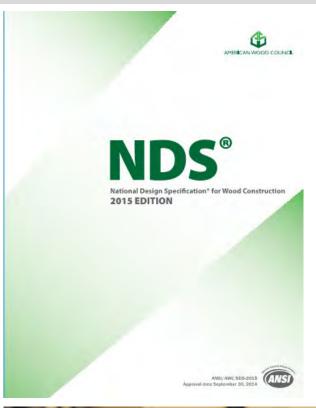
MT FRR Calculations Method:

- IBC 703.3 allows several methods of determining FRR. One is calculations per 722.
- 722.1 refers to NDS Chpt 16 for exposed wood FRR

703.3 Methods for determining fire resistance. The application of any of the methods listed in this section shall be based on the fire exposure and acceptance criteria specified in ASTM E119 or UL 263. The required *fire resistance* of a building element, component or assembly shall be permitted to be established by any of the following methods or procedures:

3. Calculations in accordance with Section 722.

722.1 General. The provisions of this section contain procedures by which the *fire resistance* of specific materials or combinations of materials is established by calculations. These procedures apply only to the information contained in this section and shall not be otherwise used. The calculated *fire resistance* of concrete, concrete masonry and clay masonry assemblies shall be permitted in accordance with ACI 216.1/TMS 0216. The calculated *fire resistance* of steel assemblies shall be permitted in accordance with Chapter 5 of ASCE 29. The calculated *fire resistance* of exposed wood members and wood decking shall be permitted in accordance with Chapter 16 of ANSI/AF&PA National Design Specification for Wood Construction (NDS).







NDS Chapter 16 includes calculation of fire resistance of NLT, CLT, Glulam, Solid Sawn and SCL wood products

Table 16.2.1B Effective Char Depths (for CLT with β_n =1.5in./hr.)

Required Fire Endurance (hr.)	Effective Char Depths, a _{char} (in.) lamination thicknesses, h _{lam} (in.)									
	5/8	3/4	7/8	1	1-1/4	1-3/8	1-1/2	1-3/4	2	
1-Hour	2.2	2.2	2.1	2.0	2.0	1.9	1.8	1.8	1.8	
1½-Hour	3.4	3.2	3.1	3.0	2.9	2.8	2.8	2.8	2.6	
2-Hour	4,4	4.3	4.1	4.0	3.9	3.8	3.6	3.6	3.6	

Nominal char rate of 1.5"/HR is recognized in NDS. Effective char depth calculated to account for duration, structural reduction in heat-affected zone



Table 16.2.1A Char Depth and Effective Char Depth (for $\beta_n = 1.5$ in./hr.)

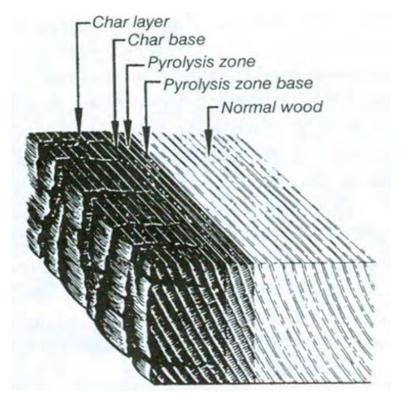
Required Fire Resistance (hr.)	Char Depth, a _{char} (in.)	Effective Char Depth, a _{eff} (in.)
1-Hour	1.5	1.8
1½-Hour	2.1	2.5
2-Hour	2.6	3.2

Table 16.2.1B Effective Char Depths (for CLT with β_n =1.5in./hr.)

Required Fire Endurance (hr.)	Effective Char Depths, a _{char} (in.) lamination thicknesses, h _{lam} (in.)									
	5/8	3/4	7/8	1	1-1/4	1-3/8	1-1/2	1-3/4	2	
1-Hour	2.2	2.2	2.1	2.0	2.0	1.9	1.8	1.8	1.8	
1½-Hour	3.4	3.2	3.1	3.0	2.9	2.8	2.8	2.8	2.6	
2-Hour	4,4	4.3	4.1	4.0	3.9	3.8	3.6	3.6	3.6	



Structural capacity check performed on remaining section, with stress increases



Credit: Forest Products Laboratory

Table 16.2.2 Adjustment Factors for Fire Design¹

				ASD					
			Design Stress to Member Strength Factor	Size Factor ²	Volume Factor 2	Flat Use Factor ²	Beam Stability Factor ³	Column Stability Factor 3	
Bending Strength	F_b	x	2.85	C_{F}	C_{V}	C_{fu}	C_L	-	
Beam Buckling Strength	F_{bE}	X	2.03	-	-	-	-	-	
Tensile Strength	\mathbf{F}_{t}	X	2.85	C_{F}	-	-	-	-	
Compressive Strength	F_c	X	2.58	C_{F}	-	-	-	C_P	
Column Buckling Strength	F_{cE}	X	2.03	-	-	-	-	-	

$$a_{char} = \beta_t t^{0.813}$$

Solid Sawn, Glulam, SCL

$$a_{char} = n_{lam} h_{lam} + \beta_t (t - (n_{lam} t_{gi}))^{0.813}$$

CLT

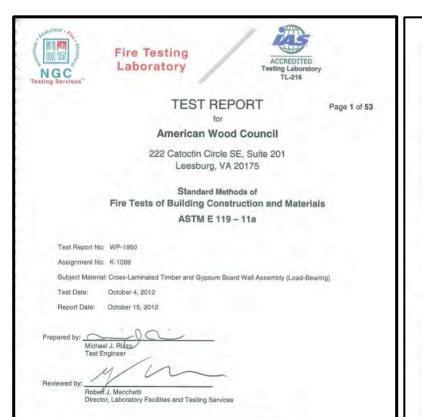
$$a_{eff} = 1.2a_{char}$$

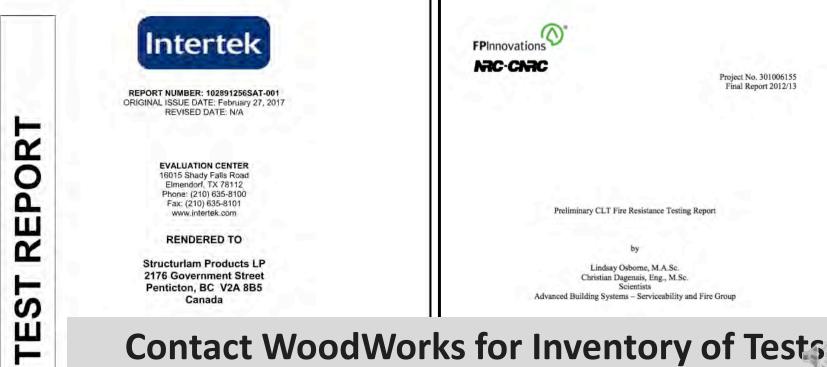
Effective Char Depth

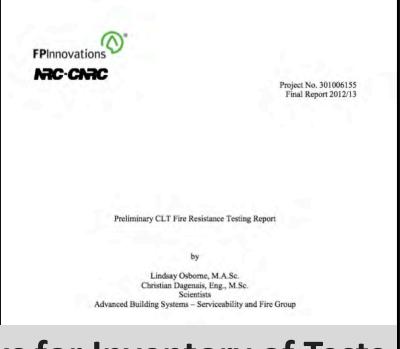


Tested Assemblies Method:

Many successful Mass Timber ASTM E119 fire tests have been completed by industry & manufacturers









Fire-Resistive Design of Mass Timber Members

Code Applications, Construction Types and Fire Ratings

Richard McLain, PE, SE • Senior Technical Director • WoodWorks Scott Breneman, PhD, PE SE • Senior Technical Director • WoodWorks

For many years, exposed heavy timber framing elements have been permitted in U.S. buildings due to their inherent fire-resistance properties. The predictability of wood's char rate has been well-established for decades and has long been recognized in building codes and standards.

Today, one of the exciting trends in building design is the growing use of mass timber—i.e., large solid wood panel products such as cross-laminated timber (CLT) and naillaminated timber (NLT)—for floor, wall and roof construction. Like heavy timber, mass timber products have inherent fire resistance that allows them to be left exposed and still achieve a fire-resistance rating. Because of their strength and dimensional stability, these products also offer a low-carbon alternative to steel, concrete, and masonry for many applications. It is this combination of exposed structure and strength that developers and designers across the country



Kaiser Group | Path Architecture

Munzing Structural Engineering

are leveraging to create innovative designs with a warm yet modern aesthetic, often for projects that go beyond traditional norms of wood design.

This paper has been written to support architects and engineers exploring the use of mass timber for commercial and multi-family construction. It focuses on how to meet fire-resistance requirements in the International Building Code (IBC), including calculation and testing-based methods. Unless otherwise noted, references refer to the 2018 IBC.

Mass Timber & Construction Type

Before demonstrating fire-resistance ratings of exposed mass timber elements, it's important to understand under what circumstances the code currently allows the use of mass timber in commercial and multi-family construction.

A building's assigned construction type is the main indicator of where and when all wood systems can be used. IBC Section 602 defines five main options (Type I through V) with all but Type IV having subcategories A and B. Types III and V permit the use of wood framing throughout much of the structure and both are used extensively for modern mass timber buildings.

Type III (IBC 602.3) – Timber elements can be used in floors, roofs and interior walls. Fire-retardant-treated wood (ERTW) framing is permitted in exterior walls with a fireresistance rating of 2 hours or less.

