New Tall Wood Code Provisions: Understanding Advanced Design Topics

Presented by Presenter's Name

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Questions related to specific materials, methods, and services will be addressed at the conclusion of this presentation.



Course Description

In January 2019, the International Code Council (ICC) approved a set of proposals to allow tall wood buildings as part of the 2021 International Building Code (IBC). Based on these proposals, the 2021 IBC will include three new construction types—Type IV-A, IV-B and IV-C—allowing the use of mass timber or noncombustible materials. These new types are based on the previous Heavy Timber construction type (renamed Type IV-HT) but with additional fireresistance ratings and levels of required noncombustible protection. This presentation will take a detailed look at the new code provisions and methods of addressing the new requirements. Topics will include tall-wood specific high rise and sprinkler requirements, methods of demonstrating fire-resistance ratings, fire design for penetrations, connections and abutting panels, allowances for exposed timber, exterior walls, concealed spaces and more.

Learning Objectives

- 1. Explore the three new tall wood construction types and discuss related code provisions such as allowable heights and fire-resistance ratings.
- 2. Discuss code-compliant options for exposing mass timber, where up to 2hour fire-resistance ratings are required, and demonstrate design methodologies for achieving these ratings.
- 3. Review code requirements unique to tall wood buildings, focusing on items such as sprinklers, shaft construction and concealed spaces.
- 4. Highlight design options for addressing topics such as fire stops at penetrations through mass timber assemblies and exterior walls fire-resistance in tall timber structures.

NEW CONSTRUCTION TYPES IN 2021 IBC

Type IV-A – Maximum 18 stories, with gypsum wallboard on all mass timber.

Type IV-B – Maximum 12 stories, limitedarea of exposed mass timber walls and ceilings allowed.

Type IV-C – Maximum 9 stories, all exposed mass timber designed for a 2hour fire resistance.



Credit: Susan Jones, atelierjones

*BUILDING FLOOR-TO-FLOOR HEIGHTS ARE SHOWN AT 12'-0" FOR ALL EXAMPLES FOR CLARITY IN COMPARISON BETWEEN 2015 TO 2021 IBC CODES.

BUSINESS OCCUPANCY [GROUP B]



New Building Types

Tall Wood Building Size Limits

		Co	nstruction T	ype (All <u>Spri</u>	nklered Valu	<u>ies</u>)	
	I-A	I-B	IV-A	IV-B	IV-C	IV-HT	III-A
Occupancies	Allo	wable Build	ing Height a	bove Grade l	Plane, Feet (l	BC Table 50	4.3)
A, B, R	Unlimited	180	<u>270</u>	<u>180</u>	<u>85</u>	85	85
	Al	lowable Nun	nber of Stori	es above Gra	de Plane (IB	SC Table 505	.4)
A-2, A-3, A- 4	Unlimited	12	<u>18</u>	<u>12</u>	<u>6</u>	4	4
В	Unlimited	12	<u>18</u>	<u>12</u>	<u>9</u>	6	6
R-2	Unlimited	12	<u>18</u>	<u>12</u>	<u>8</u>	5	5
		Allowable A	Area Factor ((At) for SM,	Feet ² (IBC 7	Table 506.2)	
A-2, A-3, A- 4	Unlimited	Unlimited	<u>135,000</u>	<u>90,000</u>	56,250	45,000	42,000
В	Unlimited	Unlimited	<u>324,000</u>	216,000	<u>135,000</u>	108,000	85,500
R-2	Unlimited	Unlimited	<u>184,500</u>	<u>123,000</u>	<u>76,875</u>	61,500	72,000

Tall Wood Building Size Limits

		Construction Type (Unsprinklered Values)							
	I-A	I-B	<u>IV-A</u>	<u>IV-B</u>	<u>IV-C</u>	IV-HT			
Occupancies	Allowa	ble Building H	Height above G	Frade Plane, F	eet (IBC Table	504.3)			
A, B, R	Unlimited	160	<u>65</u>	<u>65</u>	<u>65</u>	65			
	Allow	vable Number	of Stories abo	ve Grade Plan	e (IBC Table 5	05.4)			
A-2, A-3, A-4	Unlimited	11	<u>3</u>	<u>3</u>	<u>3</u>	3			
В	Unlimited	11	<u>5</u>	<u>5</u>	<u>5</u>	5			
R-2	Unlimited	11	<u>4</u>	<u>4</u>	<u>4</u>	4			
	А	llowable Area	Factor (At) fo	r SM, Feet ² (I	BC Table 506.	2)			
A-2, A-3, A-4	Unlimited	Unlimited	45,000	<u>30,000</u>	<u>18,750</u>	15,000			
В	Unlimited	Unlimited	108,000	72,000	45,000	36,000			
R-2	Unlimited	Unlimited	<u>61,500</u>	<u>41,000</u>	<u>25,625</u>	20,500			

Even so, Sprinklers may be required by 903.2 (all occupancies) and definitely for residential (420.4)

Tall Wood Building Size Limits

		Construction Type (Unsprinklered Values)									
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Occupancies	Allowa	ble Building H	Ieight above G	Frade Plane, F	eet (IBC Table	504.3)					
A, B, R	Unlimited	160	<u>65</u>	<u>65</u>	<u>65</u>	65					
	Allo	AllownleanmostranoGasesiane (IBC Table 505.4)									
A-2, A-3, A-4	Unlimited.		will be		$\frac{3}{2}$	3					
В	Unhited	ikiers	wiij pe	requi		5					
R-2	Unlimited	11	4	4	4	4					
	А	llowable Area	Factor (At) for	r SM, Feet ² (I	BC Table 506.	2)					
A-2, A-3, A-4	Unlimited	Unlimited	45,000	30,000	<u>18,750</u>	15,000					
В	Unlimited	Unlimited	108,000	72,000	45,000	36,000					
R-2	Unlimited	Unlimited	<u>61,500</u>	41,000	25,625	20,500					

Even so, Sprinklers may be required by 903.2 (all occupancies) and definitely for residential (420.4)

