

ICC TALL WOOD AD HOC COMMITTEE

Project Scope

In December 2015, the ICC Board established the ICC Ad Hoc Committee on Tall Wood Buildings noting the purpose of the ad hoc committee is to

1. explore the building science of tall wood buildings

- 2. investigate the feasibility, and
- 3. take action on developing code changes for tall wood buildings.

This scope will require further refinement by the committee.



ICC TALL WOOD AD HOC COMMITTEE

Membership

The Board has determined that the effort is to be undertaken by the newly formed Ad Hoc Committee on Tall Wood Buildings (AH-TWB). In making the committee appointments, the Board recognized the need to have a consensus committee comprised of the necessary balance of stakeholders including:

• Representatives from building construction material industries

- Building and Fire Officials
- Architects and engineers
- Fire protection experts
- Other construction related stakeholders



TWB Committee

- 4 Work Groups appointed
 - Definitions and Standards
 - Fire
 - Structural
 - Codes
- 82 major issues identified, assigned to specific work groups, and investigated
- Hundreds of reports reviewed and collected via ICC TWB webpage
- Performance Objectives discussed and listed





TWB Ad Hoc Objectives

TWB identified performance objectives to be met:

- No collapse under reasonable scenarios of complete burn-out of fuel without automatic sprinkler protection being considered
- No unusually high radiation exposure from the subject building to adjoining properties to present a risk of ignition under reasonably severe fire scenarios
- No unusual response from typical radiation exposure from adjacent properties to present a risk of ignition of the subject building under reasonably severe fire scenarios

TWB Ad Hoc Objectives (cont'd)

TWB identified performance objectives to be met:

- No unusual fire department access issues
- Egress systems designed to protect building occupants during design escape time, plus a factor of safety
- Highly reliable fire suppression systems to reduce risk of failure during reasonably expected fire scenarios. Degree of reliability proportional to evacuation time (height) and risk of collapse.



The TWB has determined that

its comprehensive

package of proposals

meet these performance

objectives





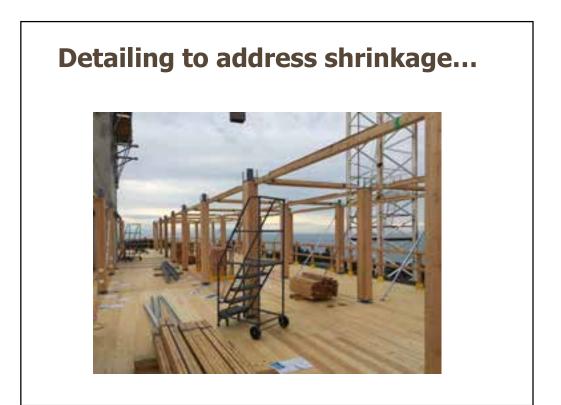
IBC Section 2304.3.3



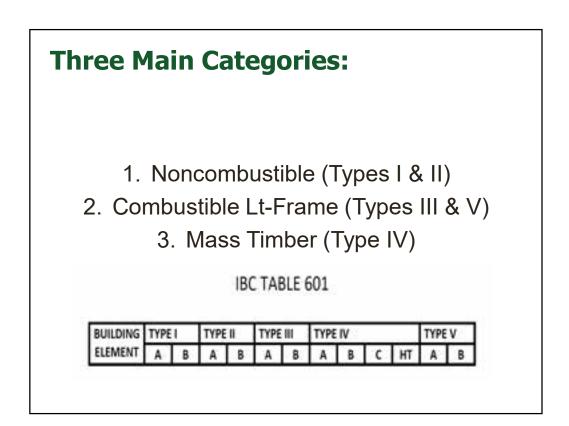
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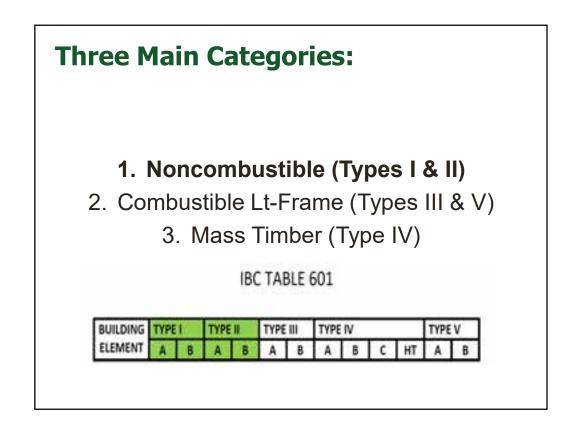
Shrinkage must be accounted for in platform construction:

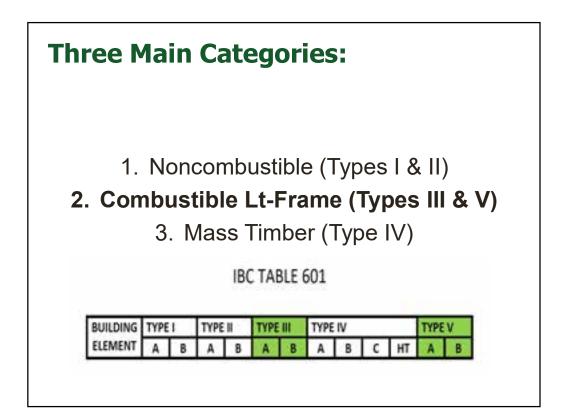
2304.3.3 Shrinkage. Wood walls and bearing partitions shall not support more than two floors and a roof unless an analysis satisfactory to the building official shows that shrinkage of the wood framing will not have adverse effects on the structure or any plumbing, electrical or mechanical systems or other equipment installed therein due to excessive shrinkage or differential movements caused by shrinkage. The analysis shall also show that the roof drainage system and the foregoing systems or equipment will not be adversely affected or, as an alternate, such systems shall be designed to accommodate the differential shrinkage or movements.