Type V (IBC 602.5) – Timber elements can be used throughout the structure, including floors, roofs and both interior and exterior walls

Type IV (IBC 602.4) - Commonly referred to as 'Heavy Timber' construction, this option

Mass Timber Fire Design Resource

- Code compliance options for demonstrating FRR
- Updated as new tests are completed
- Free download at woodworks.org



MT Fire Resistance Ratings (FRR)

Inventory of Fire Tested MT Assemblies

Table 1: North American Fire Resistance Tests of Mass Timber Floor / Roof Assemblies



CLT Panel	Manufacturer	CLT Grade or Major x Minor Grade	Ceiling Protection	Panel Connection in Test	Floor Topping	Load Rating	Fire Resistance Achieved (Hours)	Source	Testing Lab
3-ply CLT 14-mm - 1-488 in)	Nordic	SPF 1650 Fb 1.3 EMSR 3 SPF #3	2 layers 1/2" Type X gypsum	Half-Lap	None	Reduced 36% Moment Capacity	- u = 1	j (Test'i)	NRC Fire Laboratory
3-ply CLT 105mm 4.153 in)	Structurlam	SPF #1/#2 # SPF #1/#2	1 layer 5/8" Type Xgypsum	flaff-Lap	None	Reduced 7.5% Mannest Capacity	-1	1 (Test 3)	NRC Fire Laboratory
5-ply CLT (173mm#.875*)	Nordir	El	None	Topside Spline	2 staggered layers of 1/2" coment boards	Londed. See Manufacturer	2	2	NRC Fire Laboratory March 2016
5-ply CLT (175mm6-875*)	Nordic	E	1 layer of \$5/K" Type Xgypsum under 2- channels and furning strips with 3.5/8" (then layer barts)	Topside Spline	2 stagg and layers of 1/2" cament bounds	Loaded. See Manufacturer	1	5	NRC Fire Laboratory Nov 2014
5-ply CLT (175mm6.875*)	Nordie	El	None	Topside Spline	3/4 in proprietary gyperere over Maxxon amount ical mat	Roduced 54% Mament Capacity	(.5	В	UL
5-ply CLT (175mm6.875*)	Nordic	Ei	l layer 5/8" normal gypsum	Topside Spline	3/4 (a. proprietary gyperete over Maxxon acoustical mat or proprietary sound board	Rod acod 50% Mament Capacity	<u> </u>	-40	UL
5-ply-CLT (175mm6.875*)	Nordie	El	Likyer 50° Tyge X Gyn ander Resilien (Channel ander 7.70° Litora win3 1/2° Mineral Woo) feween hists	Half-Lap	None	Loaded. See Mamifacturer	2	21	Interiek 8/24/2012
5-ply CLT (175mm6-875*)	Structurlan	EI M5 MSR 2100 A SPF #2	None	Tops ide Spline	1-1/2" Maxxon Cyp-Grete 2000 over Maxxon Bounforcing Mesh	Loaded. See Manufacturer	2.5	6	Intertek, 2/22/2016
5-ply CLT (175mm6.875°)	DR Johnson	VI	No ne	Helf-Lap & Tops ide Spline	2 ⁶ gypsumtopping	Luaded. See Manufacturer	2	7	SwRI (May 2016)
5-ply CLT (175mm6.875*)	Nordic	SPF 1950 Fb MSR a SPF #3	None	Half-Lap	None	Reduced 59% Moment Capacity	(3	1 (Test-1)	NRC Fire Laboratory
5-ply CLT (175mm6.875°)	Structurlam	SPF #1/#2 # SPF #1/#2	1 layer 5/K° Type Xgypsum	Half-Lap	Nonz	Unreduced 101% Moment Capacity	2	1 (Ted 6)	NRC Fire Laboratory
7-ply CLT (245mm 9:65°)	Structurlam	SPF #1/#2 # SPF #1/#2	None	fielf-lap	None	Unreduced 101% Moment Capacity	2.3	1 (Teit 7)	NRC Fire Laboratory
5-ply CLT (175mm#.875*)	SmartLam	SL-V4	None	fialf-lay	nominal 1/2" ply wood with 8d nails.	Loaded. Say Manufacturer	1	12 (Test 4)	Western Fire Center 10/26/2016
5-ply CLT (175mm6.875*)	SmartLaw	Vi	No ne	Half-Lap	nominal 1/2* ply wood with #d nails.	Loaded See Manufacturer	2:	(2 (Test 5)	Western Fire Center 10/28/2016
5-ply CLT (175mm6 875°)	DR Johnson	VI.	None	Half-Lap	nominal 1/2"plywoodwith #damis.	Lorded. See Mamifacturer	2	(2(Test 6)	Western Fire Center 11/01/2016
5-ply CLT	кин	CVSMI	None	Half-Lap &	None	Lizade d.	1	18	SwRI



Materials Permitted

602.4 Type IV. Type IV construction is that type of construction in which the building elements are mass timber or noncombustible materials and have fire resistance ratings in accordance with Table 601. Mass timber elements shall meet the fire resistance rating requirements of this section based on either the fire resistance rating of the noncombustible protection, the mass timber, or a combination of both and shall be determined in accordance with Section 703.2 or 703.3. The minimum dimensions and permitted materials for building elements shall comply with the provisions of this section and Section 2304.11. Mass timber

Exterior load-bearing walls and nonload-bearing walls shall be mass timber construction, or shall be of noncombustible construction.

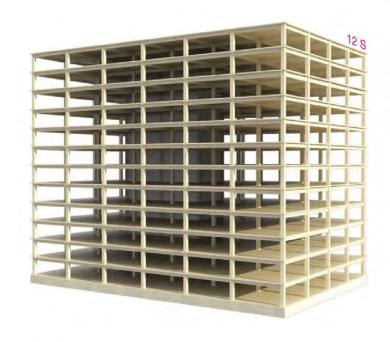
Exception:Type IV-HT Construction in accordance with Section 602.4.4.

The interior building elements, including nonload-bearing walls and partitions, shall be of mass timber construction or of noncombustible construction.

Exception: Type IV-HT Construction in accordance with Section 602.4.4...



Type IV-B



12 STORIES
BUILDING HEIGHT 180 FT
ALLOWABLE BUILDING AREA 648,000 SF
AVERAGE AREA PER STORY 54,000SF

TYPE IV-B









Credit: Susan Jones, atelierjones

IV-B



12 STORIES BUILDING HEIGHT ALLOWABLE BUILDING AREA AVERAGE AREA PER STORY

180 FT 648,000 SF 54,000SF

TYPE IV-B

Credit: Susan Jones, atelierjones

Type IV-B Height and Area Limits

Occupancy	# of Stories	Height	Area per Story	Building Area
A-2	12	180 ft	90,000 SF	270,000 SF
В	12	180 ft	216,000 SF	648,000 SF
M	8	180 ft	123,000 SF	369,000 SF
R-2	12	180 ft	123,000 SF	369,000 SF

Areas exclude potential frontage increase

In most cases, Type IV-B height & story allowances = Type I-B height & story allowances

Type IV-B area = 2 * Type IV-HT area



Credit: Kaiser+Path

IV-B

Type IV-B Protection vs. Exposed



12 STORIES
BUILDING HEIGHT 180 FT
ALLOWABLE BUILDING AREA 648,000 SF
AVERAGE AREA PER STORY 54,000SF

TYPE IV-B

Credit: Susan Jones, atelierjones





NC protection on all surfaces of Mass Timber except limited exposed areas

~20% of Ceiling or ~40% of Wall can be exposed



Type IV-B Fire Resistance Ratings (FRR)

IV-B





Primary Frame FRR

Ext or Int Bearing Wall FRR

Floor Construction FRR

Roof Construction FRR

2 HR (1 HR at Roof)

2 HR

2 HR

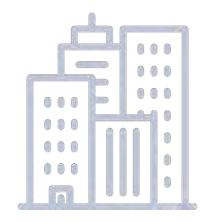
1 HR



Type IV-B Fire Resistance Ratings (FRR)

IV-B





*Applicable to most locations. Limited exposed MT permitted

FRR	Min. NC Protection		
2 HR (1 HR at Roof)	80 min* (40 min* at Roof)		
2 HR	80 min*		
2 HR	80 min*		
1 HR	40 min*		

Primary Frame FRR

Ext or Int Bearing Wall FRR

Floor Construction FRR

Roof Construction FRR

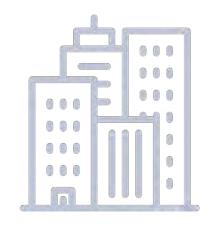
1/2" Type X Gypsum = 25 min

5/8" Type X Gypsum = 40 min



Type IV-B Protection







Floor Surface Protection

Roof Construction Protection

Ext Wall Protection

Min. 1 inch of NC protection

Min. 1 layer 5/8" type X gyp on inside face*

Min. 1 layer 5/8" type X gyp on outside face

Min. 2 layers 5/8" type X gyp on inside face*

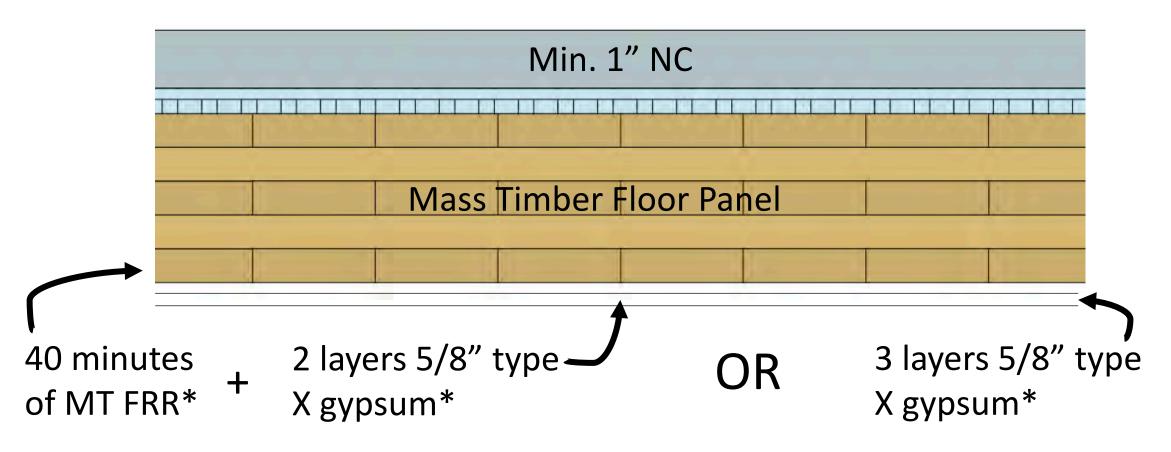
*Applicable to most locations Limited exposed MT permitted