Non-Tall Opportunities – Large Area

		Construction Type (All <u>Sprinklered Values</u>)								
	I-A	I-B	<u>IV-A</u>	<u>IV-B</u>	<u>IV-C</u>	IV-HT	III-A			
Occupancies	Allo	wable Build	ing Height a	bove Grade l	Plane, Feet (I	BC Table 50	4.3)			
A, B, R	Unlimited	180	<u>270</u>	<u>180</u>	<u>85</u>	85	85			
	Al	lowable Nun	nber of Stori	es above Gra	ade Plane (IB	C Table 505	.4)			
A-2, A-3, A- 4	Unlimited	12	<u>18</u>	<u>12</u>	<u>6</u>	4	4			
В	Unlimited	12	<u>18</u>	<u>12</u>	<u>9</u>	6	6			
R-2	Unlimited	12	18	12	8	5	5			
		Allowable A	Area Factor ((At) for SM,	Feet ² (IBC T	able 506.2)				
A-2, A-3, A- 4	Unlimited	Unlimited	<u>135,000</u>	90,000	<u>56,250</u>	45,000	42,000			
В	Unlimited	Unlimited	<u>324,000</u>	216,000	<u>135,000</u>	108,000	85,500			
R-2	Unlimited	Unlimited	<u>184,500</u>	<u>123,000</u>	<u>76,875</u>	61,500	72,000			

Type IV-A



 18 STORIES

 BUILDING HEIGHT
 270'

 ALLOWABLE BUILDING AREA
 972,000 SF

 AVERAGE AREA PER STORY
 54,000SF

TYPE IV-A

Credit: Susan Jones, atelierjones





Photos: Structurlam, naturally:wood, Fast + Epp

Type IV-A Height and Area Limits



 18 STORIES

 BUILDING HEIGHT

 ALLOWABLE BUILDING AREA

 972,000 SF

 AVERAGE AREA PER STORY

 54,000SF

TYPE IV-A

Credit: Susan Jones, atelierjones

Occupancy	# of Stories	Height	Area per Story	Building Area
A-2	18	270 ft	135,000 SF	405,000 SF
В	18	270 ft	324,000 SF	972,000 SF
Μ	12	270 ft	184,500 SF	553,500 SF
R-2	18	270 ft	184,500 SF	553,500 SF

Areas exclude potential frontage increase

In most cases, Type IV-A height & story allowances = 1.5 * Type I-B height & story allowances Type IV-A area = 3 * Type IV-HT area

Type IV-A Protection vs. Exposed



18 STORIES BUILDING HEIGHT 270 ALLOWABLE BUILDING AREA AVERAGE AREA PER STORY 54.000SF

972,000 SF

TYPE IV-A

Credit: Susan Jones, atelierjones



100% NC protection on all surfaces of Mass Timber



Type IV-A Fire	Resistan	ce Rating	s (FRR) IV-A
	FRR	Min. NC Protection	
Primary Frame FRR	3 HR (2 HR at Roof)	120 min (80 min at Roof)	
Ext or Int Bearing Wall FRR	3 HR	120 min	
Floor Construction FRR	2 HR	80 min	
Roof Construction FRR	1.5 HR	80 min	top

½" Type X Gypsum = 25 min | 5/8" Type X Gypsum = 40 min

Credit: Urban One

Noncombustible Protection (NC)

TABLE 722.7.1(a)

PROTECTION REQUIRED FROM NONCOMBUSTIBLE COVERING MATERIAL

Required Fire Resistance Rating of Building Element per Tables 601 and 602 (hours)	Minimum Protection Re Noncombustible Protection	
1	<u>40</u>	1 layer 5/8 Type X
2	<u>80</u>	2 layers 5/8 Type X
<u>3 or more</u>	<u>120</u>	3 layers 5/8 Type X

TABLE 722.7.1(b)

PROTECTION PROVIDED BY NONCOMBUSTIBLE COVERING MATERIAL

Noncombustible Protection	Protection Contribution (minutes)
1/2 inch Type X Gypsum Board	<u>25</u>
5/8 inch Type X Gypsum Board	<u>40</u>

Noncombustible Protection (NC)



The definition of "Noncombustible Protection (For Mass Timber)" is created to address the passive fire protection of mass timber.

Mass timber is permitted to have its own fireresistance rating (e.g., Mass Timber only) or have a fire resistance rating based on the fire resistance through a combination of the mass timber fireresistance plus protection by non-combustible materials as defined in Section 703.5 (e.g., additional materials that delay the combustion of mass timber, such as gypsum board).





IBC 722.7

The fire resistance rating of the mass timber elements shall consist of the fire resistance of the unprotected element (MT) added to the protection time of the noncombustible (NC) protection.

Credit: Urban

FRR





However, FRR Doesn't always need to be from a combination of MT + NC. In some cases, just NC can be used, in other cases, just MT can be used:

IBC 602.4



Mass timber elements shall meet the fire resistance rating requirements of this section based on either the fire resistance rating of the noncombustible protection, the mass timber, or a combination of both.



MT Type IV Minimum Sizes

In addition to meeting FRR, all MT elements must also meet minimum sizes

These minimum sizes have been in place for old type IV (current type IV-HT) construction and the same minimums sizes also apply to MT used in new types IV-A, IV-B and IV-C

Contained in IBC 2304.11



Type IV Minimum Sizes - Framing

Fr	aming	Solid Sawn (nominal)	Glulam (actual)	SCL (actual)
or	Columns	8 x 8	6 ³ / ₄ x 8¼	7 x 7½
Floor	Beams	6 x 10	5 x 10½	5¼ x 9½
of	Columns	6 x 8	5 x 8¼	5¼ x 7½
Roof	Beams*	4 x 6	3 X 6 ⁷ / ₈	3½ X 5½

Minimum Width by Depth in Inches See IBC 2018 2304.11 or IBC 2015 602.4 for Details

*3" nominal width allowed where sprinklered



Type IV Minimum Sizes – Floor/Roof Panels

Floor Panels/Decking:

- 4" thick CLT (actual thickness)
- 4" NLT/DLT/GLT (nominal thickness)
- 3" thick (nominal) decking covered with: 1" decking <u>or</u> 15/32" WSP <u>or</u> ½" particleboard

Roof Panels/Decking:

- 3" thick CLT (nominal thickness)
- 3" NLT/DLT/GLT (nominal thickness)
- 2" decking (nominal thickness)
- 1-1/8" WSP





MT Type IV Minimum Sizes – Walls

Exterior Walls for Type IV-A B C

• CLT or Non-combustible

Exterior Walls for Type IV-HT

- CLT or FRTW or Non-combustible
- IBC 2018 6" Thick Wall (FRTW or CLT)
- IBC 2021 4" Thick <u>CLT</u>



MT Type IV Minimum Sizes – Walls

MT Interior Walls in all Type IV:

- Laminated construction 4" thick
- Solid wood construction min. 2 layers of 1" matched boards

