



Taller with Timber: New Code Provisions and Design Steps for Tall Wood Buildings

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Photo: Kaiser+Path

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Questions related to specific materials, methods, and services will be addressed at the conclusion of this presentation.



Course Description

We are at an exciting confluence in timber construction. The need for sustainable, urban construction has never been higher. Concurrently, mass timber products such as cross-laminated timber have opened the door to many new opportunities for construction, one of which is tall wood. In January 2019, the International Code Council (ICC) approved a set of proposals to allow tall wood buildings of up to 18 stories as part of the 2021 International Building Code (IBC). This presentation will introduce the new tall wood code provisions in depth. Starting with a review of the technical research and testing that supported their adoption, it will then take a detailed look at the new code provisions and methods of addressing the new requirements. Topics will include fire-resistance ratings and allowances for exposed timber, penetrations, sprinklers, connections, exterior walls and much more. Designers can expect to take away the knowledge they need to start exploring tall wood designs on their projects.

Learning Objectives

1. Review the global history of tall wood construction and highlight the mass timber products used in these structures.
2. Explore the work and conclusions of the ICC Ad Hoc Committee on Tall Wood Buildings in establishing 14 new code provisions for the 2021 IBC that address tall wood construction.
3. Discuss code-compliant options for exposing mass timber, where up to 2-hour fire-resistance ratings are required, and demonstrate design methodologies for achieving these ratings.
4. Review code requirements unique to tall wood buildings, focusing on items such as sprinklers, shaft construction and concealed spaces.

Questions we'll answer:

- What is tall wood?
- What are the new tall wood code provisions?
- How much timber can be exposed
- How do you design for fire-resistance (exposed & protected)
- What do I need to know about acoustics in tall timber?
- What do the connections & details look like (and how does fire impact them)



GLOBAL TALL WOOD CIRCA 2015

7-14 STORIES

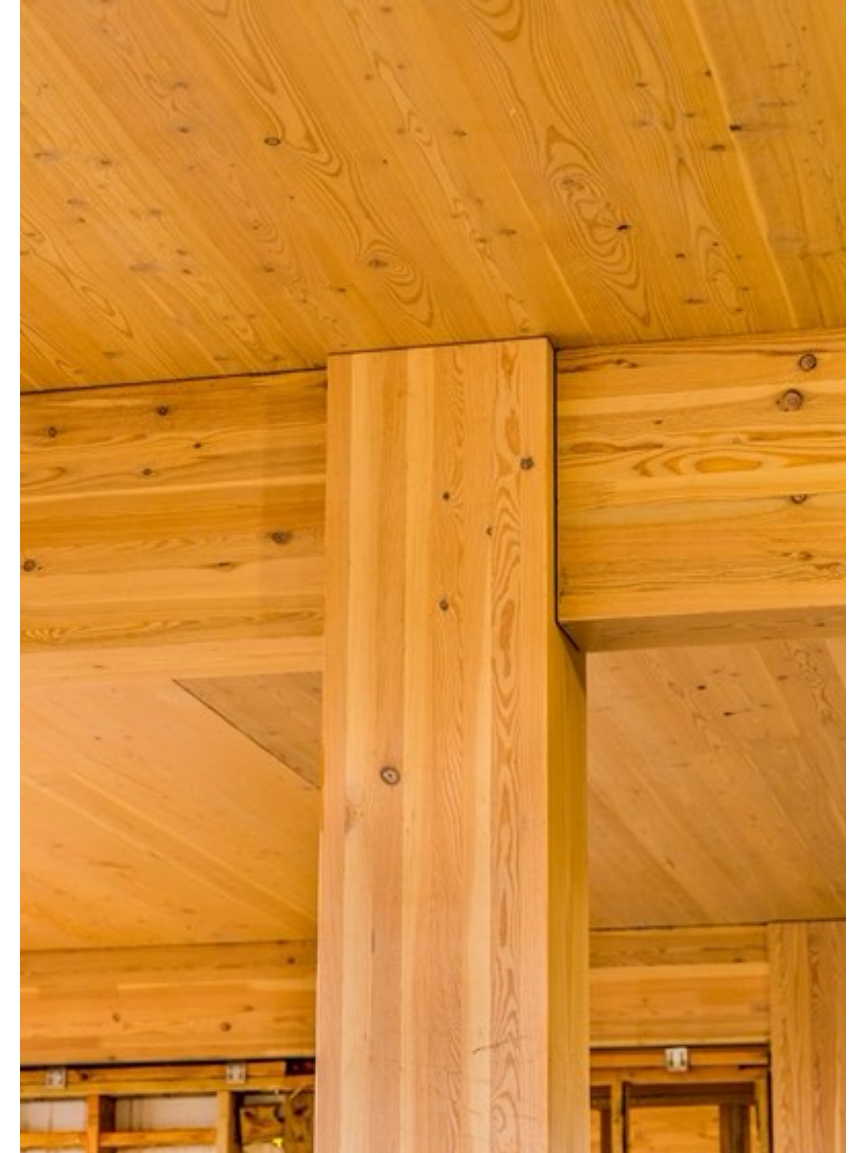


GLOBAL TALL WOOD CIRCA 2019

18-24 STORIES



TALL WOOD IN THE US CIRCA 2019



8 STORIES

Photos: Baumberger Studio/PATH Architecture/Marcus Kauffman | Architect: PATH Architecture