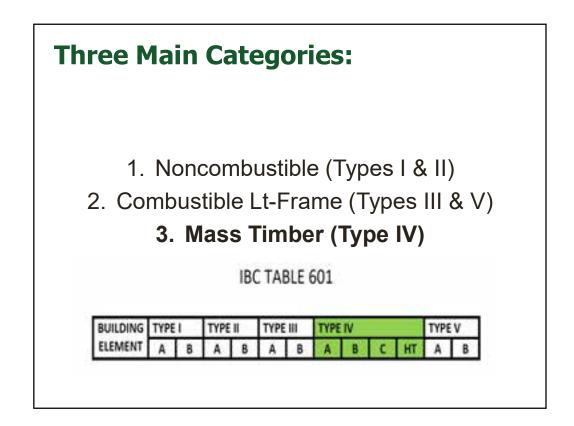














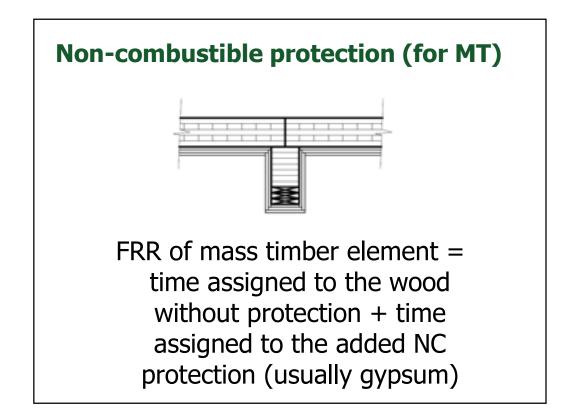
Fire Behavior Depends on:

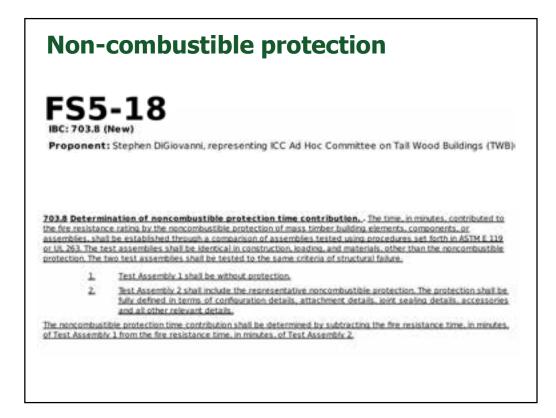
Fire behavior depends in part on:

- Amount of exposed wood
- Arrangement of exposed wood
- Thermal performance of adhesive

Behavior of Fire and Materials Protection of mass timber construction:





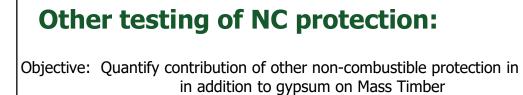


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Testing of NC protection: Western Fire Center



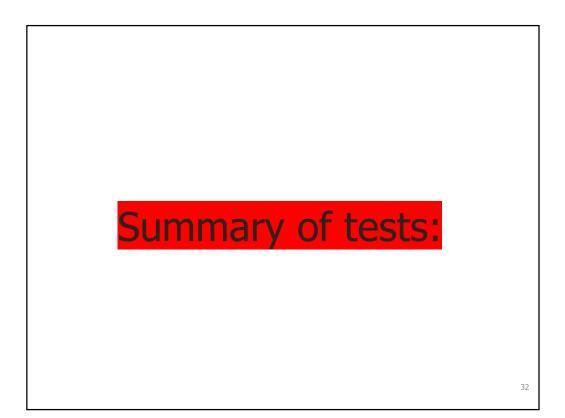
Photo Courtesy of ROCKWOOL

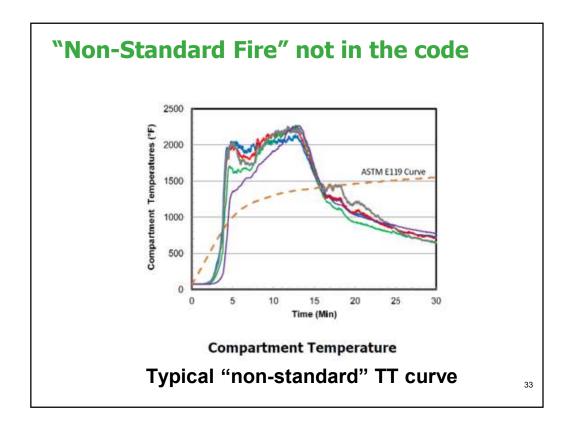


	Unprotected CLT (control test)	Single-Layer Protection	Triple-Layer Protection	Mineral Wool Protection
CLT type/grade		5-Lay	er V4 (Smartlam)	
CLT panel size	Two	7'x18' panels per test, jo	ned together for an overall size of 1-	4′x18′
Loading	24 sa	and-filled barrels, uniform	ly-distributed for an applied load of	60 psf
Span			17'-10″	
Load Ratio		75% of ASD mo	ment (including self-weight)	
Noncombustible protection	None	1 layer of 5/8" Type X gypsum wallboard	3 layers of 5/8" Type X gypsum wallboard	2" thick; 8 pcf mineral wool
GWB attachment	None	Type S screws @ 12" o.c. both directions. 1" penetration into CLT. 1.5" edge distance.	Type S screws @ 12" o.c. both directions, staggered 4"each layer. 1" penetration into CLT. 1.5" edge distance.	Type S screws and 1.5" fender washers at
Deflection at End of Test	12.5″	12.5″	12.0″	12.0″
Test duration	149.4 minutes	189.7 minutes	276.8 minutes	261.3 minutes
Noncombustible protection contribution		40.3 minutes	127.4 minutes	113 minutes
Time attributed to each layer		40.3 min/layer	42.5 min/layer	113 minutes



- NC Protection meets 2/3 FRR of Table 601 and other specific requirements?
- Overall FRR of building elements (either exposed or protected) meet the minimum FRR requirements of Table 601 (calculated or tested)?





Year	Test Sponsor and Location	Test Description	Fire Test Std
2011	FPInnovations (FPI); National Research Council of Canada (NRC)	Protected Cross-Laminated Timber (CLT) Floor and Wall Tests,	E 119
2012	American Wood Council (AWC); NGC Testing Services	5 ply CLT wall with 8700 PLF load protected with 1 layer of 5/8" type X gypsum wall board (GWB) each side	E 119
2014	AWC; Western Fire Center (WFC)	GWB-Protected Beam Tests, Protected Structural Composite Lumber (SCL) Tests	E 119
2015	AWC; Southwest Research Institute (SwRI)	Nail Laminated Timber (NLT) and CLT compartments; 2 hour FRR fire stops	Non-Standard; E 814
2016	LEVER Architecture, ARUP; SwRI	2 Hour exposed beam and column test with CLT deck	E 119
2017	FPRF, NRC; NIST National Fire Research Lab	CLT Compartment Fire Tests (w/ first generation PUR adhesive CLT)	Non-Standard
2017	US FPL, ICC Tall Wood Ad Hoc (TWB), AWC; ATF Lab	Compartment Fire Tests, Two Story Mass Timber Building	Non-Standard
2017	AWC; SwRI	Development of a Fire Performance Assessment Methodology for CLT Adhesives	New PRG 320, Annex B standard
2017	AWC; WFC	CLT Floor/Ceiling Assembly to establish the contribution of GWB to FRR	E 119
2018	NRC, CNRC	Fire Testing of Rooms with Exposed Second Generation PUR adhesive CLT	Non-Standard