Other Interior Walls in Type IV A,B,C

- Non-combustible (0 hr for nonbearing) Other Interior Walls in Type IV HT
- Non-combustible (1 hr min)
- Wood stud wall (1 hr min)

Verify other code requirements for FRR (eg. interior bearing wall; occupancy separation)



Type IV-A Fire Resistance Ratings (FRR)

FRR Examples:

Primary Structural Frame (Beam, Column, Bearing Wall): <mark>3 HR Required</mark>

NC protection = at least 120 min

Use 3 layers of 5/8" type X Gypsum = 120 min (2 HR)
 Mass Timber FRR req'd = 3 HR – 2 HR = 1 HR





Type IV-A Fire Resistance Ratings (FRR)

FRR Examples:

Floor Panels:

2 HR Required

NC Protection = at least 80 min

- Use 2 layers of 5/8" type X Gypsum = 80 min (1.33 HR), plus:
 - Mass Timber FRR req'd = 2 HR 1.33 HR = 0.67 HR, or
- Use 3 layers of 5/8" Type X Gypsum = 120 min (2 HR) and <u>no FRR from MT</u>req'd



IV-A



Type IV-A Protection





Floor Surface Protection

Roof Construction Protection

Ext Wall Protection

Min. 1 inch of NC protection

Min. 2 layers 5/8" type X gyp on inside face

Min. 1 layer 5/8" type X gyp on outside face Min. 2 layers 5/8" type X gyp on inside face (non-brng) Min. 3 layers 5/8" type X gyp on inside face (brng)



Type IV-A Fire Resistance Ratings (FRR) IV-A

FRR & NC Floor Panel Example: 2 HR



Type IV-A Fire Resistance Ratings (FRR)

Primary Frame (3 HR) + Floor Panel Example (2 HR):



IV-A

How do you determine FRR of MT?

- 2 Options:
- 1. Calculations in Accordance with IBC 722 → NDS Chapter 16
- 2. Tests in Accordance with ASTM E119





Fire exposed surface

Unexposed surface

MT FRR Calculations Method:

- IBC 703.3 allows several methods of determining FRR. One is calculations per 722.
- 722.1 refers to NDS Chpt 16 for exposed wood FRR

703.3 Methods for determining fire resistance. The application of any of the methods listed in this section shall be based on the fire exposure and acceptance criteria specified in ASTM E119 or UL 263. The required *fire resistance* of a building element, component or assembly shall be permitted to be established by any of the following methods or procedures:

3. Calculations in accordance with Section 722.

722.1 General. The provisions of this section contain procedures by which the *fire resistance* of specific materials or combinations of materials is established by calculations. These procedures apply only to the information contained in this section and shall not be otherwise used. The calculated *fire resistance* of concrete, concrete masonry and clay masonry assemblies shall be permitted in accordance with ACI 216.1/TMS 0216. The calculated *fire resistance* of steel assemblies shall be permitted in accordance of steel assemblies shall be permitted in accordance with Chapter 5 of ASCE 29. The calculated *fire resistance* of exposed wood members and wood decking shall be permitted in accordance with Chapter 16 of ANSI/AF&PA National Design Specification for Wood Construction (NDS).



NDS Chapter 16 includes calculation of fire resistance of NLT, CLT, Glulam, Solid Sawn and SCL wood products

Table 16.2.1B Effective Char Depths (for CLT

with β_n =1.5in./hr.)

Required Fire	Effective Char Depths, a _{char} (in.)									
Endurance			lami	nation	thickn	esses, h	_{lam} (in.)			
(hr.)	5/8	3/4	7/8	1	1-1/4	1-3/8	1-1/2	1-3/4	2	
1-Hour	2.2	2.2	2.1	2.0	2.0	1.9	1.8	1.8	1.8	
1 ¹ / ₂ -Hour	3.4	3.2	3.1	3.0	2.9	2.8	2.8	2.8	2.6	
2-Hour	4.4	4.3	4.1	4.0	3.9	3.8	3.6	3.6	3.6	

Nominal char rate of 1.5"/HR is recognized in NDS. Effective char depth calculated to account for duration, structural reduction in heat-affected zone



Table 16.2.1AChar Depth and Effective CharDepth (for $\beta_n = 1.5$ in./hr.)

Required Fire Resistance	Char Depth, a _{char}	Effective Char Depth, a _{eff}
(hr.)	(in.)	(in.)
1-Hour	1.5	1.8
1 ¹ / ₂ -Hour	2.1	2.5
2-Hour	2.6	3.2

Table 16.2.1B Effective Char Depths (for CLT

with β_n =1.5in./hr.)

Required Fire Endurance (hr.)	Effective Char Depths, a _{char} (in.) lamination thicknesses, h _{lam} (in.)								
	5/8	3/4	7/8	1	1-1/4	1-3/8	1-1/2	1-3/4	2
1-Hour	2.2	2.2	2.1	2.0	2.0	1.9	1.8	1.8	1.8
1 ¹ / ₂ -Hour	3.4	3.2	3.1	3.0	2.9	2.8	2.8	2.8	2.6
2-Hour	4.4	4.3	4.1	4.0	3.9	3.8	3.6	3.6	3.6

Structural capacity check performed on remaining section, with stress increases



Credit: Forest Products Laboratory

Table 16.2.2 Adjustment Factors for Fire Design¹

			ASD					
0			Design Stress to Member Strength Factor	Size Factor ²	Volume Factor ²	Flat Use Factor 3	Beam Stability Factor ³	Column Stability Factor ³
Bending Strength	Fb	х	2.85	$\mathbf{C}_{\mathbf{F}}$	C_V	Cfs	CL	
Beam Buckling Strength	\mathbf{F}_{bE}	х	2.03	-	-		•	
Tensile Strength	Ft	x	2.85	$C_{\rm F}$	2	1	-	- 22
Compressive Strength	Fc	x	2.58	$\mathbf{C}_{\mathbf{F}}$			3 3 3	CP
Column Buckling Strength	F _{cE}	х	2.03	2	-	14	121	523

 $a_{char} = \beta_{t} t^{0.813}$ Solid Sawn, Glulam, SCL $a_{char} = n_{lam} h_{lam} + \beta_{t} \left(t - \left(n_{lam} t_{gi} \right) \right)^{0.813}$ CLT

a_{eff} = 1.2a_{char} Effective Char Depth

Tested Assemblies Method:

 Many successful Mass Timber ASTM E119 fire tests have been completed by industry & manufacturers



Fire-Resistive Design of Mass Timber Members

Code Applications, Construction Types and Fire Ratings

Hichard McLam, PK, SE + Senter Technical Director + Moodelotts Soci118mmertan, PRC, PE, SE + Senter Technical Director + Woodelocite

For many years, exposed heavy timber framing elements have been permitted in U.S. buildings due to their inherent fre-resistance properties. The predictability of wood's char rate has been well-established for decades and has long been recognized in building codes and trandards.