Type IV-B Fire Resistance Ratings (FRR)

IV-B

FRR & NC Floor Panel Example: 2 HR



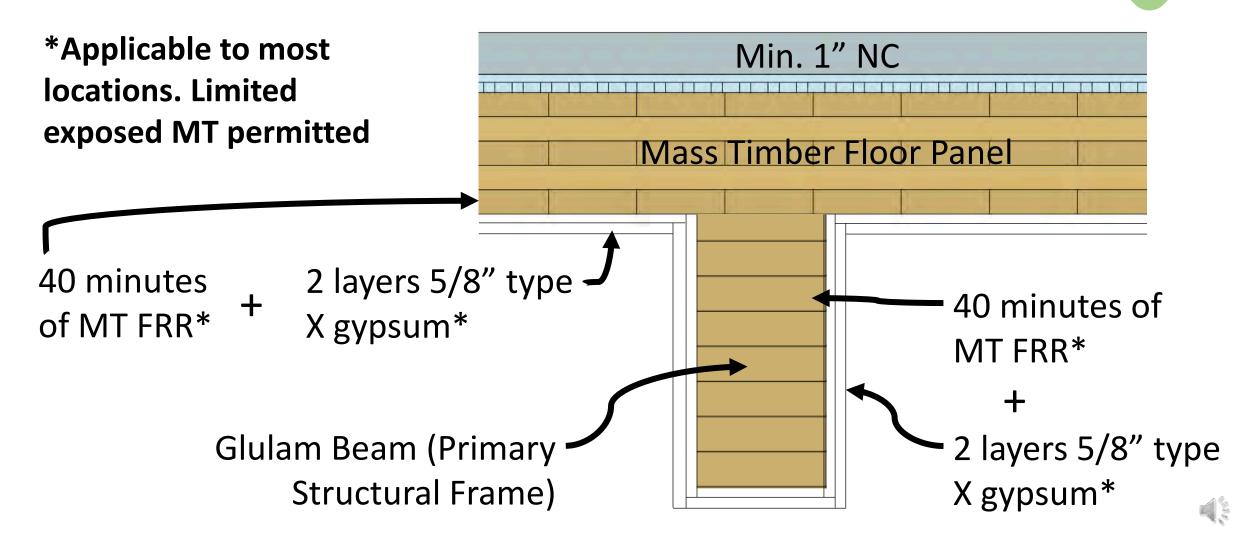
^{*}Applicable to most locations. Limited exposed MT permitted



Type IV-B Fire Resistance Ratings (FRR)

IV-B

Primary Frame (2 HR) + Floor Panel Example (2 HR):



IV-B

Limited Exposed MT allowed in Type IV-B for:

- MT beams and columns which are not integral part of walls or ceilings, no area limitation applies
- MT ceilings and beams up to 20% of floor area in dwelling unit or fire area, <u>or</u>
- MT walls and columns up to 40% of floor area in dwelling unit or fire area, or
- Combination of ceilings/beams and walls/columns, calculated as follows:



Credit: Kaiser+Path

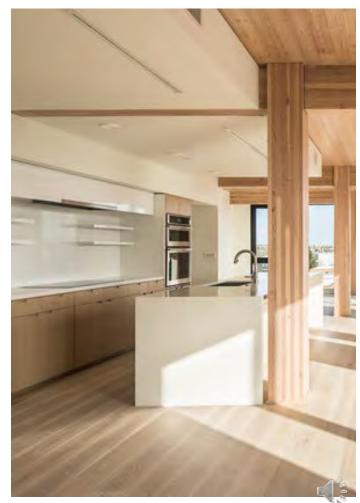
IV-B

Mixed unprotected areas, exposing both ceilings and walls:

In each dwelling unit or fire area, max.
 unprotected area =

$$(U_{tc}/U_{ac}) + (U_{tw}/U_{aw}) \le 1.0$$

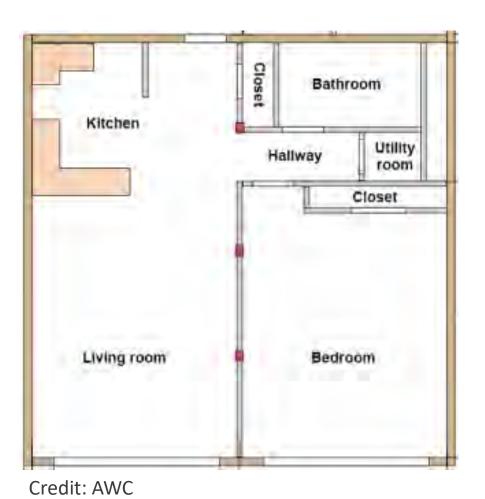
- U_{tc} = Total unprotected MT ceiling areas
- U_{ac} = Allowable unprotected MT ceiling areas
- U_{tw} = Total unprotected MT wall areas
- U_{aw} = Allowable unprotected MT wall areas



Credit: Kaiser+Path



Design Example: Mixing unprotected MT walls & ceilings



800 SF dwelling unit

- $U_{ac} = (800 \text{ SF})*(0.20) = 160 \text{ SF}$
- $U_{aw} = (800 \text{ SF})*(0.40) = 320 \text{ SF}$
- Could expose 160 SF of MT ceiling,
 OR 320 SF of MT Wall, OR
- If desire to expose 100 SF of MT ceiling in Living Room, determine max. area of MT walls that can be exposed





Design Example: Mixing unprotected MT walls & ceilings



$$(U_{tc}/U_{ac}) + (U_{tw}/U_{aw}) \le 1.0$$

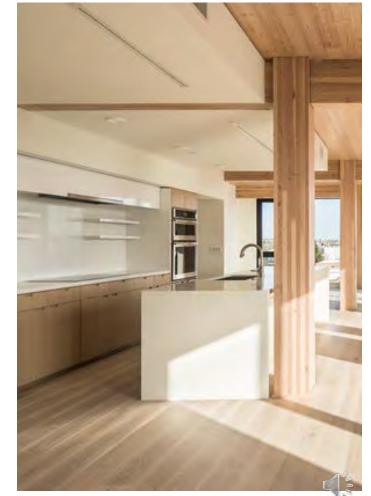
(100/160) + $(U_{tw}/320) \le 1.0$
 $U_{tw} = 120 \text{ SF}$

 Can expose 120 SF of MT walls in dwelling unit in combination with exposing 100 SF of MT ceiling

Credit: AWC

Horizontal separation of unprotected areas:

 Unprotected portions of mass timber walls and ceilings shall be not less than 15 feet from unprotected portions of other walls and ceilings, measured horizontally along the ceiling and from other unprotected portions of walls measured horizontally along the floor.



Credit: Kaiser+Path

Type IV-C



9 STORIES
BUILDING HEIGHT 85'
ALLOWABLE BUILDING AREA
AVERAGE AREA PER STORY 45,000 SF

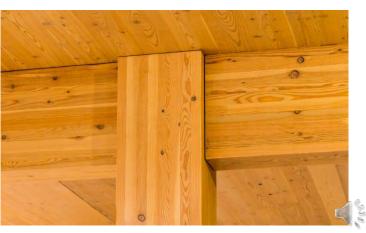
TYPE IV-C



Photos: Baumberger Studio/PATH Architecture/Marcus Kauffman







Credit: Susan Jones, atelierjones

IV-C



9 STORIES
BUILDING HEIGHT 85
ALLOWABLE BUILDING AREA
AVERAGE AREA PER STORY 45

AREA 405,000 SF ORY 45,000 SF

TYPE IV-C

Credit: Susan Jones, atelierjones

Type IV-C Height and Area Limits

Occupancy	# of Stories	Height	Area per Story	Building Area
A-2	6	85 ft	56,250 SF	168,750 SF
В	9	85 ft	135,000 SF	405,000 SF
M	6	85 ft	76,875 SF	230,625 SF
R-2	8	85 ft	76,875 SF	230,625 SF

Areas exclude potential frontage increase

In most cases, Type IV-C height allowances = Type IV-HT height allowances, but add'l stories permitted due to enhanced FRR

Type IV-C area = 1.25 * Type IV-HT area



IV-C

Type IV-C Protection vs. Exposed



9 STORIES
BUILDING HEIGHT 85'
ALLOWABLE BUILDING AREA 405,000 SF
AVERAGE AREA PER STORY 45.000 SF

TYPE IV-C

Credit: Susan Jones, atelierjones





All Mass Timber surfaces may be exposed

Exceptions: Shafts, concealed spaces, outside face of exterior walls



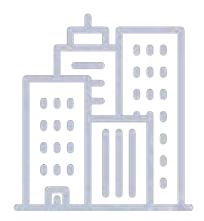
Ema Peter

Credit: Kaiser+Path,

Type IV-C Fire Resistance Ratings (FRR)