GLULAM



Photos: APA

CROSS-LAMINATED TIMBER (CLT)



NAIL-LAMINATED TIMBER (NLT)



Photo: Think Wood



Photo: StructureCraft



Photo: LendLease

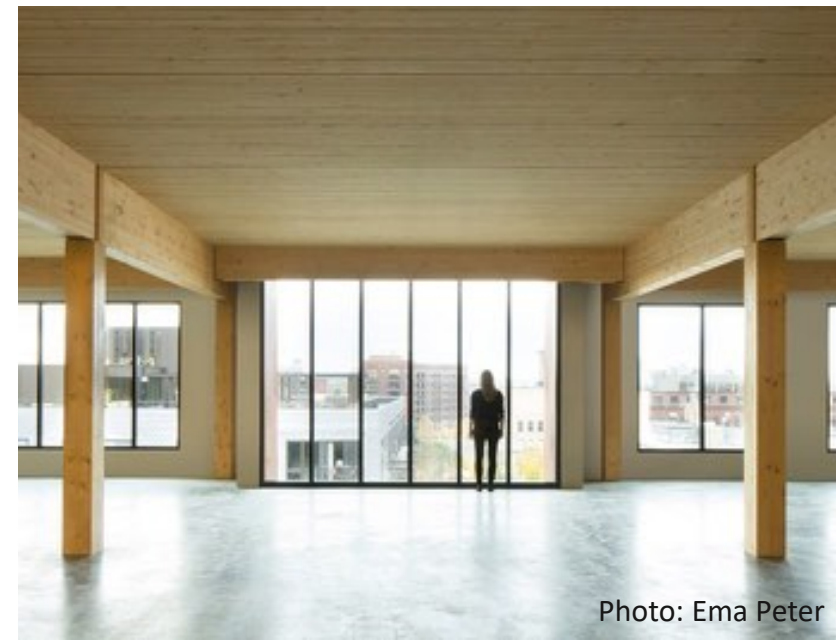


Photo: Ema Peter

DOWEL-LAMINATED TIMBER (DLT)



Photo: StructureCraft

MASS PLYWOOD PANELS (MPP)



Photo: WoodWorks

DECKING



Photo: StructureCraft



Photo: LEVER Architecture



Photo: Bernard André Photography



TALL WOOD IN THE U.S.

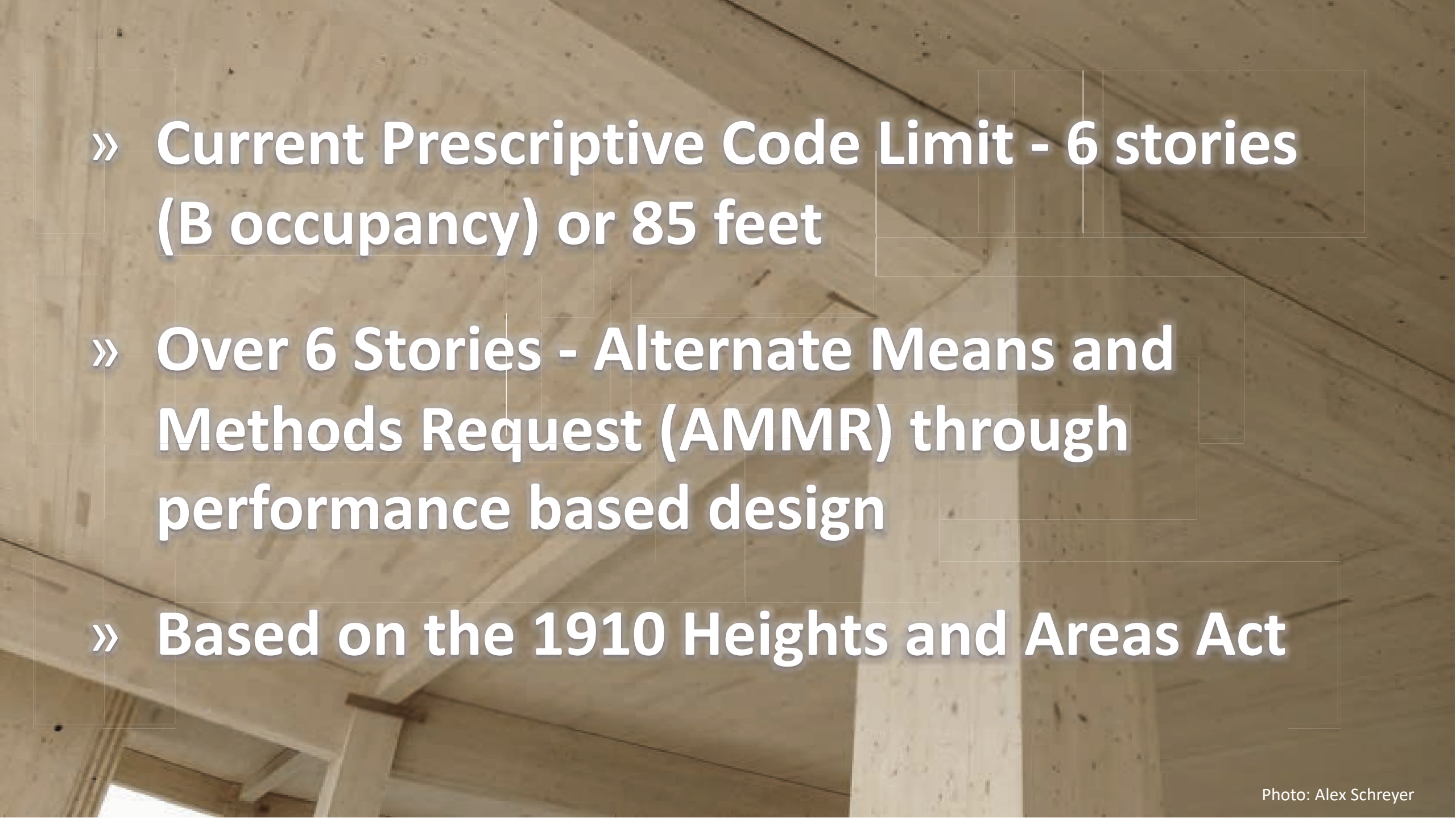
- 
- » **Current Prescriptive Code Limit - 6 stories (B occupancy) or 85 feet**
 - » **Over 6 Stories - Alternate Means and Methods Request (AMMR) through performance based design**
 - » **Based on the 1910 Heights and Areas Act**