Today, one of the exciting trends in building design is the growing use of mast timber—i.e., large sold wood panel products such as cross-laminated timber (Ci,T) and naillaminated timber (Ni,T)—for floor, wall and not construction. Like heavy timber, mass timber products have inherent fire resistance that allows them to be left supposed and still schlave a fine-resistance ratio. Because of their strength and dimensional stability, these products also offer a lowcatton ellernative to steel, concrete, and memory for many applications. It is the combination of supposed structure and sheright heat developers and despress across the coerty are leveraging to create innovative designs with a warm yet modern aesthetic, often for projects that go beyond traditional norms of wood design.

This paper has been written to support architects and engineers exploring the use of mass timber for commercial and multi-family construction. It focuses on how to meet fire-resistance requirements in the informational Building Code (IBC), including calculation and testing-based methods. Unless otherwise noted, references refer to the 2018 IBC

Mass Timber & Construction Type

Before demonstrating fre-resistance ratings of exposed mass timber elements, it's important to understand under what documentances the code currently allows the use of mass timber in commercial and multi-family construction.

> A building's assigned construction type is the main indicator of where all when all wood systems can be used. IBC Section 602 defines five main options (Type I shough VI) with all but Type IV having subcategories A and B. Types III and V permit the use of wood framing throughout much of the structure and both are used extensively for modern mass simber buildings.

Type IV SRC 602.3 – Timber elements can be used in floom, nots and interior wals. Fre-netartizer-treated wood IFRTWI framing is permitted in exterior wals with a fremesistance rating of 2 hours or leas.

Type V IBC 602 51 – Timber elements can be used throughout the structure, including foors, roots and both interior and exterior wale.

Type /V IBC 602.0 - Commonly referred to as "Heavy Timber" construction, this option

Mass Timber Fire Design Resource

- Code compliance options for demonstrating FRR
 - Updated as new tests are completed
- Free download at woodworks.org



Municing Structural Engineer
MT Fire Resistance Ratings (FRR)

Inventory of Fire Tested MT Assemblies

Table 1: North American Fire Resistance Tests of Mass Timber Floor / Roof Assemblies

NO.	WoodWorks
-	WOOD PRODUCTS COUNCIL

CLT Pand	Manu lacturer	CLT Grade or Major x Minor Grade	Colling Prototion	Panel Connection in Test	Floor Topping	Load Rating	Fire Resistance Achieved (Hours)	Source	Testing Lab
3-ply CLT (114.0m 4.488.m)	Nordic	619F 1656 Ph 13E MSR 652F 47	2 Japan 1/2" Type X gyprom	Half-Lap	Nutre	Refuced 34% Memorit Capacity	1 E	1 (Test 1)	NRC Fire Laboratory
3-ply CLT (10f nm 4.111 in)	Structurilam	SPF #1/#2 x SPF #1/#2	1 key or 5-9° Type Xgyproon	Half-Lag	New	Roduced 73% Moment Capacity	0.00	1 (Turt 5)	NRC Fire Laboratory
5.ply CLT (113mm+6.875*)	Nonlie	- 10	New	Tepside Splins	2 maggined layers of 1/2 ⁴ cemint bounds	Loaled. Sur Manufacturer	2	2	NRC Fire Laboratory March 2016
5-ply CLT (175mmi 6.875*)	Nesdic	10	1 lay at a 5.4° Type Xgypsum und at 2- channels and farring strips with 5.5.9° (framelics) batts	Tops ide Splime	2 stagg and layers of 1/2° censor (boards	Loaled, Sar Manufacturer	2	5	NRC Fire Laboratory Nov 2014
5-ply CLT (175mm6375*)	Nordie	ы	None	Topside Spline	3/4 in propriating gyperits over Mexicon acountical mar	Reduced 50% Moment Capacity	1.8	3	UL
5-ply CLT (175mm6.375°)	Nordie	11	1 layar 3/4° normal gypram	Topside Spline	3/4 in propriating gypends over Maxion accustical mat or propriating sound board	Reduced 50% Manual Capacity	2	- x	UL
3-ply CLT (175mm#-375*)	Nordie	н	1 Japar 53* Type X Gyp states Real-last Channel under 7 29* 5 Joint with 3 12* Mineral Want bewenn Joint	Statt-Lap	Staff-Lap None Leaded, 3		21	Intertek 8/24/2012	
5-p3y CLT (175mm4.875*)	Structure	E1 M5 MSR 2199 x 5PF #2	Near	Topside Spline	1-1-2" Maxim Cyp-Gate 2000 over Mexcen Relationing Mash	Londod, See Manufacturer	2.5		Intertek, 2/22/2016
5-pty-CUT (175mm6.875*)	DR Johnson	vi	Netw	Half-Lap & Topside Spline			2	7	SwRI (May 2016)
3-93y (L.T (173mm#375*)	Number	SPF1850FbMSR x SPF83	Notes	Half-Lap	Half-Lap None Robust 13		I (Tot 3)	NRC Fire Laboratory	
5-p3y 4LT (175mm-6.825*)	Structure	30F #1.92 x 50F #1.92	1 layur 3/8° Type Xgypsam	Half-Lep	Namy	Uninford 101% Momant Capacity	2	1 (Tel I)	NRC Fire Laboratory
7-ply CLT (245mm 9.65*)	Structurian	SPE #1.42 x SPE #1.42	Now	Half-Lap	Nine	Unriduced 101% Manual Capacity	2.6	1 (Tent T)	NRC Fire Laboratory
5-ply-CLT (173mm+6.875*)	SmartLam	3L-144	New	Half-Lap	neminal 1/2° plywood with #d nails,	Lo aloit. Sio Menufacturet	2	12 (Tet 4)	Western Fire Center 10/26/2016
3-ply CLT (175mmil: 375*)	SeartLas	vi	New	Hulf-Lap	neminal 12*plymod with Eduals.	Loraled. Sor Montfactures	2	12(Tet 3)	Western Fire Center 10/28/2016
5-plyCLT (175mm+375*)	DR. Jok news	×1	Noter	Half-Cap	nominal 1/2" plywood with 8d nails.	Loaded. Sw Manufacturei	2	12(Tot 6)	Western Fire Center 11/01/2016
Septy CLT	6131	CV3MI	Notes	theit-Lap de	Note	Localed,		13	SwRJ

Materials Permitted

602.4 Type IV. Type IV construction is that type of construction in which the building elements are mass timber or noncombustible materials and have fire resistance ratings in accordance with Table 601. Mass timber elements shall meet the fire resistance rating requirements of this section based on either the fire resistance rating of the noncombustible protection, the mass timber, or a combination of both and shall be determined in accordance with Section 703.2 or 703.3. The minimum dimensions and permitted materials for building elements shall comply with the provisions of this section and Section 2304.11. Mass timber

Exterior load-bearing walls and nonload-bearing walls shall be mass timber construction, or shall be of noncombustible construction.