IV-C





Primary Frame FRR

Ext or Int Bearing Wall FRR

Floor Construction FRR

Roof Construction FRR

2 HR (1 HR at Roof)

2 HR

2 HR

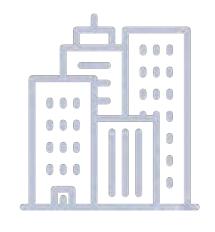
1 HR

2 Hour Floor 2 Hour Frame 2 Hour Floor

Same FRR as IV-B, but all MT in IV-C may be exposed*

Type IV-C Protection







Floor Surface Protection

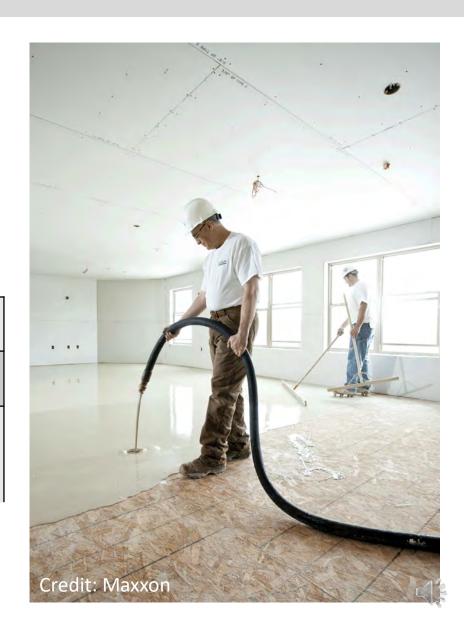
Roof Construction Protection

Ext Wall Protection

None req'd

None req'd

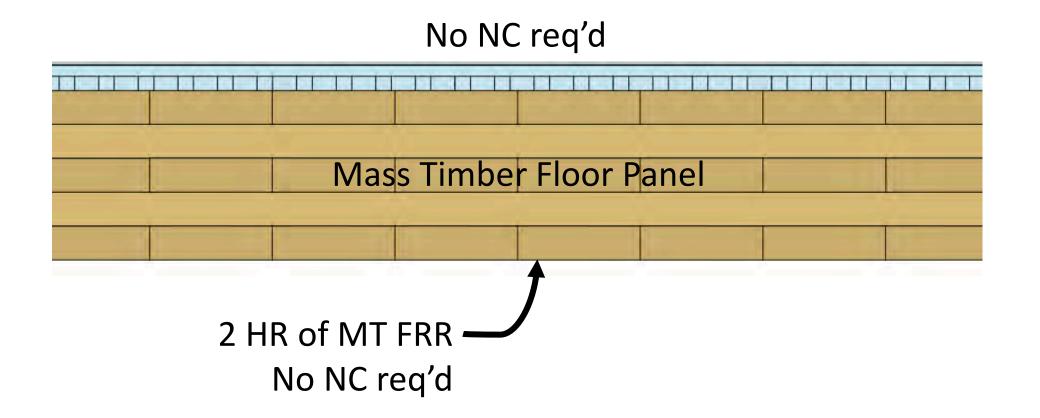
Min. 1 layer 5/8" type X gyp on outside face None req'd on inside face



Type IV-C Fire Resistance Ratings (FRR)

IV-C

FRR & NC Floor Panel Example: 2 HR

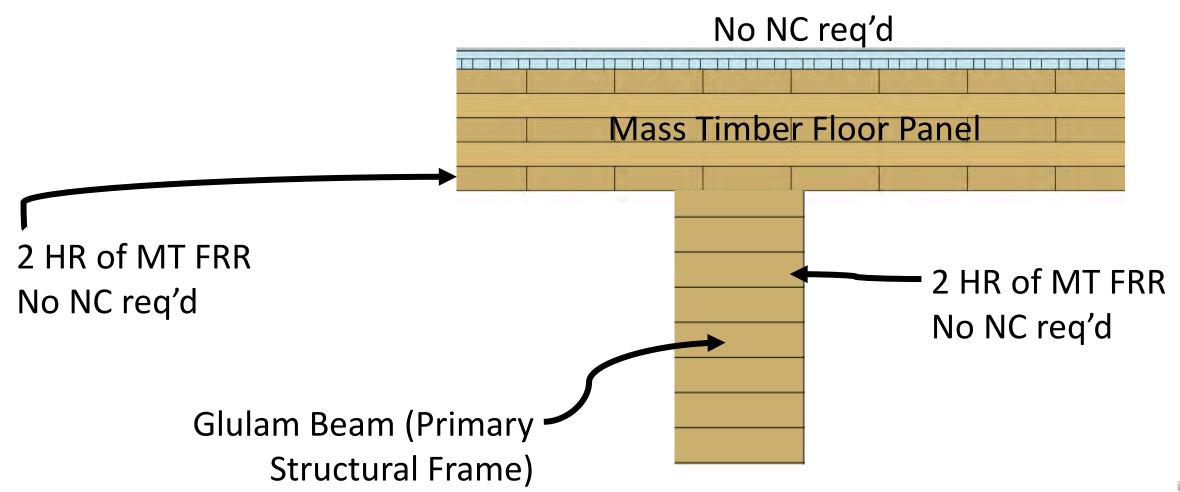




Type IV-C Fire Resistance Ratings (FRR)

IV-C

Primary Frame (2 HR) + Floor Panel Example (2 HR):





Fire Resistance Ratings (FRR) Recap













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11001	\sim	13616	

Primary Frame @ Roof

Floor Construction

Primary Frame

Exterior Bearing Walls

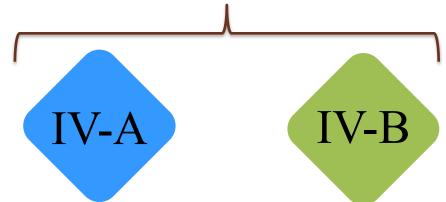
Interior Bearing Walls

1.5	1	1	нт
2	1	1	нт
2	2	2	нт
3	2	2	нт
3	2	2	2
3	2	2	1 or HT



Noncombustible Protection (NC) Recap

Noncombustible Protection Required















Credit: LEVER Architecture





Interior Wall Construction Recap



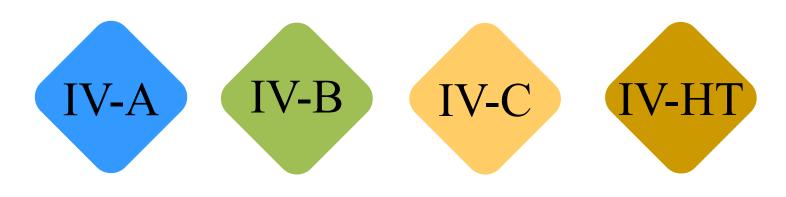
Fire Rating (bearing wall)

Construction – MT

NC Protection

Noncombustible non-bearing wall

Wood Stud Wall

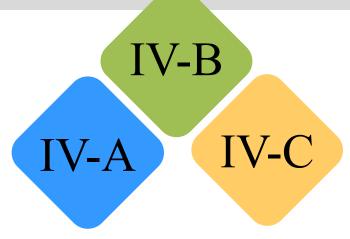


3 Hr	2 Hr	2 Hr	1 Hr or HT*			
Laminated construction 4" thick (CLT, NLT, etc) Solid wood construction min. 2 layers of 1" matched boards						
Per Interior Requirements No						
	1 Hr					
	1 Hr					



Exterior Wall Construction Recap







IBC 2018

Fire Rating (bearing wall)

Mass Timber

Exterior NC Protection

Interior NC Protection

Light Frame FRTW

3 Hr	2 Hr	2 Hr	2 Hr	2Hr	
Mass Timber/CLT			4" min thick <u>CLT</u> * 6" <u>Wall</u> *		
40 Min NC & No Exterior Combustible Coverings			FRT Sheathing, Gyp or other NC		
Per Interior Requirements			Not Required		
No			Yes* 6" Wall*		

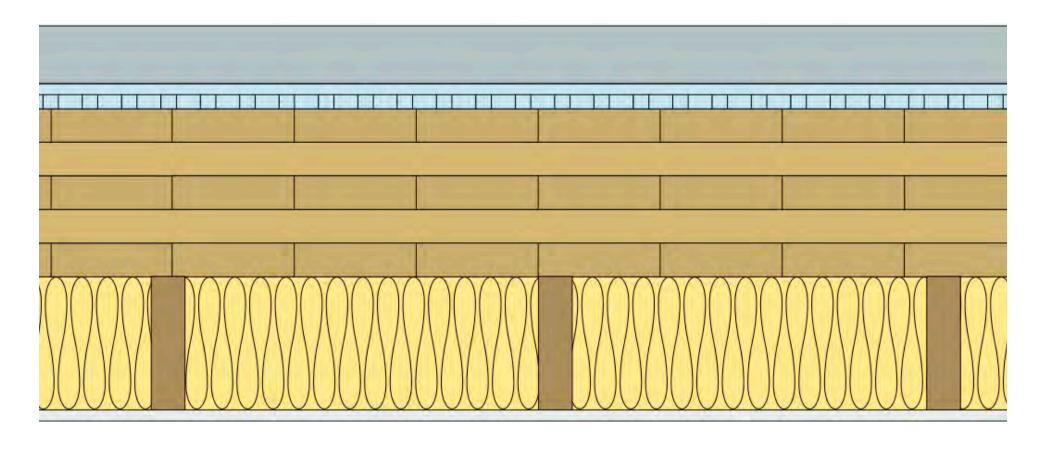
IBC 2021



Concealed Spaces in Type IV

What if I have a dropped ceiling? Can I have a dropped ceiling?