Photo: Blaine Brownell



Photo: Christian Columbres



ICE Block I, RMW Architecture & Interiors, Buehler Engineering, Bernard André Photography



Photo: Swinerton

U.S. TALL WOOD DEVELOPMENT AND CHANGES

Interest in tall wood projects in the US was rapidly increasing. Some building officials were reluctant to approved proposed plans, primarily due to lack of code direction and precedent



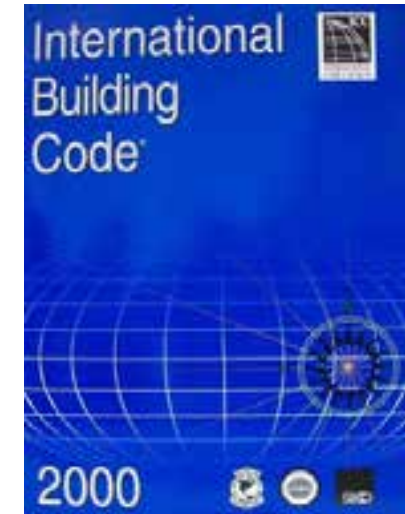
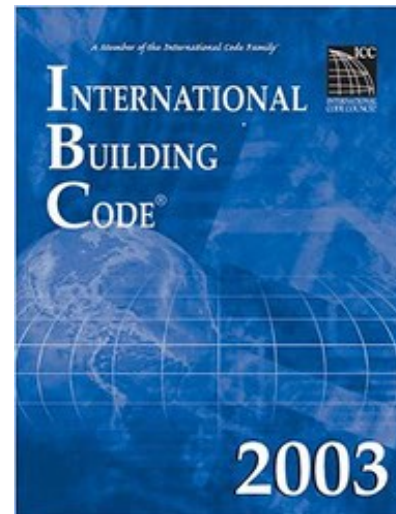
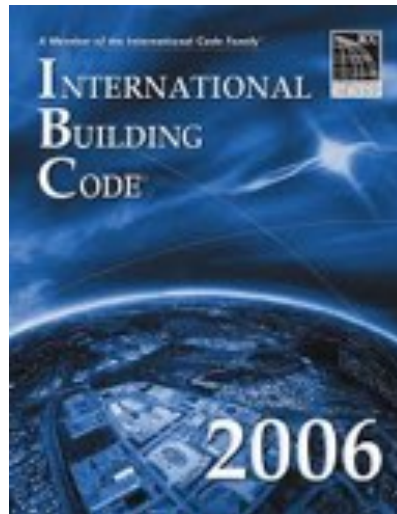
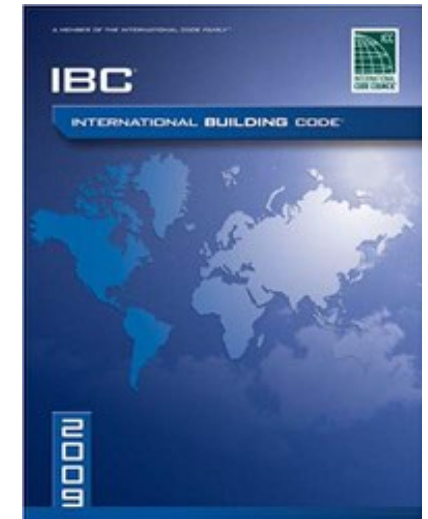
Empire State Building, New York City, New York, 1931



Photo: Seagate Mass Timber Inc
Pollux Chang Photographer

UBC Brock Commons Student Residence, Vancouver, British Columbia, 2018

3 YEAR CODE CYCLE



U.S. TALL WOOD DEVELOPMENT AND CHANGES



In December 2015, the ICC Board established the ICC Ad Hoc Committee on Tall Wood Buildings. Objectives:

1. Explore the building science of tall wood buildings
2. Investigate the feasibility, and
3. Take action on developing code changes for tall wood buildings.