Exception: Type IV-HT Construction in accordance with Section 602.4.4.

The interior building elements, including nonload-bearing walls and partitions, shall be of mass timber construction or of noncombustible construction.

Exception: Type IV-HT Construction in accordance with Section 602.4.4..

Type IV-B



12 STORIES BUILDING HEIGHT ALLOWABLE BUILDING AREA 648,000 SF AVERAGE AREA PER STORY 54,000SF

180 FT

TYPE IV-B





Credit: Susan Jones, atelierjones

Credit: LEVER Architecture

Type IV-B Height and Area Limits

		-	-		14.
				1	
	1000	TAXABLE PARTY.	-		
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IV-B

12 STORIES BUILDING HEIGHT 180 FT ALLOWABLE BUILDING AREA 648,000 SF AVERAGE AREA PER STORY 54,000SF

TYPE IV-B

Credit: Susan Jones, atelierjones

Occupancy	# of Stories	Height	Area per Story	Building Area
A-2	12	180 ft	90,000 SF	270,000 SF
В	12	180 ft	216,000 SF	648,000 SF
Μ	8	180 ft	123,000 SF	369,000 SF
R-2	12	180 ft	123,000 SF	369,000 SF

Areas exclude potential frontage increase

In most cases, Type IV-B height & story allowances = Type I-B height & story allowances

Type IV-B area = 2 * Type IV-HT area





12 STORIES BUILDING HEIGHT 180 FT ALLOWABLE BUILDING AREA 648,000 SF AVERAGE AREA PER STORY 54,000SF

TYPE IV-B

Credit: Susan Jones, atelierjones



NC protection on all surfaces of Mass Timber except limited exposed areas ~20% of Ceiling or ~40% of Wall can be exposed

Type IV-B Fire Resistance Ratings (FRR) IV-B 2 Hour Floor Frame **Primary Frame FRR** 2 HR (1 HR at Roof) Hour **2 HR Ext or Int Bearing Wall FRR 2 HR** 2 **Floor Construction FRR 1 HR Roof Construction FRR** 2 Hour Floor

Credit: Kaiser+Path

Type IV-B Fire Resistance Ratings (FRR)

	*Applicable to locations. Limit exposed MT pe	ed	
	FRR	Min. NC Protection	
Primary Frame FRR	2 HR (1 HR at Roof)	80 min* (40 min* at Roof)	
Ext or Int Bearing Wall FRR	2 HR	80 min*	
Floor Construction FRR	2 HR	80 min*	
Roof Construction FRR	1 HR	40 min*	

 $\frac{1}{2}$ " Type X Gypsum = 25 min | 5/8" Type X Gypsum = 40 min



IV-B

Type IV-B Protection





Floor Surface Protection

Roof Construction Protection

Ext Wall Protection

Min. 1 inch of NC protection

Min. 1 layer 5/8" type X gyp on inside face*

Min. 1 layer 5/8" type X gyp on outside face Min. 2 layers 5/8" type X gyp on inside face*

*Applicable to most locations Limited exposed MT permitted



Type IV-B Fire Resistance Ratings (FRR)

FRR & NC Floor Panel Example: 2 HR

IV-B



*Applicable to most locations. Limited exposed MT permitted

Type IV-B Fire Resistance Ratings (FRR)

Primary Frame (2 HR) + Floor Panel Example (2 HR):



IV-B

Limited Exposed MT allowed in Type IV-B for:

- MT beams and columns which are not integral part of walls or ceilings, no area limitation applies
- MT ceilings and beams up to 20% of floor area in dwelling unit or fire area, <u>or</u>
- MT walls and columns up to 40% of floor area in dwelling unit or fire area, <u>or</u>
- Combination of ceilings/beams and walls/columns, calculated as follows:



IV-B

Credit: Kaiser+Path

Mixed unprotected areas, exposing both ceilings and walls:

In each dwelling unit or fire area, max.
unprotected area =

 $(\mathrm{U_{tc}}/\mathrm{U_{ac}}) + (\mathrm{U_{tw}}/\mathrm{U_{aw}}) \leq 1.0$

- U_{tc} = Total unprotected MT ceiling areas
- U_{ac} = Allowable unprotected MT ceiling areas
- U_{tw} = Total unprotected MT wall areas
- U_{aw} = Allowable unprotected MT wall areas





Design Example: Mixing unprotected MT walls & ceilings



800 SF dwelling unit

- U_{ac} = (800 SF)*(0.20) = 160 SF
- U_{aw} = (800 SF)*(0.40) = 320 SF
- Could expose 160 SF of MT ceiling, <u>OR</u> 320 SF of MT Wall, <u>OR</u>

IV-B

 If desire to expose 100 SF of MT ceiling in Living Room, determine max. area of MT walls that can be exposed

Credit: AWC

Design Example: Mixing unprotected MT walls & ceilings



- $\begin{array}{l} (U_{tc}/U_{ac}) + (U_{tw}/U_{aw}) \leq 1.0 \\ (100/160) + (U_{tw}/320) \leq 1.0 \\ U_{tw} = 120 \; \text{SF} \end{array}$
- Can expose 120 SF of MT walls in dwelling unit in combination with exposing 100 SF of MT ceiling

IV-B

Credit: AWC

Horizontal separation of unprotected areas:

 Unprotected portions of mass timber walls and ceilings shall be not less than 15 feet from unprotected portions of other walls and ceilings, measured horizontally along the ceiling and from other unprotected portions of walls measured horizontally along the floor.