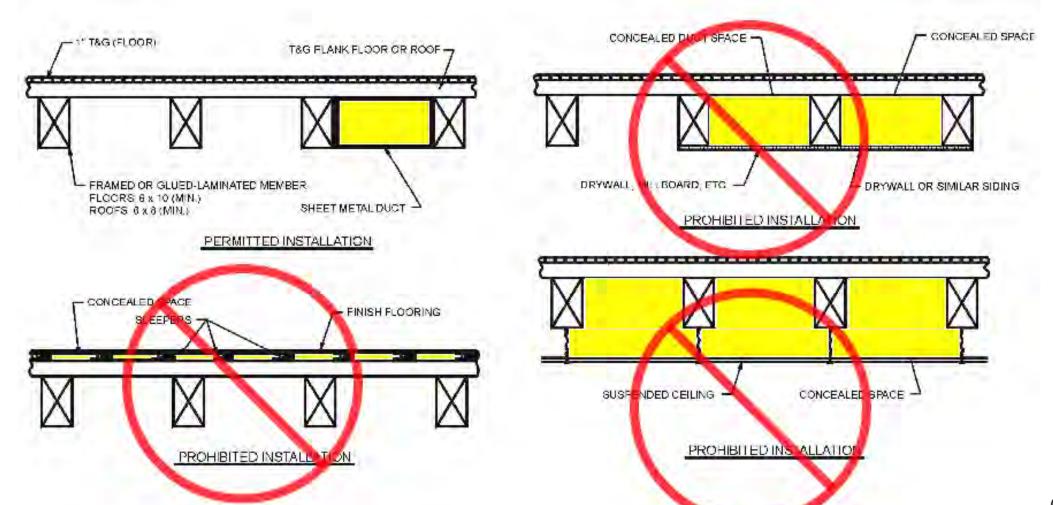
Impact on FRR, NC placement, sprinkler requirements

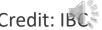




Concealed Spaces in Type IV

Previous Type IV (now IV-HT) provisions prohibited concealed spaces





Concealed Spaces in Type IV

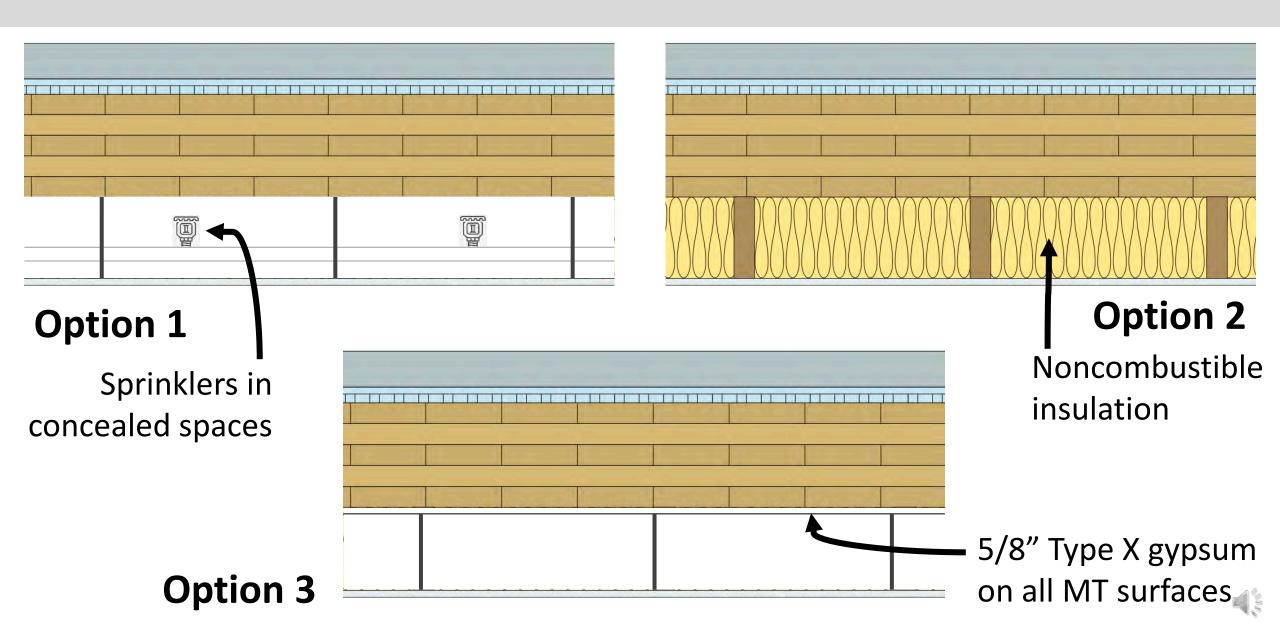
Type IV-HT (IBC 2021) permits concealed spaces where one of the following conditions exists:

- 1. The building is sprinklered throughout with an NFPA 13 Sprinkler and automatic sprinklers are provided in the concealed space.
- 2. The concealed space is completely filled with noncombustible insulation.
- 3. Surfaces within the concealed space are fully sheathed with not less than 5/8" Type X gypsum.

Concealed spaces within interior walls and partitions with a one hour or greater fire resistance rating complying Section 2304.11.2.2 do not require additional protection.



Concealed Spaces in Type IV-HT



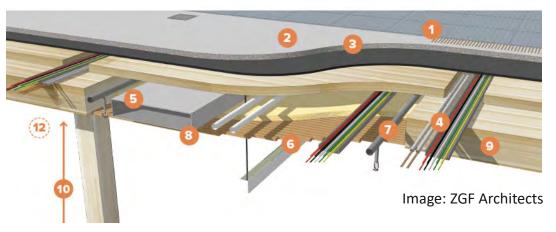
Concealed Spaces in Type IV-A, IV-B, IV-C

New IV-HT concealed space provisions do not apply to IV-A, IV-B or IV-C

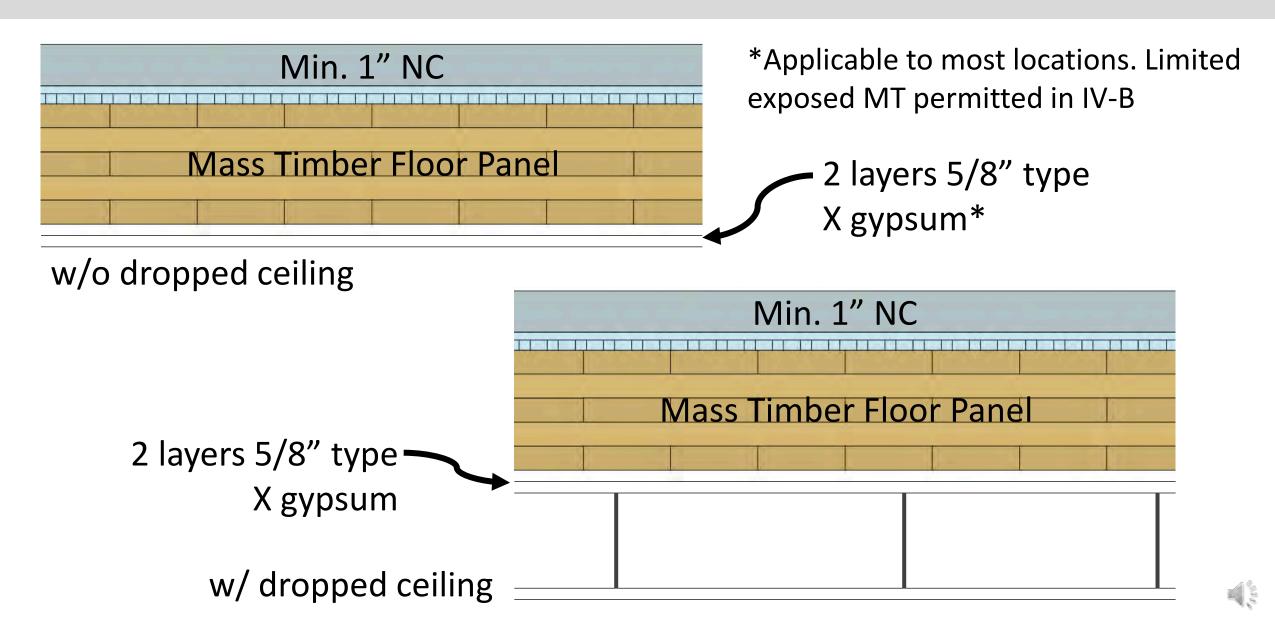
But, can still have concealed spaces in IV-A, IV-B, IV-C:

- IV-A and IV-B: Combustible construction forming concealed spaces protected with NC of 80 minutes (2 layers of 5/8" Type X Gypsum)
- IV-C: Combustible construction forming concealed spaces protected with NC of 40 minutes (1 layer of 5/8" Type X Gypsum)

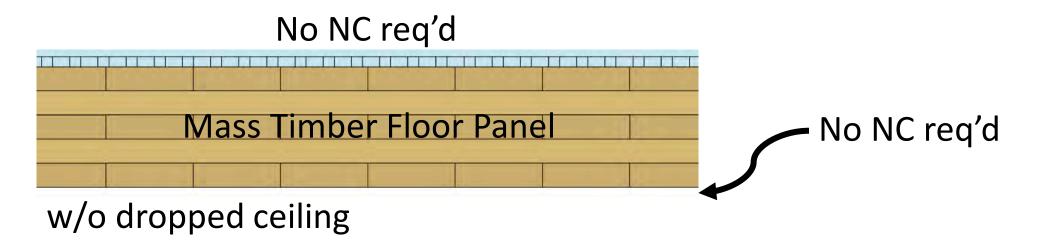


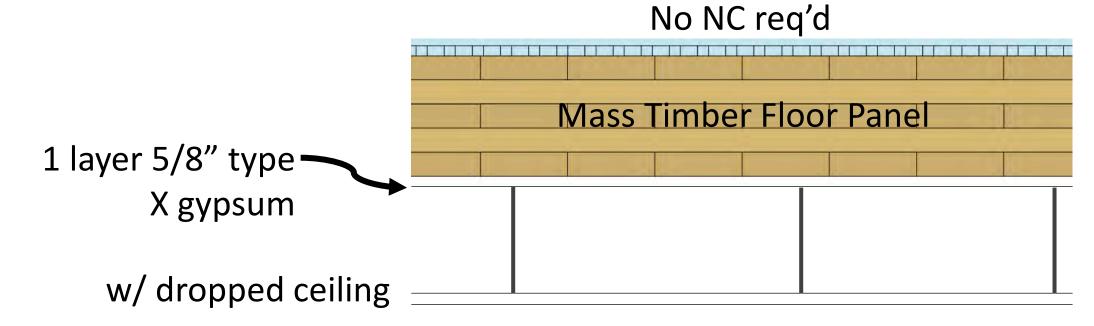


Concealed Spaces in Type IV-A, IV-B



Concealed Spaces in Type IV-C







Tall Wood Shaft Enclosures

- When can shaft enclosures be MT?
- What FRR requirements exist?
- If shaft enclosure is MT, is NC req'd?