TALL WOOD APPROVED!

Unofficial results posted Dec 19, 2018

Final votes ratified Jan 31, 2019

AWC: Tall Mass Timber code changes get final approval

Dec 19, 2018

LEESBURG, VA. – The International Code Council (ICC) has released the unofficial voting results on code change proposals considered in 2018, including passage of the entire package of [14 tall mass timber code change proposals](#). The proposals create three new types of construction (Types IV-A, IV-B and IV-C), which set fire safety requirements, and allowable heights, areas and number of stories for tall mass timber buildings. Official results are expected to be announced during the first quarter of 2019. The new provisions will be included in the 2021 International Building Code (IBC).

"Mass timber has been capturing the imagination of architects and developers, and the ICC result means they can now turn sketches into reality. ICC's rigorous study, testing and voting process now

2021 IBC Introduces 3 new tall wood construction types:

IV-A, IV-B, IV-C

Previous type IV renamed type IV-HT

BUILDING ELEMENT	TYPE I		TYPE II		TYPE III		TYPE IV				TYPE V	
	A	B	A	B	A	B	A	B	C	HT	A	B

New Building Types



18 STORIES
BUILDING HEIGHT 270'
ALLOWABLE BUILDING AREA 972,000 SF
AVERAGE AREA PER STORY 54,000SF

TYPE IV-A



12 STORIES
BUILDING HEIGHT 180 FT
ALLOWABLE BUILDING AREA 648,000 SF
AVERAGE AREA PER STORY 54,000SF

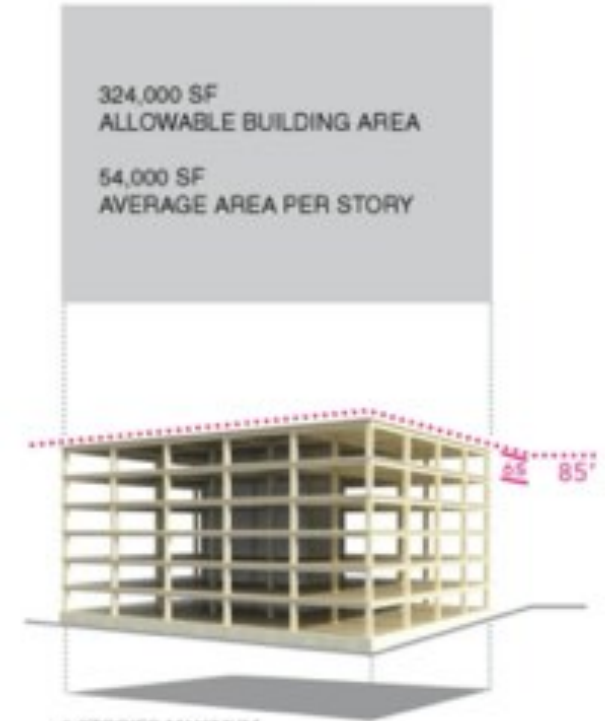
TYPE IV-B



9 STORIES
BUILDING HEIGHT 85'
ALLOWABLE BUILDING AREA 405,000 SF
AVERAGE AREA PER STORY 45,000 SF

TYPE IV-C

IBC 2021



TYPE IV- HT

IBC 2015

BUSINESS OCCUPANCY [GROUP B]

*BUILDING FLOOR-TO-FLOOR HEIGHTS ARE SHOWN AT 12'-0" FOR ALL EXAMPLES FOR CLARITY IN COMPARISON BETWEEN 2015 TO 2021 IBC CODES.

Type IV-C



9 STORIES
BUILDING HEIGHT 85'
ALLOWABLE BUILDING AREA 405,000 SF
AVERAGE AREA PER STORY 45,000 SF

TYPE IV-C



Credit: Susan Jones, atelierjones

Photos: Baumberger Studio/PATH
Architecture/Marcus Kauffman

Type IV-C Protection vs. Exposed

IV-C



9 STORIES
BUILDING HEIGHT 85'
ALLOWABLE BUILDING AREA 405,000 SF
AVERAGE AREA PER STORY 45,000 SF

TYPE IV-C

Credit: Susan Jones, atelierjones



Credit: Kaiser+Path, Ema Peter

All Mass Timber surfaces may be exposed

Exceptions: Shafts, concealed spaces, outside face of exterior walls

Type IV-C Height and Area Limits

IV-C



9 STORIES
BUILDING HEIGHT 85'
ALLOWABLE BUILDING AREA 405,000 SF
AVERAGE AREA PER STORY 45,000 SF

TYPE IV-C

Occupancy	# of Stories	Height	Area per Story	Building Area
A-2	6	85 ft	56,250 SF	168,750 SF
B	9	85 ft	135,000 SF	405,000 SF
M	6	85 ft	76,875 SF	230,625 SF
R-2	8	85 ft	76,875 SF	230,625 SF