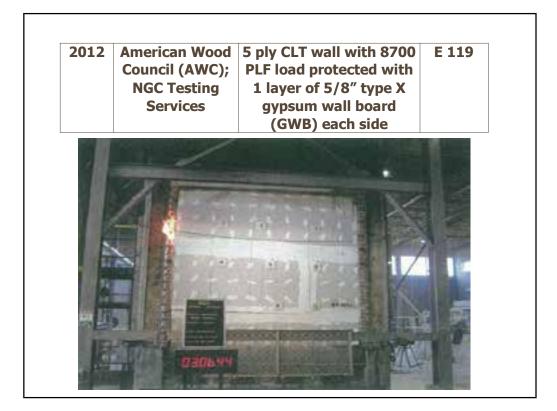
2011	FPInnovations (FPI); National Research Council of	Protected Cross- Laminated Timber (CLT) Floor and Wall Tests,	E 119
	Canada (NRC)		

As discussed in 2.8, in 2011, FPInnovations (FPI), in collaboration with the National Research Council of Canada (NRC), conducted a series of 8 full-scale fire resistance tests of CLT floors and walls [50]. All tests followed the ULC \$101 time-temperature curve, a fire exposure comparable to the ASTM E119 time-temperature curve. Three of the CLT floors and one of the CLT walls were protected with GWB.

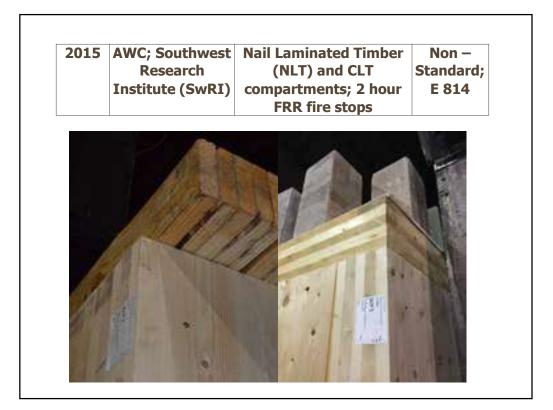
As reported in Section 2.8 for unprotected CLT floor and wall tests, loading of the floors and walls was based on Canadian standards. For purposes of this analysis, allowable stress design (ASD) values were determined by using relevant grades from the CLT product standard, PRG-320 [51]. Structural fire resistance was then calculated using NDS design provisions and appropriate ASD design values from PRG-320.

NRC Test #1 - Protected Floor: NRC Test #2 - Protected Wall: NRC Test #5 - Protected Floor: NRC Test #6 - Protected Floor:

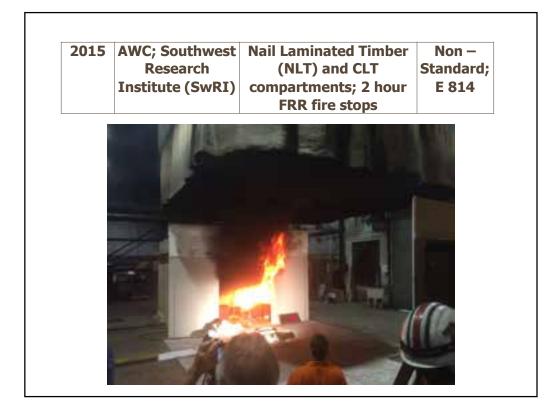




(W	Western Center /FC)	S	tructu	s, Pro Iral Co	tecte ompo	d site		E 1	19				
									min Au				
Design Stress Ratio	Thickness		SCL Beam + GWB	SCL Beam	OWB	SC Bei	L Im	SCL Beam	0WB Only				
56%	5/8° Type X	1	71	33	38 1	-	Contraction of the	30	40				
113%	5/8' Type X	2	139	50	90	13	0	50	-80				
84%	5/8" Type X	1	74	35	29.1	8	8	26	-40				
84%	5/8° Type X	2	114	35	79	10	8	26	-80				
	Design Stress Ratio 56% 54% 84%	Table 3.6b Ad GWB Desc Design Stress Ratio (inches) 56% 54% Type X 113% 54% Type X 84% 55% Type X	Table 3.6b Added Com GWB Description Design Stress Ratio (inches) 56% 56% Type X 1 113% 56% Type X 2 64% 55% Type X 2 84% 55% Type X 2	Lumbe Table 3.6b Added Contribution of Contrelating andited of Contribution of Contribution of Contributico	Lumber (SC Table 3.6b Added Contribution of Gypsu Table 3.6b Added Contribution of Gypsu Design Stress Thickness Beam Stress Thickness Beam Beam Ratio (inches) Layers CU SCL SCL Stress Thickness Beam Beam Ratio (inches) Layers CU SCL SCL Sd% 5/8° Type X 1 71 33 113% 5/8° Type X 1 74 35 84% 5/8° Type X 2 114 35	Lumber (SCL) Te Table 3.6b Added Contribution of Gypsum Wallbo GWB Description Test Times (minutes) Design Stress Thickness Beam GWB Only Only Stress Thickness Beam GWB Stress CL SCL SCL Stress Beam Beam GWB Stress Clip Stress GWB Only Only Stress Thickness Beam Beam GWB Stress Thickness Beam GWB Stress Thickness Beam GWB Stress Stress GWB Only Only Only Only <td <="" colspan="2" th=""><th>Lumber (SCL) Tests Table 3.6b Added Contribution of Gypsum Wallboard P Owner of Gypsum Wallboard P GWB Description Test Times (minutes) Est Dresign Stuber of Gypsum Wallboard P Stuber of Gypsum Wallboard P</th><th>Lumber (SCL) Tests Table 3.6b Added Contribution of Gypsum Wallboard Protect GWB Description Test Times (minutes) Estimated Design SCL <th colspa="2" scl<="" th=""><th>Lumber (SCL) Tests Table 3.6b Added Contribution of Gypsum Wallboard Protection GWB Description Test Times (minutes) Estimated Times (Design SCL <th co<="" th=""></th></th></th></th></td>	<th>Lumber (SCL) Tests Table 3.6b Added Contribution of Gypsum Wallboard P Owner of Gypsum Wallboard P GWB Description Test Times (minutes) Est Dresign Stuber of Gypsum Wallboard P Stuber of Gypsum Wallboard P</th> <th>Lumber (SCL) Tests Table 3.6b Added Contribution of Gypsum Wallboard Protect GWB Description Test Times (minutes) Estimated Design SCL <th colspa="2" scl<="" th=""><th>Lumber (SCL) Tests Table 3.6b Added Contribution of Gypsum Wallboard Protection GWB Description Test Times (minutes) Estimated Times (Design SCL <th co<="" th=""></th></th></th></th>		Lumber (SCL) Tests Table 3.6b Added Contribution of Gypsum Wallboard P Owner of Gypsum Wallboard P GWB Description Test Times (minutes) Est Dresign Stuber of Gypsum Wallboard P Stuber of Gypsum Wallboard P	Lumber (SCL) Tests Table 3.6b Added Contribution of Gypsum Wallboard Protect GWB Description Test Times (minutes) Estimated Design SCL SCL <th colspa="2" scl<="" th=""><th>Lumber (SCL) Tests Table 3.6b Added Contribution of Gypsum Wallboard Protection GWB Description Test Times (minutes) Estimated Times (Design SCL <th co<="" th=""></th></th></th>	<th>Lumber (SCL) Tests Table 3.6b Added Contribution of Gypsum Wallboard Protection GWB Description Test Times (minutes) Estimated Times (Design SCL <th co<="" th=""></th></th>	Lumber (SCL) Tests Table 3.6b Added Contribution of Gypsum Wallboard Protection GWB Description Test Times (minutes) Estimated Times (Design SCL SCL <th co<="" th=""></th>	