IV-B

Credit: Kaiser+Path

Type IV-C



9 STORIES BUILDING HEIGHT 85' ALLOWABLE BUILDING AREA 405,000 SF AVERAGE AREA PER STORY 45,000 SF

TYPE IV-C



Photos: Baumberger Studio/PATH Architecture/Marcus Kauffman







Credit: Susan Jones, atelierjones

Type IV-C Height and Area Limits

IV-C



9 STORIES BUILDING HEIGHT 85' ALLOWABLE BUILDING AREA 405,000 SF AVERAGE AREA PER STORY 45,000 SF

TYPE IV-C

Credit: Susan Jones, atelierjones

Occupancy	# of Stories			Building Area
A-2	6	85 ft	56,250 SF	168,750 SF
В	9	85 ft	135,000 SF	405,000 SF
Μ	6	85 ft	76,875 SF	230,625 SF
R-2	8	85 ft	76,875 SF	230,625 SF

Areas exclude potential frontage increase

In most cases, Type IV-C height allowances = Type IV-HT height allowances, but add'I stories permitted due to enhanced FRR Type IV-C area = 1.25 * Type IV-HT area

IV-C



9 STORIES BUILDING HEIGHT ALLOWABLE BUILDING AREA 405.000 SF AVERAGE AREA PER STORY 45,000 SF

TYPE IV-C



All Mass Timber surfaces may be exposed

Exceptions: Shafts, concealed spaces, outside face of exterior walls

Ema Peter

Credit: Kaiser+Path,

Credit: Susan Jones, atelierjones

Type IV-C Fire Resistance Ratings (FRR) IV-C 2 Hour Floor 2 Hour Frame ... **Primary Frame FRR** 2 HR (1 HR at Roof) ram **2 HR** Ext or Int Bearing Wall FRR our **2 HR Floor Construction FRR 1 HR Roof Construction FRR**

Same FRR as IV-B, but all MT in IV-C may be

I¥

Credit: Ema Peter

2 Hour Floor

Type IV-C Protection



Type IV-C Fire Resistance Ratings (FRR)

FRR & NC Floor Panel Example: 2 HR

No NC req'd

IV-C





Fire Resistance Ratings (FRR) Recap

		IV-A	IV-B	IV-C	IV-HT
Roof Construction		1.5	1	1	НТ
Primary Frame @ Roof		2	1	1	нт
Floor Construction		2	2	2	нт
Primary Frame		3	2	2	нт
Exterior Bearing Walls		3	2	2	2
Interior Bearing Walls		3	2	2	1 or HT

Required Fire Resistance Rating in Hours (per Table 601 only)

Noncombustible Protection (NC) Recap



Credit: PATH Architecture

Credit: LEVER Architecture

Photo: Blaine Brownell

Interior Wall Construction Recap



*IBC 2021 requires at least 1 Hr FRR for HT walls supporting 2 levels

Exterior Wall Construction Recap

	IV-A	IV-B	V-C	IV-	HT	
					IBC 2021	IBC 2018
Fire Rating (bearing wall)		3 Hr	2 Hr	2 Hr	2 Hr	2Hr
Mass Timber		Mass Timber/CLT		4" min thick <u>CLT</u> *	6" <u>Wall</u> *	
Exterior NC Protection		40 Min NC & No Exterior Combustible Coverings		FRT Sheathing,	Gyp or other NC	
Interior NC Protection		Per Interior Requirements			Not R	equired
Light Frame FRTW		No			Yes*	6" Wall*

*Changes in IBC 2015, 2018, and 2021 editions

Concealed Spaces in Type IV

What if I have a dropped ceiling? Can I have a dropped ceiling?

• Impact on FRR, NC placement, sprinkler requirements



Concealed Spaces in Type IV

Previous Type IV (now IV-HT) provisions prohibited concealed spaces



Concealed Spaces in Type IV

Type IV-HT (IBC 2021) permits concealed spaces where one of the following conditions exists:

- 1. The building is sprinklered throughout with an NFPA 13 Sprinkler and automatic sprinklers are provided in the concealed space.
- 2. The concealed space is completely filled with noncombustible insulation.
- Surfaces within the concealed space are fully sheathed with not less than 5/8" Type X gypsum.

Concealed spaces within interior walls and partitions with a one hour or greater fire resistance rating complying Section 2304.11.2.2 do not require additional protection.

Concealed Spaces in Type IV-HT





Option 2 Noncombustible insulation

5/8" Type X gypsum
on all MT surfaces

Option 1

Sprinklers in concealed spaces



Concealed Spaces in Type IV-A, IV-B, IV-C

New IV-HT concealed space provisions do not apply to IV-A, IV-B or IV-C

But, can still have concealed spaces in IV-A, IV-B, IV-C:

- <u>IV-A and IV-B</u>: Combustible construction forming concealed spaces protected with NC of 80 minutes (2 layers of 5/8" Type X Gypsum)
- <u>IV-C:</u> Combustible construction forming concealed spaces protected with NC of 40 minutes (1 layer of 5/8" Type X Gypsum)





Concealed Spaces in Type IV-A, IV-B



Concealed Spaces in Type IV-C



Tall Wood Shaft Enclosures

- When can shaft enclosures be MT?
- What FRR requirements exist?
- If shaft enclosure is MT, is NC req'd?







Tall Wood Shaft Enclosures



2 HR (not less than FRR of floor assembly penetrated, IBC 713.4)

DOES TALL WOOD = HIGH RISE?

Photo: Ema Peter
Mid-Rise vs. High-Rise



FIGURE 6-6 Determination of high-rise building

Sprinklers in High Rises

Two Water Mains Required if:
Building Height Exceeds 420 ft, or
Type IV-A and IV-B buildings that exceed 120 ft in height

ADDRESSING CLT CHAR FALL OFF

CLT Fire Performance – Char Fall Off

CLT char fall off or heat induced delamination occurs when laminations (or pieces thereof) fall off the underside of a CLT panel under extended fire conditions.



CLT Fire Performance – Fire Re-Growth

In tall buildings, preventing fire re-growth is key. Fire re-growth is a phenomenon in which the heat-release rate of a fire intensifies following a decay phase. Fire re-growth can be initiated when delamination occurs, as this exposes un-charred wood surfaces, thereby resulting in an influx of fuel available for consumption by the fire.