Areas exclude potential frontage increase

In most cases, Type IV-C height allowances = Type IV-HT height allowances, but add'l stories permitted due to enhanced FRR

Type IV-C area = 1.25 * Type IV-HT area

Type IV-B



12 STORES
BUILDING HEIGHT 180 FT
ALLOWABLE BUILDING AREA 645,000 SF
AVERAGE AREA PER STORY 54,000SF

TYPE IV-B

Credit: Susan Jones, atelierjones



Credit: LEVER Architecture



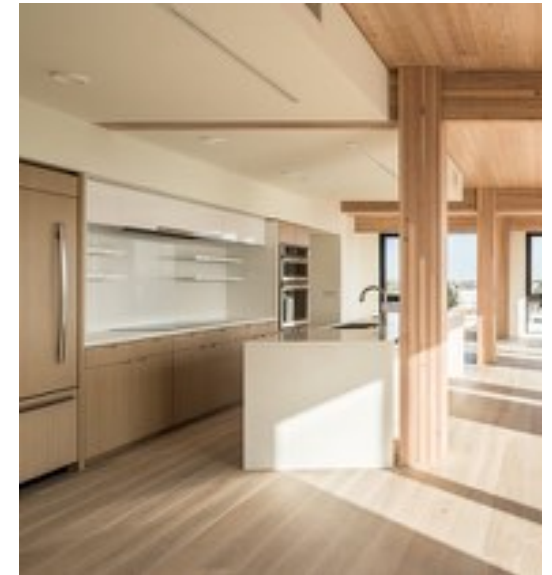
Type IV-B Protection vs. Exposed

IV-B



12 STORES
BUILDING HEIGHT 180 FT
ALLOWABLE BUILDING AREA 648,000 SF
AVERAGE AREA PER STORY 54,000SF

TYPE IV-B



Credit: Kaiser+Path

NC protection on all surfaces of Mass Timber except limited exposed areas

~20% of Ceiling or ~40% of Wall can be exposed, see code for requirements

Credit: Susan Jones, atelierjones

Type IV-B Protection vs. Exposed

IV-B

Limited Exposed MT allowed in Type IV-B for:

- **MT beams and columns which are not integral part of walls or ceilings, no area limitation applies**
- **MT ceilings and beams up to 20% of floor area in dwelling unit or fire area, or**
- **MT walls and columns up to 40% of floor area in dwelling unit or fire area, or**
- **Combination of ceilings/beams and walls/columns, calculated as follows:**



Credit: Kaiser+Path

Type IV-B Protection vs. Exposed

IV-B

Design Example: Mixing unprotected MT walls & ceilings



Credit: AWC

800 SF dwelling unit

- $U_{ac} = (800 \text{ SF}) * (0.20) = 160 \text{ SF}$
- $U_{aw} = (800 \text{ SF}) * (0.40) = 320 \text{ SF}$
- **Could expose 160 SF of MT ceiling, OR 320 SF of MT Wall, OR**
- **If desire to expose 100 SF of MT ceiling in Living Room, determine max. area of MT walls that can be exposed**

Type IV-B Protection vs. Exposed

IV-B



Credit: AWC

Type IV-B Protection vs. Exposed

IV-B



Credit: AWC

Type IV-B Protection vs. Exposed

IV-B

Horizontal separation of unprotected areas:

- Unprotected portions of mass timber walls and ceilings shall be **not less than 15 feet** from unprotected portions of other walls and ceilings, measured horizontally along the ceiling and from other unprotected portions of walls measured horizontally along the floor.



Credit: Kaiser+Path

Type IV-B Protection vs. Exposed

IV-B



Type IV-B Height and Area Limits



12 STORES
BUILDING HEIGHT 180 FT
ALLOWABLE BUILDING AREA 648,000 SF
AVERAGE AREA PER STORY 54,000SF

TYPE IV-B

Occupancy	# of Stories	Height	Area per Story	Building Area
A-2	12	180 ft	90,000 SF	270,000 SF
B	12	180 ft	216,000 SF	648,000 SF
M	8	180 ft	123,000 SF	369,000 SF
R-2	12	180 ft	123,000 SF	369,000 SF

Areas exclude potential frontage increase

In most cases, Type IV-B height & story allowances = Type I-B height & story allowances