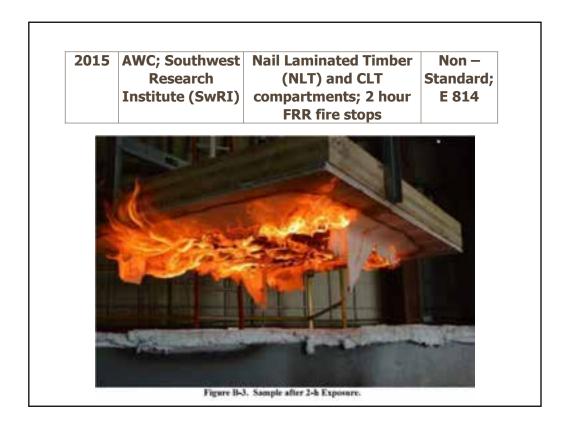


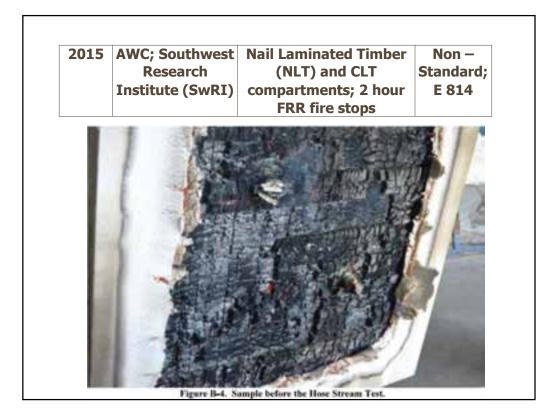
2015	AWC; Southwest Research Institute (SwRI)	(NLT) and CLT	Non – Standard; E 814

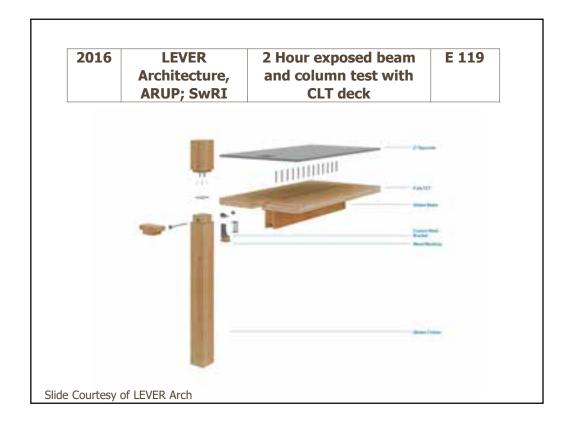


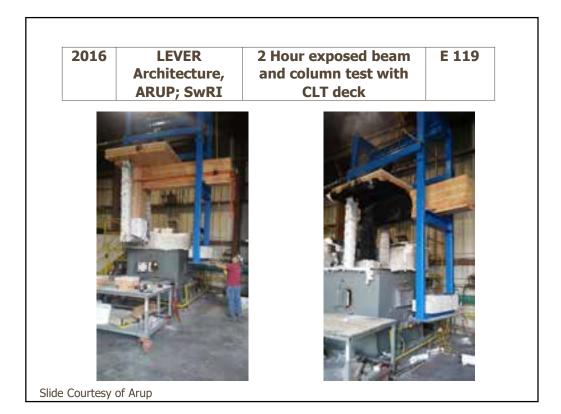
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·	-		1 A

2015	AWC; Southwest Research Institute (SwRI)	Nail Laminated Timber (NLT) and CLT compartments; 2 hour FRR fire stops	Non – Standard E 814
	OF A PENETRATION IN ACCORDANCE	WITH ASTM E814-13A, THOD FOR FIRE TESTS OF	
	FINAL REPORT Consisting of 18 Pages		
	SwRI® Project No. 01.21 Test Date: September 3 Report Date: October 2	0, 2015	
	Test Date: September 3	0, 2015	









2017	FPRF, NRC; NIST National Fire Research Lab	CLT Compartment Fire Tests (w/ first generation PUR adhesive CLT)	Non- Standard
	lone for NFPA's Pro	rch Foundation (FPRF) operty Insurance Researc	h Group
		ntribution of CLT_elemen lect data for <u>insurance m</u>	
Tests p	erformed by NRC	Canada	
Tests p	erformed at NIST	facilities	17
C C	aartmant tasta		And the second se

- 6 Compartment tests:
 - 2 with all CLT protected
 - 4 with various surfaces exposed
- Report available at FPRF website:
 <u>https://www.nfpa.org/News-and-Research</u>