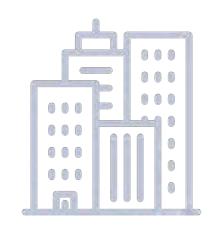






Tall Wood Shaft Enclosures





Exit & Hoistway Enclosures

E&H Enclosures FRR







ft: MT protected with 2 layers 5/8" type X gyp (if 2 HR req'd) or 3 layers 5/8" type X gyp (if 3 HR req'd) both sides

Above 12 Stories or 180 ft: Noncombustible shafts (IBC 2021 602.4)

NC or MT protected with 2 layers 5/8" type X gyp (IBC 2021 602.4.2.6) both sides

NC or MT protected with 1 layer 5/8" type X gyp (IBC 602.4.3.6) both sides

2 HR (not less than FRR of floor assembly penetrated, IBC 713.4)





DOES TALL WOOD = HIGH RISE?

Mid-Rise vs. High-Rise

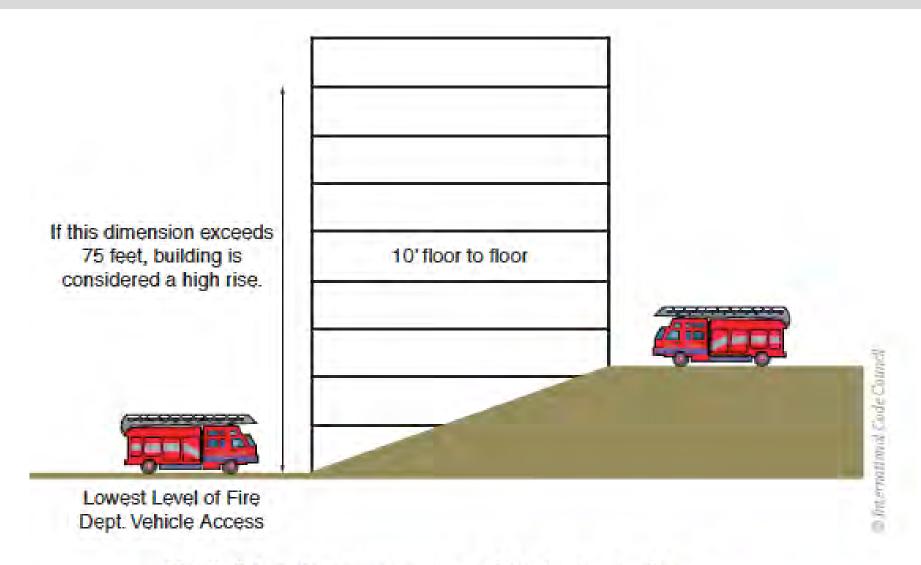


FIGURE 6-6 Determination of high-rise building





- Two Water Mains Required if:
 - Building Height Exceeds 420 ft, or
 - Type IV-A and IV-B buildings that exceed 120 ft in height





CLT Fire Performance – Char Fall Off

CLT char fall off or heat induced delamination occurs when laminations (or pieces thereof) fall off the underside of a CLT panel under extended fire conditions.







CLT Fire Performance – Fire Re-Growth

In tall buildings, preventing fire re-growth is key.

Fire re-growth is a phenomenon in which the heat-release rate of a fire intensifies following a decay phase. Fire re-growth can be initiated when delamination occurs, as this exposes un-charred wood surfaces, thereby resulting in an influx of fuel available for consumption by the fire.







CLT Fire Performance – Char Fall Off

Facts about CLT char fall off:

- Only an item to consider in tall buildings. Important to avoid in high-rise construction where required performance is containment of fire within compartment of origin with no sprinkler or fire service suppression
- Not applicable when discussing mid-rise mass timber (or any building under types II, III, IV-HT or V)
- Largely a function of adhesive performance under high temps
- Has been addressed in PRG 320-18 (required for all CLT under 2021 IBC, not just tall wood)

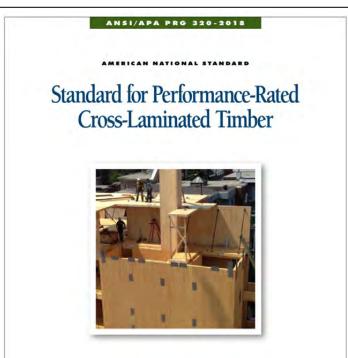


CLT Fire Performance – PRG 320

2021 IBC Section 602.4 added:

Cross-laminated timber shall be labeled as conforming to PRG 320 - 18 as referenced in Section 2303.1.4.







CLT Fire Performance – PRG 320

PRG 320 is manufacturing & performance standard for CLT.

2018 edition (referenced in 2021 IBC) added new elevated temperature adhesive performance requirements validated by full-scale and medium-scale qualification testing to ensure CLT does not exhibit fire re-growth

When designing tall wood – specify CLT per PRG 320-18 (req'd in IBC 2021 for all CLT)

ANSI/APA PRG 320-2018

Standard for Performance-Rated Cross-Laminated Timber



ANNEX B. PRACTICE FOR EVALUATING ELEVATED TEMPERATURE PERFORMANCE OF ADHESIVES USED IN CROSS-LAMINATED TIMBER (MANDATORY)





In Construction Types IV-A, IV-B & IV-C, building elements are required to be FRR as specified in IBC Tables 601 and 602. Connections between these building elements must be able to maintain FRR no less than that required of the connected members.





Wood connections, including connectors, fasteners, and portions of wood members included in the connection design, shall be protected from fire exposure for the required fire resistance time. Protection shall be provided by wood, fire-rated gypsum board, other approved materials, or a combination thereof.

Source: NDS

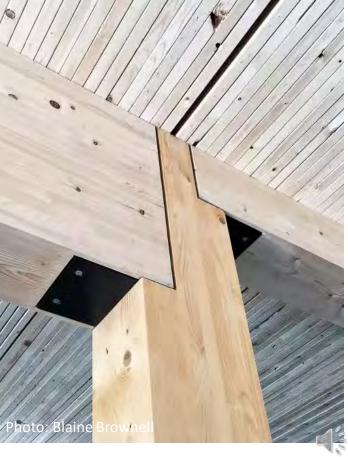


Many ways to demonstrate connection fire protection: calculations, prescriptive NC, test results, others as approved by AHJ









2017 Glulam Beam to Column Connection Fire Tests under standard ASTM E119 time-temperature exposure







Fire Test Results

Test	Beam	Connector	Applied Load	FRR	
1	8.75" x 18" (222mm x 457mm)	1 x Ricon S VS 290x80	3,905lbs (17.4kN)	1hr	
2	10.75" x 24" (273mm x 610mm)	Staggered double Ricon S VS 200x80	16,620lbs (73.9kN)	1.5hrs	
3	10.75" x 24" (273mm x 610mm)	1 x Megant 430	16,620lbs (73.9kN)	1.5hrs	



Softwood Lumber Board

Glulam Connection Fire Test Summary Report

Issue | June 5, 2017

Full Report Available at:

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CHEMISTRY AND CHEMICAL ENGINEERING DIVISION



(LDI)

FIRE PERFORMANCE EVALUATION OF A LOAD BEARING GLULAM BEAM TO COLUMN CONNECTION, INCLUDING A CLT PANEL, TESTED IN GENERAL ACCORDANCE WITH ASTM E119-16a, STANDARD TEST METHODS FOR FIRE TESTS OF BUILDING CONSTRUCTION AND MATERIALS

FINAL REPORT Consisting of 32 Pages

https://www.thinkwood.com/wp-content/uploads/2018/01/reThink-Wood-Arup-SLB-Connection-Fire-Testing-Summary-web.pdf