Type IV-B area = 2 * Type IV-HT area

Type IV-A



18 STORIES
BUILDING HEIGHT 270'
ALLOWABLE BUILDING AREA 972,000 SF
AVERAGE AREA PER STORY 54,000SF

TYPE IV-A

Credit: Susan Jones, atelierjones



Photos: Structurlam, naturally:wood,
Fast + Epp, Urban One

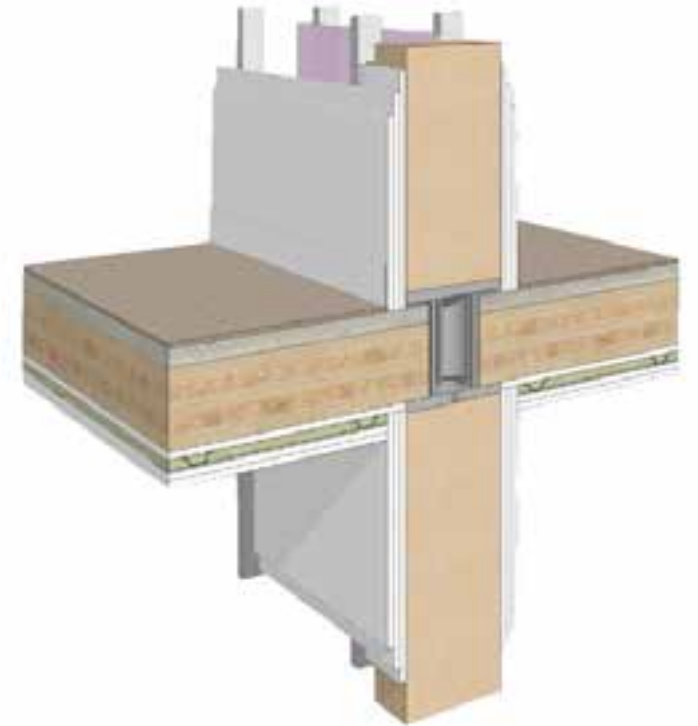
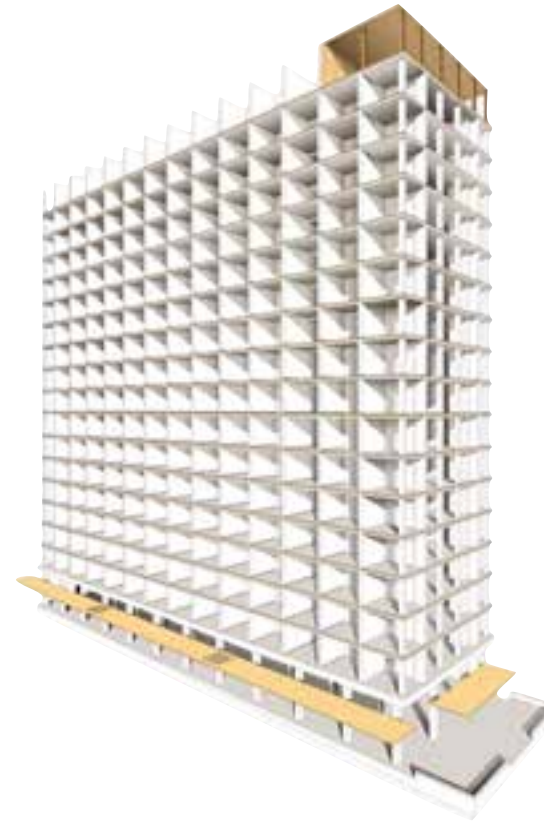
Type IV-A Protection vs. Exposed



18 STORIES
BUILDING HEIGHT 270'
ALLOWABLE BUILDING AREA 972,000 SF
AVERAGE AREA PER STORY 54,000SF

TYPE IV-A

Credit: Susan Jones, atelierjones



100% NC protection on all surfaces of
Mass Timber

Credit: Acton Ostry Architects, Fast + Epp

Type IV-A Height and Area Limits



18 STORIES
BUILDING HEIGHT 270'
ALLOWABLE BUILDING AREA 972,000 SF
AVERAGE AREA PER STORY 54,000SF

TYPE IV-A

Credit: Susan Jones, atelierjones

Occupancy	# of Stories	Height	Area per Story	Building Area
A-2	18	270 ft	135,000 SF	405,000 SF
B	18	270 ft	324,000 SF	972,000 SF
M	12	270 ft	184,500 SF	553,500 SF
R-2	18	270 ft	184,500 SF	553,500 SF

Areas exclude potential frontage increase

In most cases, Type IV-A height & story allowances = 1.5 * Type I-B height & story allowances

Type IV-A area = 3 * Type IV-HT area

Materials Permitted

602.4 Type IV. Type IV construction is that type of construction in which the building elements are mass timber or noncombustible materials and have fire resistance ratings in accordance with Table 601. Mass timber elements shall meet the fire resistance rating requirements of this section based on either the fire resistance rating of the noncombustible protection, the mass timber, or a combination of both and shall be determined in accordance with Section 703.2 or 703.3. The minimum dimensions and permitted materials for building elements shall comply with the provisions of this section and Section 2304.11. Mass timber

Exterior load-bearing walls and nonload-bearing walls shall be mass timber construction, or shall be of noncombustible construction.

Exception: Type IV-HT Construction in accordance with Section 602.4.4.

The interior building elements, including nonload-bearing walls and partitions, shall be of mass timber construction or of noncombustible construction.

Exception: Type IV-HT Construction in accordance with Section 602.4.4..