Images courtesy of Joseph Su, NRC Canada

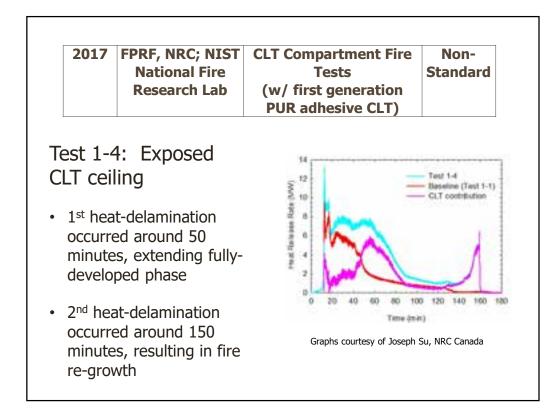
2017	FPRF, NRC; NIST National Fire Research Lab	T (w/ first	eartment Fire ests generation nesive CLT)	Non- Standard
when	nificant contributio all surfaces were p ype X gypsum wall	rotected		
CLT co	e surfaces were exp ontribution increase sing exposed CLT s	ed with		A
	ing performed by F te of Sweden (RIS		المراقف	-FE TH

Images courtesy of Joseph Su, NRC Canada

2017	FPRF, NRC; NIST	CLT Compartment Fire	Non-
	National Fire	Tests	Standard
	Research Lab	(w/ first generation	
		PUR adhesive CLT)	

- · Fire re-growth observed in multiple FPRF tests
- Fire re-growth caused by failure of bond lines before being reached by char front (i.e., heat-delamination)





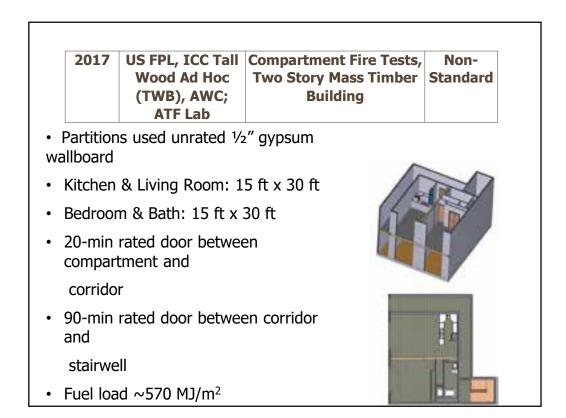
2017	US FPL, ICC Tall	Compartment Fire Tests ,	Non-
	Wood Ad Hoc	Two Story Mass Timber	Standard
	(TWB), AWC;	Building	
	ATF Lab		

- Purpose: Perform tests of realistic fire scenarios applicable to tall wood construction in order to <u>evaluate</u> <u>occupant and firefighter tenability</u> for egress and suppression efforts, and to provide data necessary <u>to</u> <u>guide further development of relevant code and standard</u> <u>provisions</u>
- Conducted at U.S. government facilities (ATF)
- Supervised by U.S. Forest Product Laboratory staff

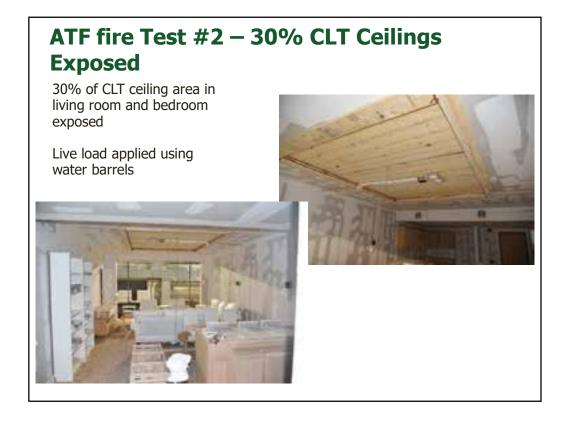


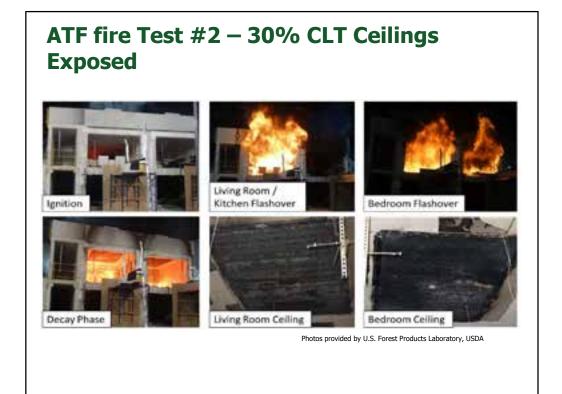
2017	US FPL, ICC Tall Wood Ad Hoc (TWB), AWC; ATF Lab	Compartment Fire Tests, Two Story Mass Timber Building	
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Test	Description	Date	Duration
Test 1	All mass timber surfaces protected with 2 layers of 5/8" Type X GWB	5/23/17	3 hours
Test 2	30% of CLT ceiling area in living room and bedroom exposed	5/31/17	4 hours
Test 3	Two opposing CLT walls exposed – one in bedroom and one in living room (there is a partition wall)	6/20/17	4 hours
Test 4	All mass timber surfaces fully exposed in bedroom and living room. Sprinklered – normal activation	6/27/17	6 minutes
Test 5	All mass timber surfaces fully exposed in bedroom and living room (except bathroom). Sprinklered – 23 min delayed activation	6/29/17	30 minutes









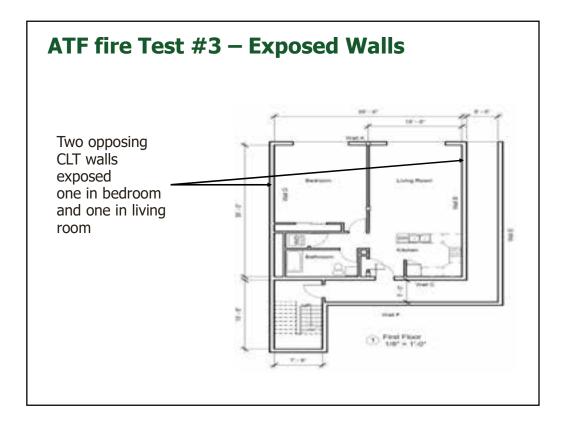
Atf fire Test #2 – 30% CLT Ceilings Exposed

Post-Fire Condition of Glulam After Gypsum Removal

- Fire intensity decreased subsequent to consumption of furnishings and contents (known as *decay phase*)
- Exposed mass timber surfaces selfextinguished in the decay phase
- Mass timber surfaces protected with 2 layers of 5/8" Type X GWB remained mostly uncharred