PENETRATIONS IN TALL WOOD

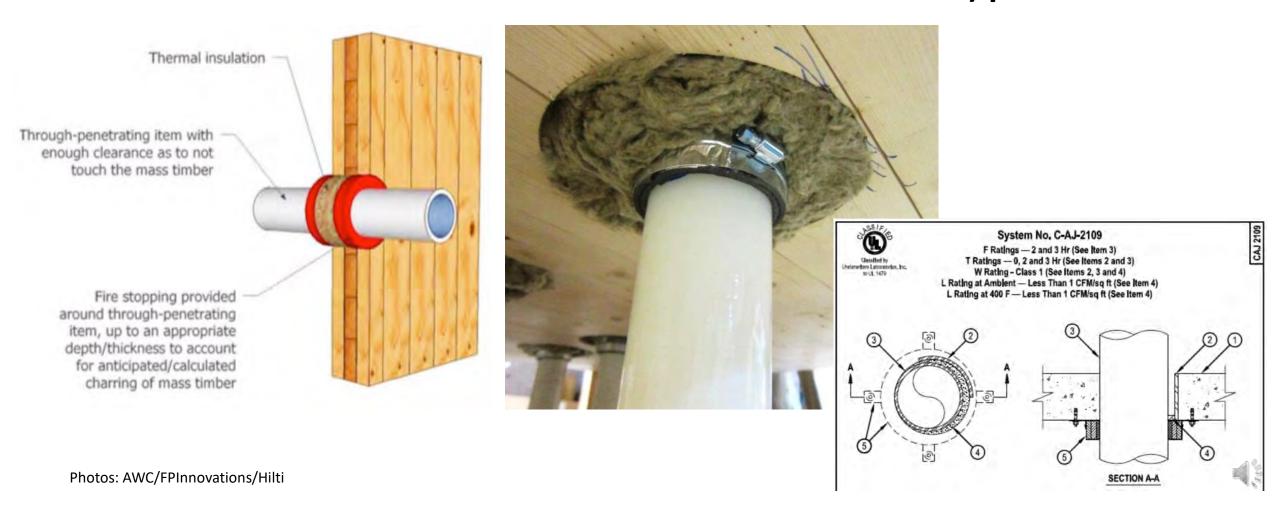
Although not a new code requirement or specific to tall wood, more testing & information is becoming available on firestopping of penetrations through MT assemblies







Most firestopping systems include combination of fire safing (eg. noncombustible materials such as mineral wool insulation) plus fire caulk



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CHEMISTRY AND CHEMICAL ENGINEERING DIVISION

FIRE TECHNOLOGY DEPARTMENT WWW.FIRE.SWRI.ORG FAX (210) 522-3377



Firestop systems tests on Mass Timber Contact WoodWorks for information

FIRE RESISTANCE PERFORMANCE EVALUATION OF A PENETRATION FIRESTOP SYSTEM TESTED IN ACCORDANCE WITH ASTM E814-13A, STANDARD TEST METHOD FOR FIRE TESTS OF PENETRATION FIRESTOP SYSTEMS

FINAL REPORT Consisting of 18 Pages

SwRI® Project No. 01.21428.01.001a Test Date: September 30, 2015 Report Date: October 22, 2015

Prepared for:

American Wood Council 222 Catoctin Circle SE Leesburg, VA 20175 FIRE PERFORMANCE OF FIRESTOPS, PENETRATIONS, AND FIRE DOORS IN MASS TIMBER ASSEMBLIES

Lindsay Ranger 1, Christian Dagenais 1, Conroy Lum1, Tony Thomas 1

ABSTRACT: Integrity and continuity must be maintained for fire separations required to provide fit prevent passage of hot gases or increased temperature on the unexposed side. Vulnerable locations, when are introduced into mass timber systems, are susceptible to fire spread. Service and closure penetrat timber fire separation have been investigated. Many of the fire stop systems were able to achieve I-½ accordance with CAN/ULC-S115, which would be required for 2-hr fire resistance rated assemblies, su tall wood buildings. Construction details are outlined which ensure adequate fire performance of these penetrations.

KEYWORDS: Firestop, through-penetrations, fire rated door, mass timber, cross-laminated tim buildings, fire resistance

1 INTRODUCTION

Many tall wood buildings using mass timber are planned or are currently being designed for construction around the world. A few have been built in Canada, including an 18 storey cross-laminated timber (CLT) and glulam building in British Columbia. The prescriptive requirements in the National Building Code of Canada (NBCC) [1] do not (yet) permit the construction of wood buildings taller than six stories, however an alternative

construction, as well as in several alter building designs.

Although the general fire performance of well documented, there are still sever warrant further investigation to ensure safety levels are met and a number available for designers to use. Generating generic assemblies will reduce the need I completed on an individual construction



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FIRESTOPPING TEST WITNESS REPORT

for

NORDIC STRUCTURES



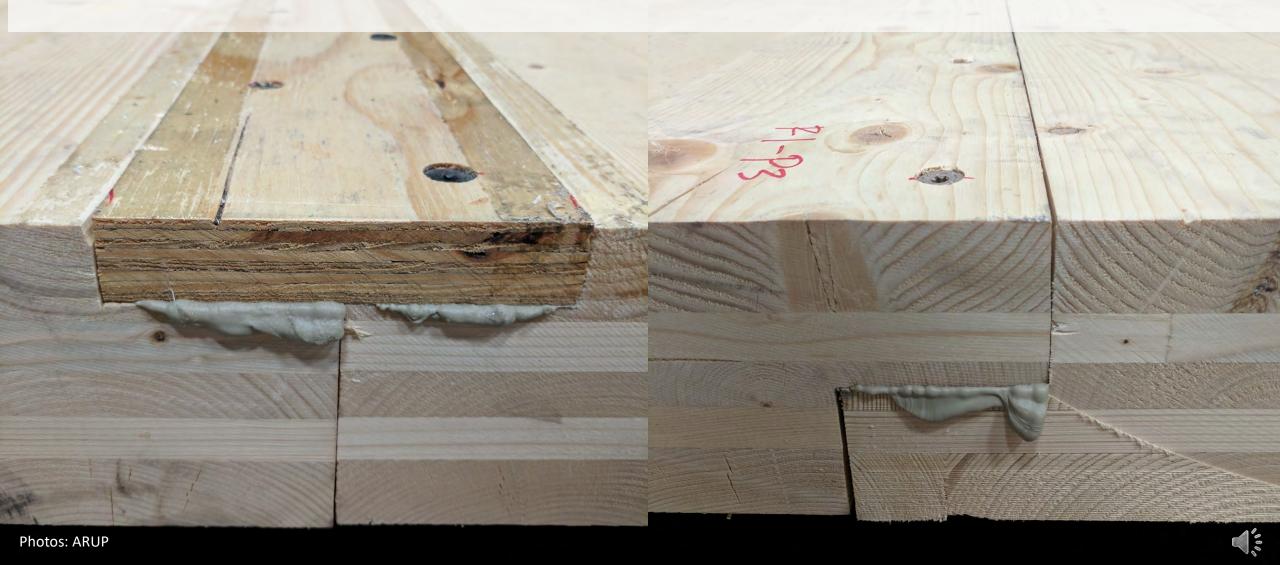
Inventory of Fire Tested Penetrations in MT Assemblies

Table 3: North American Fire Tests of Penetrations and Fire Stops in CLT Assemblies



CLT Panel	Exposed Side Protection	Penetrating Item	Penetrant Centered or Offset in Hole	Firestopping System Description	F Rating	T Rating	Stated Test Protocal	Source	Testing Lab
3-ply (78mm(3.07*)	None	1.5* diameter data cable bunch	Centered	5.5 in diameter hole. Mineral wool was installed in the 1 in. annular space around the data cables to a total depth of approximately 2 - 5/64 in. The remaining 1 in, annular space from the top of the mineral wool to the top of the floor assembly was filled with Hilli FS-One Max cash king.	1 hour	0.5 hour	CANUILE S115	26	Interiek March 30, 2016
3-ply (78mm3.07%)	None	2" copperpipe	Centered	4.375 in diameter hole. Pips wrap was installed around the copper pipe to a total depth of approximately 2 − 5/64in. The remaining 1 in .amnular space starting at the top of the mineral wool to the top of the floor ≥ sembly was filled with Hilli FS-One Max caulking.	4 forur	NA.	CANULC SUS	26	Jatonek March 30, 2016
3-p(y (78mm 3.07*)	None	2.5° sched. 40 pipe	Centured	4.92 in diameter hole. Pipe way was installed around the schedule 40 pipe to a total depth of approximately 2 - 5/felin. The remaining 1 in an nulm space starting at the top of the pipe way to the top of the floor assembly was filled with Hill FS-One Max coulking.	1. hour	N.A.	CANTILE SHIP	26	Murch 30, 2016
3-ply (78mm3.07*)	None	6" cast iron pipe	Centered	8.35 in diameter hole. Minoral wool was installed in the Lin annular space around the cast iron pipe to a total depth of approximately 2 - 5/64 in. The tenuining Lin annular space starting at the top of the pipe wrap to the top of the floor assembly was filled with Hilti FS- One Max coulding	1 hour	NA.	CANULC S115	26	March 30, 2016
3-ply (78mm 3.07*)	None	Hilli 6 in drop in device System No.: F-B-2049	Centered	9.01° diameter hole. Mineral wool was installed in the 1 – 1/4 in annular space around the drop-in device to a total depth of approximately 1 – 7/64 in and the remaining 1 in annular space from the top of the mineral wool to the top edge of the 9 – 1/64 in hole in the CLT was filled with fifth FS-One Max caulking.	I hour	0.75 hour	CANULC SHIS	26	Intertek March 30, 2016
5-ply CLT {131 innv 5.16*)	Note	1.5* diameter data cubic bunch	Contered	3.5° diameter hole. Mineral wool was installed in the tin, annular space around the data cables to a total depth of approximately 4 – 5/32 in. The remaining 1 in, annular space from the top of the mineral wool to the top of the floor assembly was filled with Hilli FS-One Max casilving.	2 hours	1.5 hours	CANULC SILE	26	Intertek March 50, 2016
5-ply CLT (131/mm 5.16*)	None	2" copperpipe	Centsred	4.375 in diameter hole. Pipe wrap was installed around the copper pipe to a total depth of approximately 4 = 5/32 in. The remaining 1 in annular space starting at the top of the minural wood to the top of the floor mountely was filled with Hilli FS-One Max can lking.	2 hours	NA.	CANUTE STI 5	26	Interiok March 30 ,2016
5-ply CLT (131 mm 5.16*)	Note	2.57 schod.40 pipe	Contend	4,92 in diameter hole. Pipe wrap was installed around the schedule 40 pipe to a total depth of approximately 4 - 5/32 in The remaining 1 in annular space starting at the top of the pipe wrap to the top of the floor assembly was filled with Hitti FS-One Max caulking.	2 hours	0.5 hour	CANULE STEE	26	Interick March 30, 2018
5-ply CLT (131 ann 5.16*)	None	6" cast from pipe	Centered	8.35 in diameter hole. Mineral woo i was installed in the Lin. annular space around the cast from pipe to a total depth of approximately 4 - 5/52 in. The remaining Lin. annular space starting at the top of the pipe wrap to the top of the flowr assembly was filled with Hilti PS- One Max caulking.	2 hours	NA-	CANUTE STIS	26	Intertek March 30 , 20 16
5-ply CLT (131 mm 5-16*)	None	Hilti 6 in drop in device System No: F-B-2049	Contered	9.01" diameter hole. Mineral wool was installed in the 1-1/4 in annular space around the drop-in device to a total depth of approximately 1-7/64 in and the remaining 1 in annular space from the top of the mineral wool to the top edge of the 9-1/64 in hole in the CLT was filled with fifth FS-One Max caulking.	2 hours	1.5 hours	CANULC SHE	26	Jisteriek March 30, 2016
3-ply i ?Sunm ë #7.5*)	None	1° nomenal PVC pipe	Contored	4.21 in diameter with a 3/4 in plywood reducer flush with the top of the slab reducing the opening to 2.28 in. Two wraps of filliti CP 648-E W45/1-3/4" Firest op wrap strip at two locations with a 30 gauge steel sleeve which extended from the top of the slab to 1 in below the slab. The first location was with the bottom of the wrap strip flush with the bottom of the steel sleeve and the second was with the bottom of the wrap strip flush with the bottom of the steel sleeve and the second was with the bottom of the wrap strip 5 in. From the bottom of the slab. The void between the seel sleeve and between the steel sleeve and pipe at the top was filled with Roxal Safe mineral wool leaving a 3/4 in deep void at the top of the assembly. Hilli PS-One Max Intunescent Firestop Scalant was applied to a depth of 3/4 in on the top of the assembly between the plywood and steel sleeve as well as the steel sleeve and pipe.	2 hours	2 hours	ASIM DE 14	24	QAI Laboratories March 5, 2917