Building Elements in Type IV Construction



Photo:: Ema Peter

Minimum sizes for existing
Type IV (now IV-HT)
apply to the new
Type IV-A, IV-B and IV-C

See
IBC 2018 2304.11
IBC 2015 602.4

Tall Wood Fire Resistance Ratings (FRR)

FRR Requirements for Tall Mass Timber Structures (hours)

Building Element	IV-A	IV-B	IV-C
Primary Frame	3	2	2
Exterior Bearing Walls	3	2	2
Interior Bearing Walls	3	2	2
Roof Construction	1.5	1	1
Primary Frame at Roof	2	1	1
Floor Construction	2	2	2

Source: 2021 IBC Table 601

Noncombustible Protection (NC)

Where timber is required to be protected, NC must contribute at least 2/3 FRR

Required Noncombustible Contribution to FRR

FRR of Building Element (hours)	Minimum from Noncombustible Protection (minutes)
1	40
2	80
3 or more	120

Source: 2021 IBC Section 722.7

Noncombustible Protection (NC)

Prescriptive Noncombustible Contributions to FRR

Type of Protection	Contribution per Layer (minutes)
1/2" Type X gypsum board	25
5/8" Type X gypsum board	40

Source: 2021 IBC Section 722.7.1

Required Noncombustible Contribution to FRR

FRR of Building Element (hours)	Minimum from Noncombustible Protection (minutes)
1	40
2	80
3 or more	120

1 layer 5/8 Type X

2 layers 5/8 Type X

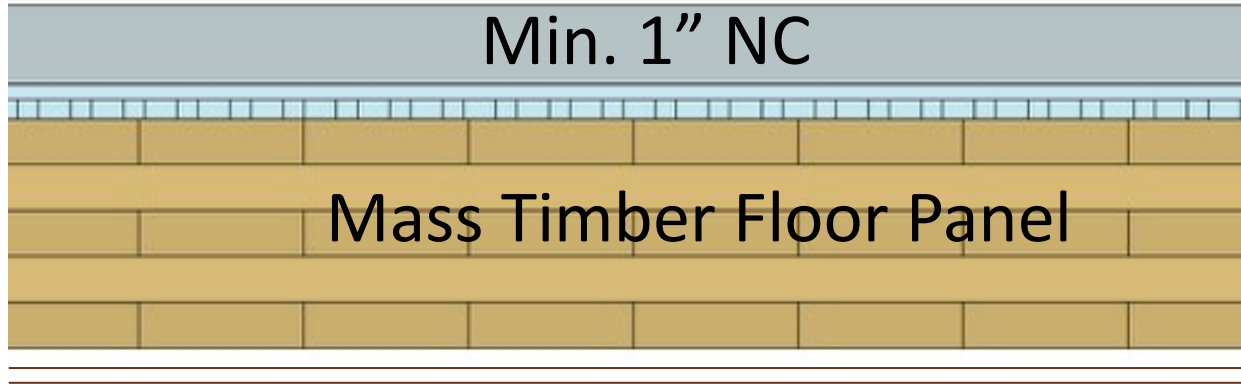
3 layers 5/8 Type X

Source: 2021 IBC Section 722.7

IV-A

IV-B

Type IV-A and IV-B NC Protection over MT Floor



In Type IV-A and IV-B, the floor assembly shall contain a noncombustible material not less than one inch in thickness above the mass timber.



Credit: Maxxon

Type IV-A Fire Resistance Ratings (FRR)

IV-A

Primary Frame (3-hr) + Floor Panel Example (2-hr):