	Time After Ignition (mm:ss)					
Test No.	Flashover (600°C) Living Room	Flashover (600°C) Bedroom	Flames in Hallway	Compartment door Fails	Sprinkler Activation	
1 1 st floor	13:27	17:20	26:51	57:46	N/A	
2 2 nd floor	11:42	17:20	30:38	63:59	N/A	
3 2 nd floor	12:37	17:00	13:06 (door frame installation error)	29:42 (door frame installation error)	N/A	
4 1 st floor	-	-	-	-	2:37	
5 1 st floor	-	-	-	-	23:00	







Adhesive qualification tests

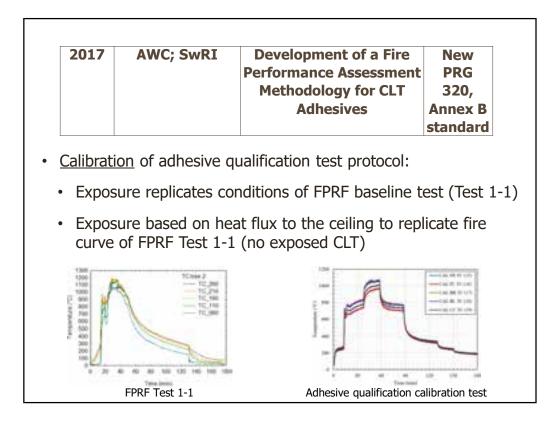
Direction provided by ICC-TWB Ad-Hoc Committee

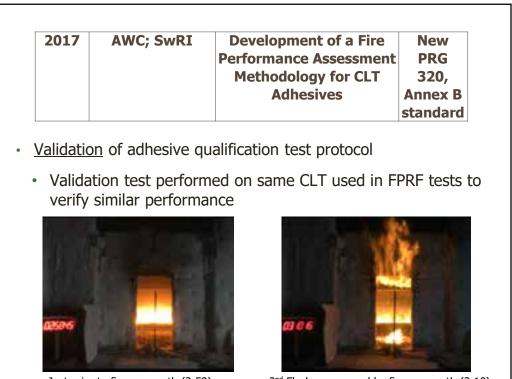
- Need test protocol capable of identifying heat-delaminating adhesives
- Code-referenced standards governing CLT should require adhesive qualification using this protocol



2017	AWC; SwRI	Development of a Fire Performance Assessment Methodology for CLT Adhesives	New PRG 320, Annex B standard
est proto	col developed by	y Southwest Research Insti	tute (SwR
Large-s	cale compartme	nt test (9' x 19' compartme	ent)
Expose	d CLT ceiling (as	was tested in FPRF Test 1-	-4)
	me CLT span as RF tests (~15')	in	
	me loading as in sts (20 psf)	FPRF	
• Sa	me ventilation ra	atio as	

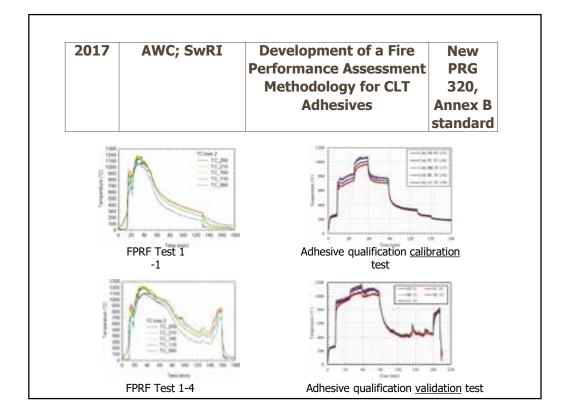
201	7 AWC; SwRI	Development of a Fire Performance Assessment Methodology for CLT Adhesives	New PRG 320, Annex B standard
1	Validato tost s	otup for EDDE T/T our	
1.	valluate test so	etup for FPRF T/T cur	ve
2.	Recreate char original PUR	drop off or "delaminat	tion" of
3.	Melamine adhe	esive testing	
	2 nd generation	PUR adhesive testing	3
4.	•		-

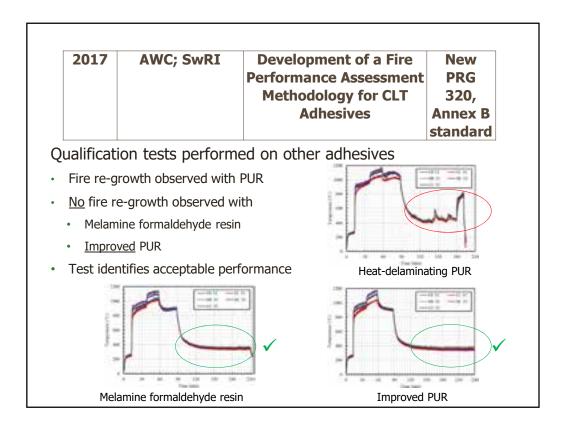


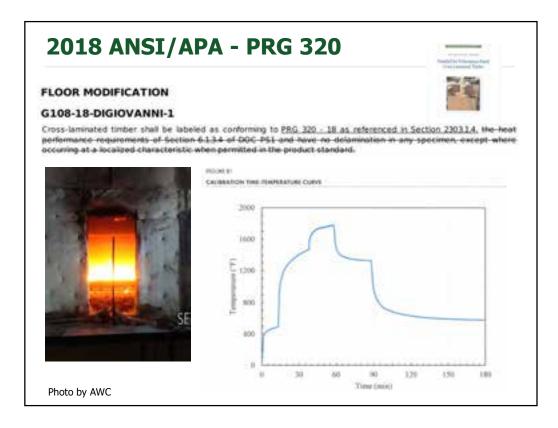


Just prior to fire re-growth (2:59)

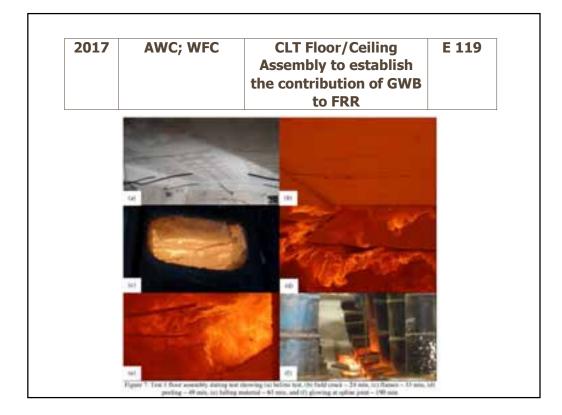
2nd Flashover caused by fire re-growth (3:10)