CLT Fire Performance – Char Fall Off

Facts about CLT char fall off:

- Only an item to consider in tall buildings. Important to avoid in high-rise construction where required performance is containment of fire within compartment of origin with no sprinkler or fire service suppression
- Not applicable when discussing mid-rise mass timber (or any building under types II, III, IV-HT or V)
- Largely a function of adhesive performance under high temps
- Has been addressed in PRG 320-18 (required for all CLT under 2021 IBC, not just tall wood)



CLT Fire Performance – PRG 320

2021 IBC Section 602.4 added:

Cross-laminated timber shall be labeled as conforming to PRG 320 - 18 as referenced in Section 2303.1.4.



Standard for Performance-Rated Cross-Laminated Timber

CAN MATIOMAL STANDARS

ANSI/APA PRG 330-2018





CLT Fire Performance – PRG 320

PRG 320 is manufacturing & performance standard for CLT. 2018 edition (referenced in 2021 IBC) added new elevated temperature adhesive performance requirements validated by fullscale and medium-scale qualification testing to ensure CLT does not exhibit fire re-growth

When designing tall wood – specify CLT per PRG 320-18 (req'd in IBC 2021 for all CLT)



ANNEX B. PRACTICE FOR EVALUATING ELEVATED TEMPERATURE PERFORMANCE OF ADHESIVES USED IN CROSS-LAMINATED TIMBER (MANDATORY)

CONNECTIONS IN TALL WOOD

In Construction Types IV-A, IV-B & IV-C, building elements are required to be FRR as specified in IBC Tables 601 and 602. Connections between these building elements must be able to maintain FRR no less than that required of the connected members.



16.3 Wood Connections

Wood connections, including connectors, fasteners, and portions of wood members included in the connection design, shall be protected from fire exposure for the required fire resistance time. Protection shall be provided by wood, fire-rated gypsum board, other approved materials, or a combination thereof.

Many ways to demonstrate connection fire protection: calculations, prescriptive NC, test results, others as approved by AHJ



2017 Glulam Beam to Column Connection Fire Tests under standard ASTM E119 time-temperature exposure







Fire Test Results

Test	Beam	Connector	Applied Load	FRR	
1	8.75" x 18" (222mm x 457mm)	1 x Ricon S VS 290x80	3,905lbs (17.4kN)	1hr	
2	10.75" x 24" (273mm x 610mm)	Staggered double Ricon S VS 200x80	16,620lbs (73.9kN)	1.5hrs	
3	10.75" x 24" (273mm x 610mm)	1 x Megant 430	16,620lbs (73.9kN)	1.5hrs	

Softwood Lumber Board Glulam Connection Fire Test Summary Report

Issue | June 5, 2017

Full Report Available at:

https://www.thinkwood.com/wp-content/uploads/2018/01/reThink-Wood-Arup-SLB-Connection-Fire-Testing-Summary-web.pdf

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FIRE PERFORMANCE EVALUATION OF A LOAD BEARING GLULAM BEAM TO COLUMN CONNECTION, INCLUDING A CLT PANEL, TESTED IN GENERAL ACCORDANCE WITH ASTM E119-16a, STANDARD TEST METHODS FOR FIRE TESTS OF BUILDING CONSTRUCTION AND MATERIALS

FINAL REPORT Consisting of 32 Pages

PENETRATIONS IN TALL WOOD

Although not a new code requirement or specific to tall wood, more testing & information is becoming available on firestopping of penetrations through MT assemblies



Most firestopping systems include combination of fire safing (eg. noncombustible materials such as mineral wool insulation) plus fire caulk





Inventory of Fire Tested Penetrations in MT Assemblies

Table 3: North American Fire Tests of Penetrations and Fire Stops in CLT Assemblies

CLT Panel	Exposed Side Protection	Pen etrating Item	Penetrant Centered or Offset in Hole	Firestopping System Description	F Rating	T Rating	Stated Test Protocal	Source	Testing Lab
3-ply (78mm 3.07*)	None	1.5° diameter data cable bunch	Centered	3.5 in diameter hole. Mineral wool was installed in the 1in, annular space around the data cables to a total depth of approximately 2 - 5/64 in. The remaining 1in, annular space from the top of the mineral wool to the top of the floor assembly was filled with Hilti FS-One Max caulking.	1 hour	0.5 hour	CANULC S115	26	Intertek March 30, 201
3-ply (78mm3.07*)	None	2" copper pipe	Centered	4.375 in diameter hole. Pipe wrap was installed around the copper pipe to a total depth of approximately 2 - 5/64in. The remaining lin. annular space starting at the top of the mineral wool to the top of the floor assembly was filled with Hilti FS-One Max caulking.	1 hour	NA.	CANULC S115	26	In tert ek March 30, 201
3-ply (78mm3.07*)	None	2.5" sch ed. 40 pipe	Centered	4.92 in diameter hole. Pipe wrap was installed around the schedule 40 pipe to a total depth of approximately 2 - 5/64 in. The remaining 1 in . annular space starting at the top of the pipe wrap to the top of the floor assembly was filled with HiltiFS-One Max caulking.	1 hour	NA.	CANULC \$115	26	In tertek March 30, 201
3-ply (78mm 3.07*)	None	6* cast iron pipe	Centered	8.35 in diameter hole. Mineral wool was installed in the lin. annular space around the cast iron pipe to a total depth of approximately 2 – 5/64 in. The remaining lin. annular space starting at the top of the pipe wap to the top of the floor assembly was filled with Hilt iFS-One Max caulking.	1 hour	NA.	CANULC S115	2.6	Intertek March 30, 201
3-ply (78mm3.07*)	None	Hilti 6 in drop in device. System No.: F-B-2049	Centered	9.01" diameter hole. Mineral wool was installed in the 1 – 1/4in. annular space around the drop-in device to a total depth of approximately 1 – 7/64in and the remaining 1 in. annular space from the top of the mineral wool to the top edge of the 9 – 1/64in. hole in the CLT was filled with Hilti FS-One Max caulking.	1 hour	0.75 hour	CANULC S115	26	In tert ek March 30, 201
5-ply CLT 131 mm 5.16*)	None	1.5* diameter data cable bunch	Centered	3.5° diameter hole. Mineral wool was installed in the 1 in. annular space around the data cables to a total depth of approximately 4 - 5/32 in. The remaining 1 in. annular space from the top of the mineral wool to the top of the floor assembly was filled with Hilti FS-One Max caulking.	2 hours	1.5 hours	CANULC S115	2.6	Interiek March 30, 201
5-ply CLT 131mm 5.16*)	None	2" copper pipe	Centered	4.375 in diameter hole. Pipe wrap was installed around the copper pipe to a total depth of approximately 4 - 5/32 in. The remaining 1 in. annular space starting at the top of the mineral wool to the top of the floor assembly was filled with Hilti FS-One Max caulking.	2 hours	N.A.	CANULC \$115	26	Intertek March 30, 201
5-ply CLT 131 mm 5.16*)	None	2.5* sch ed. 40 pip e	Centered	4.92 in diameter hole. Pipe wrap was installed around the schedule 40 pipe to a total depth of approximately 4 – 5/32 in. The remaining 1 in annular space starting at the top of the pipe wrap to the top of the floor assembly was filled with HiltiFS-One Max caulking.	2 hours	0.5 hour	CANULC S115	26	Intertek March 30, 201
5-ply CLT 131 mm 5.16*)	None	6° cast iron p ipe	Centered	8.35 in diameter hole. Mineral wool was installed in the lin. annular space around the cast iron pipe to a total depth of approximately 4 – 5/32 in. The remaining lin. annular space starting at the top of the pipe wrap to the top of the floor assembly was filled with Hilt i FS-One Max caulking.	2 hours	NA.	CANULC \$115	2.6	Intertek March 30, 201
5-ply CLT 131 mm 5.16*)	None	Hilti 6 in drop in device. System No.: F-B-2049	Centered	9.01" diameter hole. Mineral wool was installed in the 1 - 1/4in. annular space around the drop-in device to a total depth of approximately 1 - 7/64in and the remaining 1 in. annular space from the top of the mineral wool to the top edge of the 9 - 1/64in. hole in the CLT was filled with Hilti FS-One Max caulking.	2 hours	1.5 hours	CANULC S115	26	In tert ek March 30, 201
5-ply 75mm6-875*)	None	l* nominal PVC pipe	Centered	4.21 in diameter with a 3/4 in plywood reducer flush with the top of the slab reducing the opening to 2.28 in. Two wraps of Hilti CP 648-E W45/1-3/4" Firestop wrap strip at two locations with a 30 gauge steel sleeve which extended from the top of the slab to 1 in below the slab. The first location was with the bottom of the wrap strip flush with the bottom of the steel sleeve and the second was with the bottom of the wrap strip 3 in. from the bottom of the slab. The void between the steel sleeve and the CLT and between the steel sleeve and pipe at the top was filled with Roxul Safe mineral wool leaving a 3/4 in deep void at the top of the assembly. Hilti FS-One Max Intumescent Firestop Sealant was applied to a depth of 3/4 in on the top of the assembly between the plywood and steel sleeve as well as the steel sleeve and pipe.	2 hours	2 hours	ASTM E814	24	QAI Laboratori March 3, 201
	-								