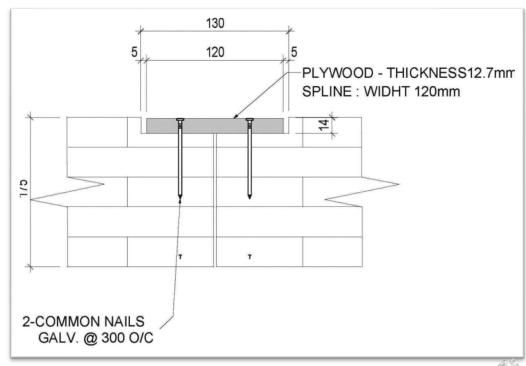
SEALANTS AT MT PANEL EDGES



Sealants at MT Panel Edges

703.9 Sealing of adjacent mass timber elements. In buildings of Type IVA, IVB, and IVC construction, sealant or adhesive shall be provided to resist the passage of air in the following locations:

- 1. At abutting edges and intersections of mass timber building elements required to be fire resistance-rated
- 2. At abutting intersections of mass timber building elements and building elements of other materials where both are required to be fire resistance-rated.





Sealants at MT Panel Edges

Sealants shall meet the requirements of ASTM C920 (elastomeric joint sealants). Adhesives shall meet the requirements of ASTM D3498 (gap filling construction adhesives, i.e. not fire caulk).

Exception: Sealants or adhesives need not be provided where they are not a required component of a fire resistance- rated assembly.







Sealants at MT Panel Edges

Several MT fire tested assemblies have successfully been completed w/o adhesives/sealants at abutting panel edges

2021 IBC will require periodic special inspections of adhesive/sealant installation (when required to be installed)







Occupancy Separation

Protection of MT used for occupancy separation

Addition to IBC 508.4.4.1 requires:

Mass timber elements serving as fire barriers or horizontal assemblies to separate occupancies in Type IV-B or IV-C construction shall be separated from the interior of the building with a minimum of ½" gypsum board or a noncombustible equivalent.



Photo: MIT | John Klein

Incidental Use Separation

Protection of MT used for incidental use separation

New section 509.4.1.1 requires:

Where Table 509 specifies a fire- resistancerated separation, mass timber elements serving as fire barriers or a horizontal assembly in Type IV-B or IV-C construction shall be separated from the interior of the incidental use with a minimum of ½" gypsum board or a noncombustible equivalent.



Photo: MIT | John Klein

New code provisions in International Fire Code (IFC) address construction fire safety of tall wood buildings

3308.4 Fire safety requirements for buildings of Types IV-A, IV-B, and IV-C construction. Buildings of Types IV-A, IV-B, and IV-C construction designed to be greater than six stories above grade plane shall meet the following requirements during construction unless otherwise approved by the fire code official.

- 1. Standpipes shall be provided in accordance with Section 3313.
- 2. A water supply for fire department operations, as approved by the fire chief.





IFC 3313 Standpipe Requirements

SECTION 3313 STANDPIPES

3313.1 Where required.

In buildings required to have standpipes by Section 905.3.1, not less than one standpipe shall be provided for use during construction. Such standpipes shall be installed prior to construction exceeding 40 feet (12 192 mm) in height above the lowest level of fire department vehicle access. Such standpipe shall be provided with fire department hose connections at accessible locations adjacent to usable stairways. Such standpipes shall be extended as construction progresses to within one floor of the highest point of construction having secured decking or flooring.

3313.2 Buildings being demolished.

Where a building is being demolished and a standpipe is existing within such a building, such standpipe shall be maintained in an operable condition so as to be available for use by the fire department. Such standpipe shall be demolished with the building but shall not be demolished more than one floor below the floor being demolished.

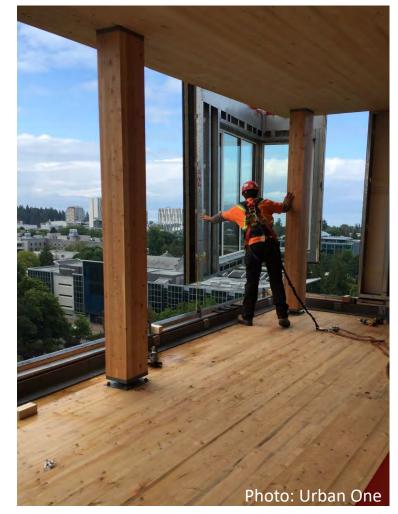
3313.3 Detailed requirements.

Standpipes shall be installed in accordance with the provisions of Section 905.

Exception: Standpipes shall be either temporary or permanent in nature, and with or without a water supply, provided that such standpipes comply with the requirements of Section 905 as to capacity, outlets and materials.

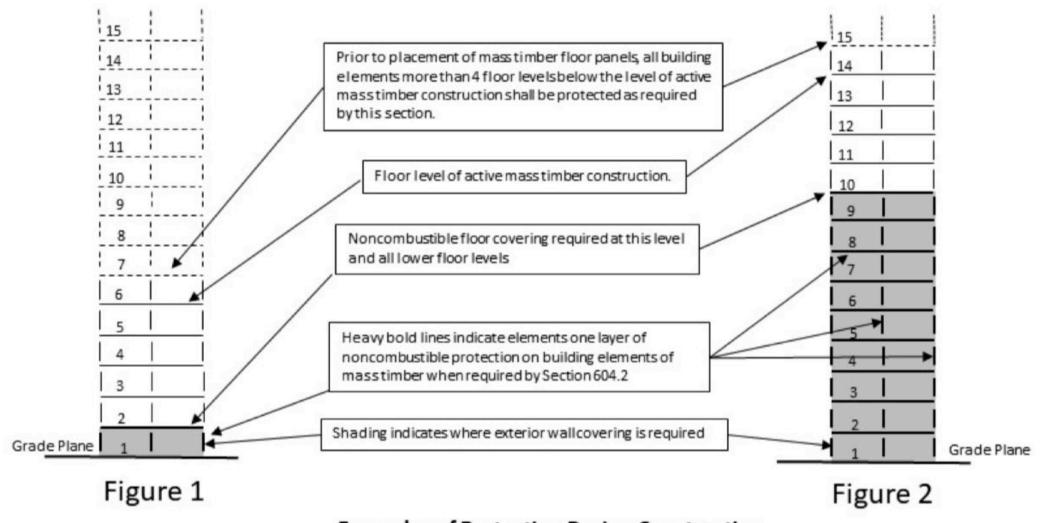
IFC 3308.4 Cont'd

- 3. Where building construction exceeds six stories above grade plane, at least one layer of noncombustible protection where required by Section 602.4 of the International Building Code shall be installed on all building elements more than 4 floor levels, including mezzanines, below active mass timber construction before erecting additional floor levels.
- 4. Where building construction exceeds six stories above grade plane required exterior wall coverings shall be installed on all floor levels more than 4 floor levels, including mezzanines, below active mass timber construction before erecting additional floor level.









For Mass Timber Buildings Greater Than 6 Stories Above Grade Plane





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