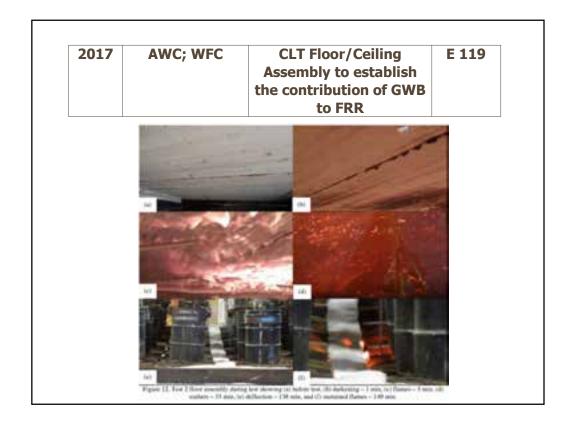


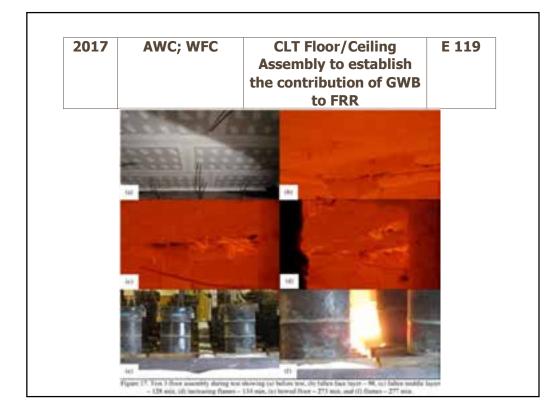


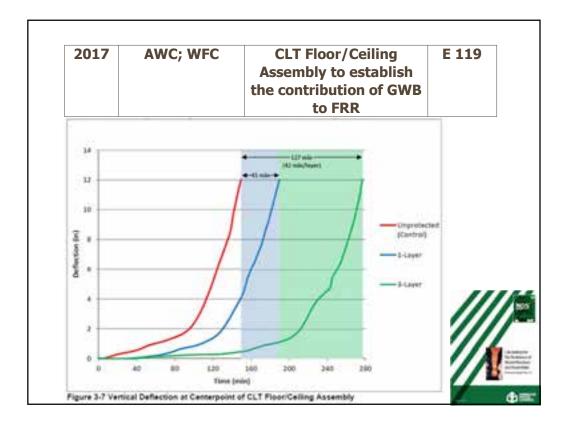


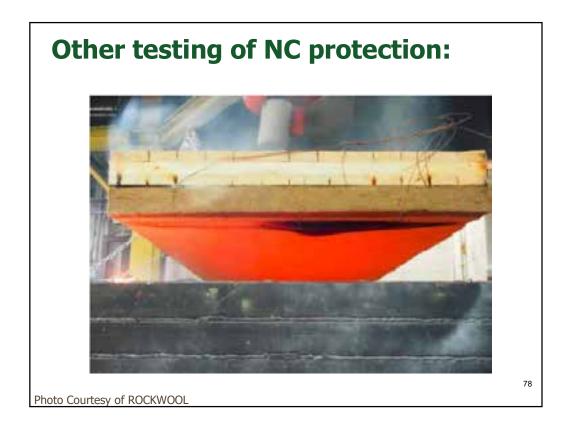








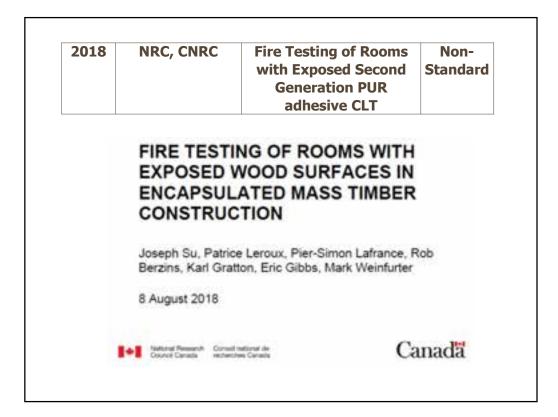


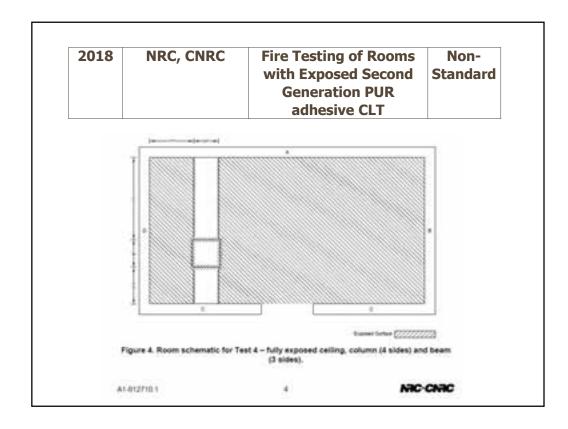


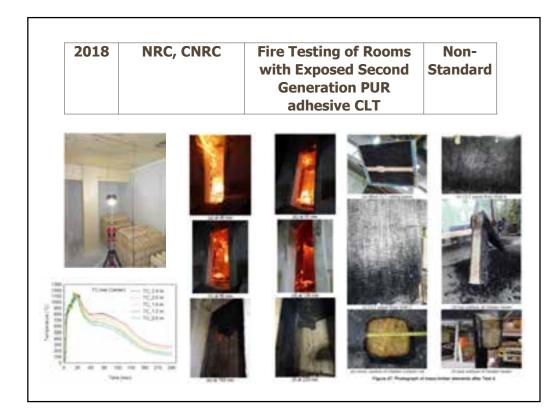
Other testing of NC protection:

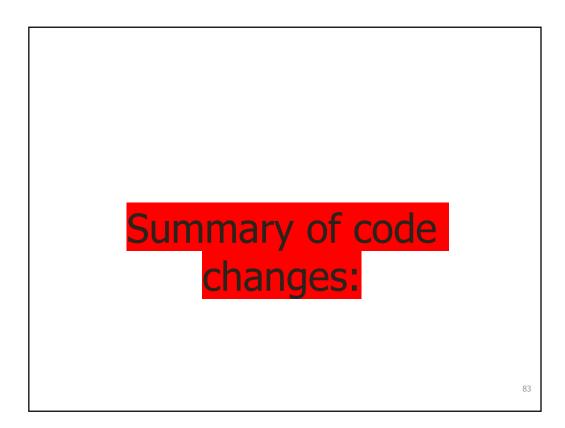
Objective: Quantify contribution of other non-combustible protection in in addition to gypsum on Mass Timber