SEALANTS AT MT PANEL EDGES



Sealants at MT Panel Edges

703.9 Sealing of adjacent mass timber elements. In buildings of Type IVA, IVB, and IVC construction, sealant or adhesive shall be provided to resist the passage of air in the following locations:

- At abutting edges and intersections of mass timber building elements required to be fire resistance-rated
- At abutting intersections of mass timber building elements and building elements of other materials where both are required to be fire resistance-rated.



Sealants at MT Panel Edges

Sealants shall meet the requirements of ASTM C920 (elastomeric joint sealants). Adhesives shall meet the requirements of ASTM D3498 (gap filling construction adhesives, i.e. not fire caulk).

Exception: Sealants or adhesives need not be provided where they are not a required component of a fire resistance- rated assembly.



Sealants at MT Panel Edges

Several MT fire tested assemblies have successfully been completed w/o adhesives/sealants at abutting panel edges

2021 IBC will require periodic special inspections of adhesive/sealant installation (when required to be installed)



Occupancy Separation

Protection of MT used for occupancy separation

Addition to IBC 508.4.4.1 requires:

Mass timber elements serving as fire barriers or horizontal assemblies to separate occupancies in Type IV-B or IV-C construction shall be separated from the interior of the building with a minimum of ½" gypsum board or a noncombustible equivalent.



Incidental Use Separation

Protection of MT used for incidental use separation

New section 509.4.1.1 requires:

Where Table 509 specifies a fire- resistancerated separation, mass timber elements serving as fire barriers or a horizontal assembly in Type IV-B or IV-C construction shall be separated from the interior of the incidental use with a minimum of ½" gypsum board or a noncombustible equivalent.



New code provisions in International Fire Code (IFC) address construction fire safety of tall wood buildings

3308.4 Fire safety requirements for buildings of Types IV-A, IV-B, and IV-C construction. Buildings of Types IV-A, IV-B, and IV-C construction designed to be greater than six stories above grade plane shall meet the following requirements during construction unless otherwise approved by the fire code official.

- 1. Standpipes shall be provided in accordance with Section 3313.
- 2. A water supply for fire department operations, as approved by the fire chief.



IFC 3313 Standpipe Requirements

SECTION 3313 STANDPIPES

3313.1 Where required.

In buildings required to have standpipes by Section 905.3.1, not less than one standpipe shall be provided for use during construction. Such standpipes shall be installed prior to construction exceeding 40 feet (12 192 mm) in height above the lowest level of fire department vehicle access. Such standpipe shall be provided with fire department hose connections at accessible locations adjacent to usable stairways. Such standpipes shall be extended as construction progresses to within one floor of the highest point of construction having secured decking or flooring.

3313.2 Buildings being demolished.

Where a building is being demolished and a standpipe is existing within such a building, such standpipe shall be maintained in an operable condition so as to be available for use by the fire department. Such standpipe shall be demolished with the building but shall not be demolished more than one floor below the floor being demolished.

3313.3 Detailed requirements.

Standpipes shall be installed in accordance with the provisions of Section 905.

Exception: Standpipes shall be either temporary or permanent in nature, and with or without a water supply, provided that such standpipes comply with the requirements of Section 905 as to capacity, outlets and materials.

IFC 3308.4 Cont'd

- 3. Where building construction exceeds six stories above grade plane, at least one layer of noncombustible protection where required by Section 602.4 of the International Building Code shall be installed on all building elements more than 4 floor levels, including mezzanines, below active mass timber construction before erecting additional floor levels.
- 4. Where building construction exceeds six stories above grade plane required exterior wall coverings shall be installed on all floor levels more than 4 floor levels, including mezzanines, below active mass timber construction before erecting additional floor level.

Exception: Shafts and vertical exit enclosures





Figure 1

Figure 2

Examples of Protection During Construction For Mass Timber Buildings Greater Than 6 Stories Above Grade Plane

QUESTIONS?

Speaker name

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