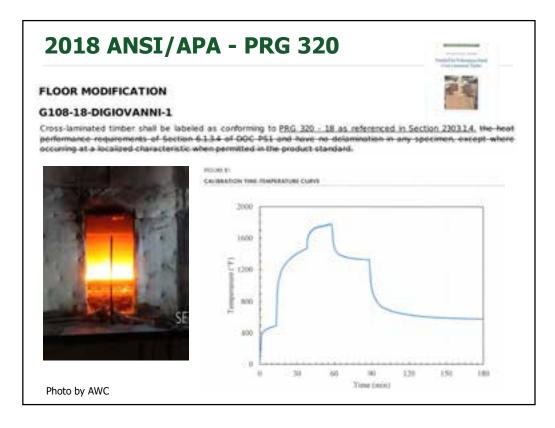
	Unprotected CLT (control test)	Single-Layer Protection	Triple-Layer Protection	Mineral Wool Protection
CLT type/grade	5-Layer V4 (Smartlam)			
CLT panel size	Two 7'x18' panels per test, joined together for an overall size of 14'x18'			4′x18′
Loading	24 sa	nd-filled barrels, uniform	ly-distributed for an applied load of	60 psf
Span			17'-10"	
Load Ratio		75% of ASD mo	ment (including self-weight)	
Noncombustible protection	None	1 layer of 5/8" Type X gypsum wallboard	3 layers of 5/8" Type X gypsum wallboard	2" thick; 8 pcf mineral wool
GWB attachment	None	Type S screws @ 12" o.c. both directions. 1" penetration into CLT. 1.5" edge distance.	Type S screws @ 12" o.c. both directions, staggered 4"each layer. 1" penetration into CLT. 1.5" edge distance.	Type S screws and 1.5" fender washers at
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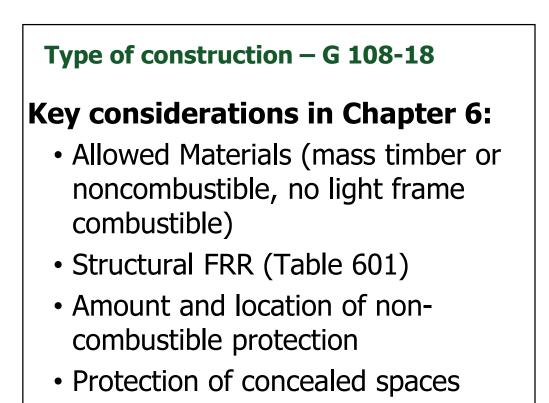




Groups of code changes:

14 approved change fall into 6 basic subjects:

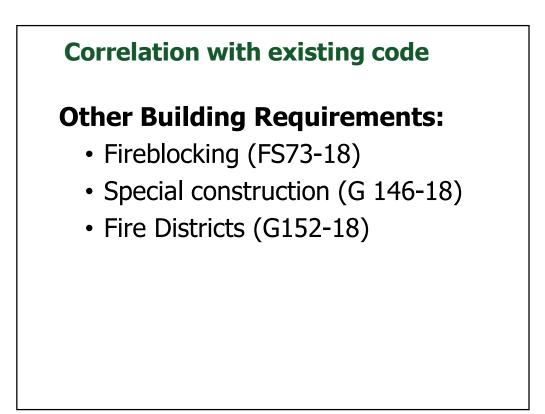
- Non-combustible protection
- New construction types (materials and amount of protection)
- Height and area
- Other building requirements
- Construction and maintenance
- Correlation with existing code



Other building requirements

Other Building Requirements:

- Sealant at edges (FS6-18)
- High-rise sprinkler redundant water supply for Type IVA and IV B greater than 120 height above grade (G 28-18)
- Separated occupancy and incidental use separations additional requirements (G89-18)



Construction and maintenance

Fire Code Requirements:

- Construction Fire Safety (F266-18)
- Owners Responsibilities (F 88-18)

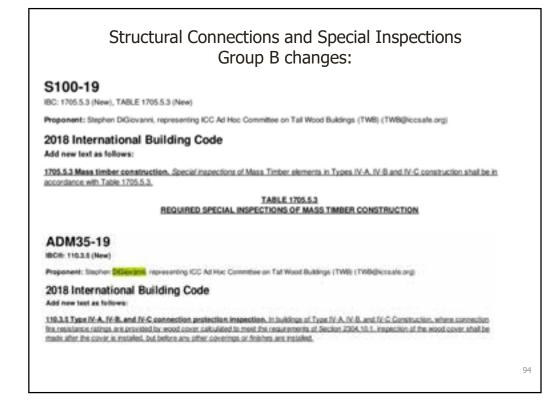
Additional Fire Protection During Construction Requirements

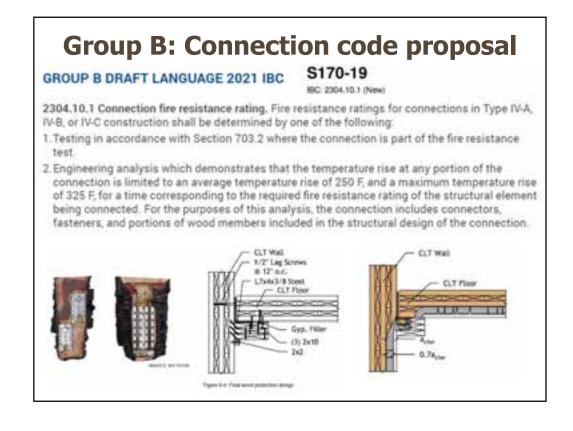
- Requirements for fire protection during construction:
 - Standpipes in accordance with IFC 3313
 - Water supply for fire department operations
 - One layer of noncom protection, <u>if required</u>, on all mass timber more than 4 stories below uppermost floor under construction
 - Exterior wall coverings on all floor levels more than 4 levels below floor under construction – includes mezzanines

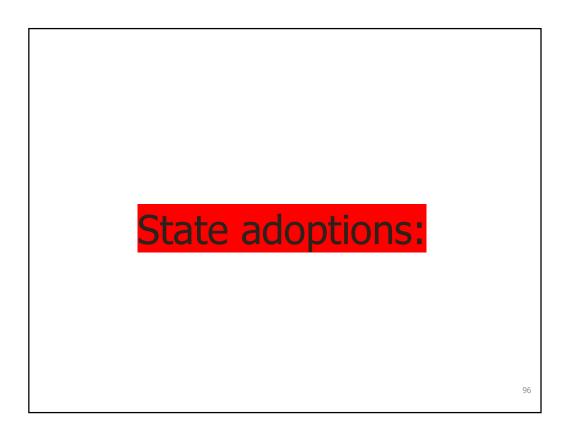












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