Minimum 1" noncombustible material

Mass timber floor panel

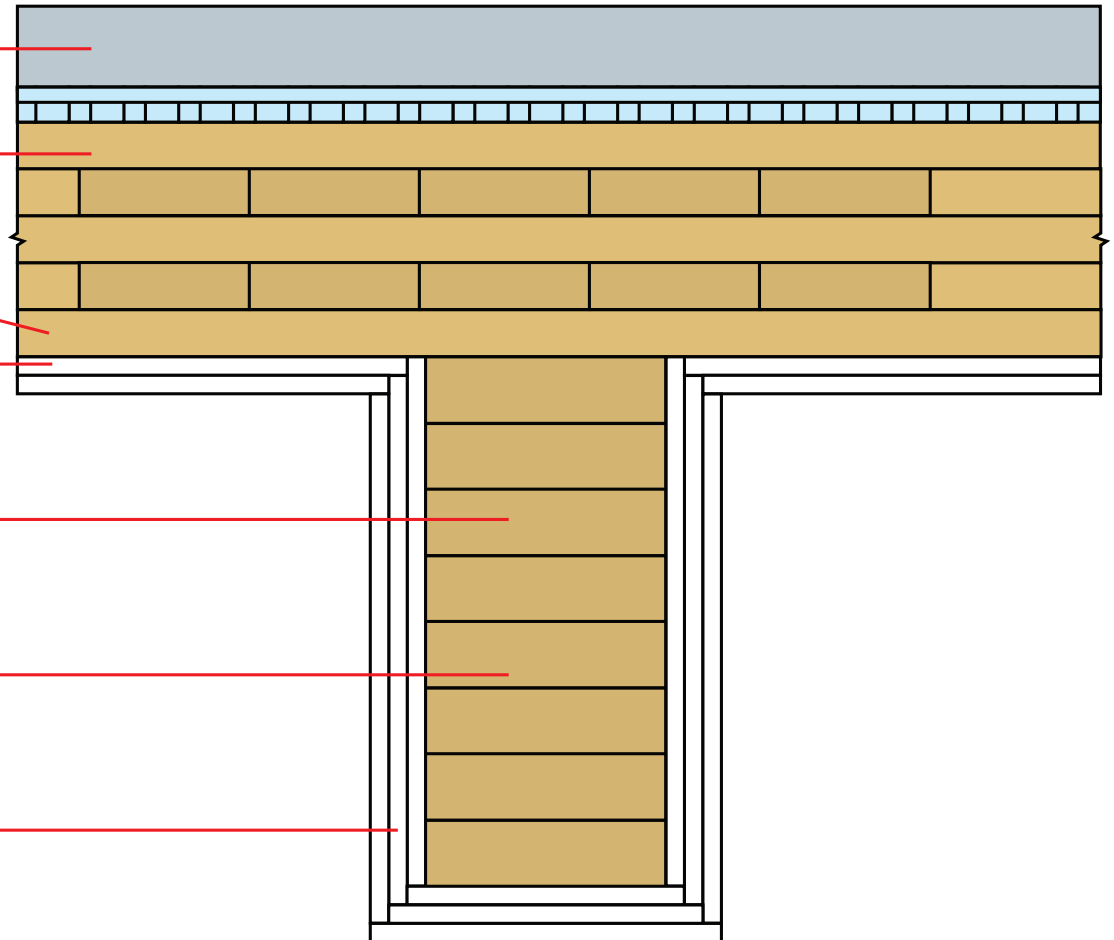
40 minutes of MT FRR

Two layers 5/8" Type X gypsum

Glulam beam (primary structural frame)

60 minutes of MT FRR

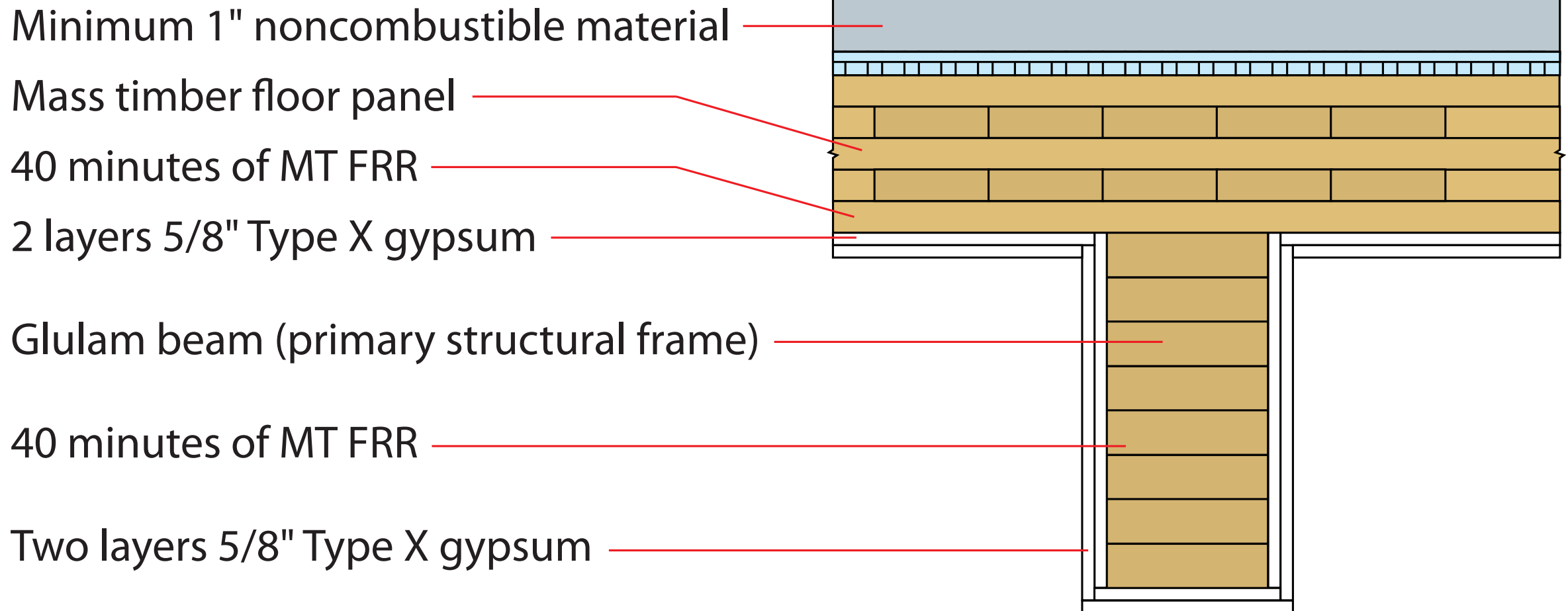
Three layers 5/8" Type X gypsum



Type IV-B Fire Resistance Ratings (FRR)

IV-B

Primary Frame (2-hr) + Floor Panel (2-hr)



Type IV-B Fire Resistance Ratings (FRR)

IV-B

Primary Frame (2-hr) + Floor Panel Example (2-hr)

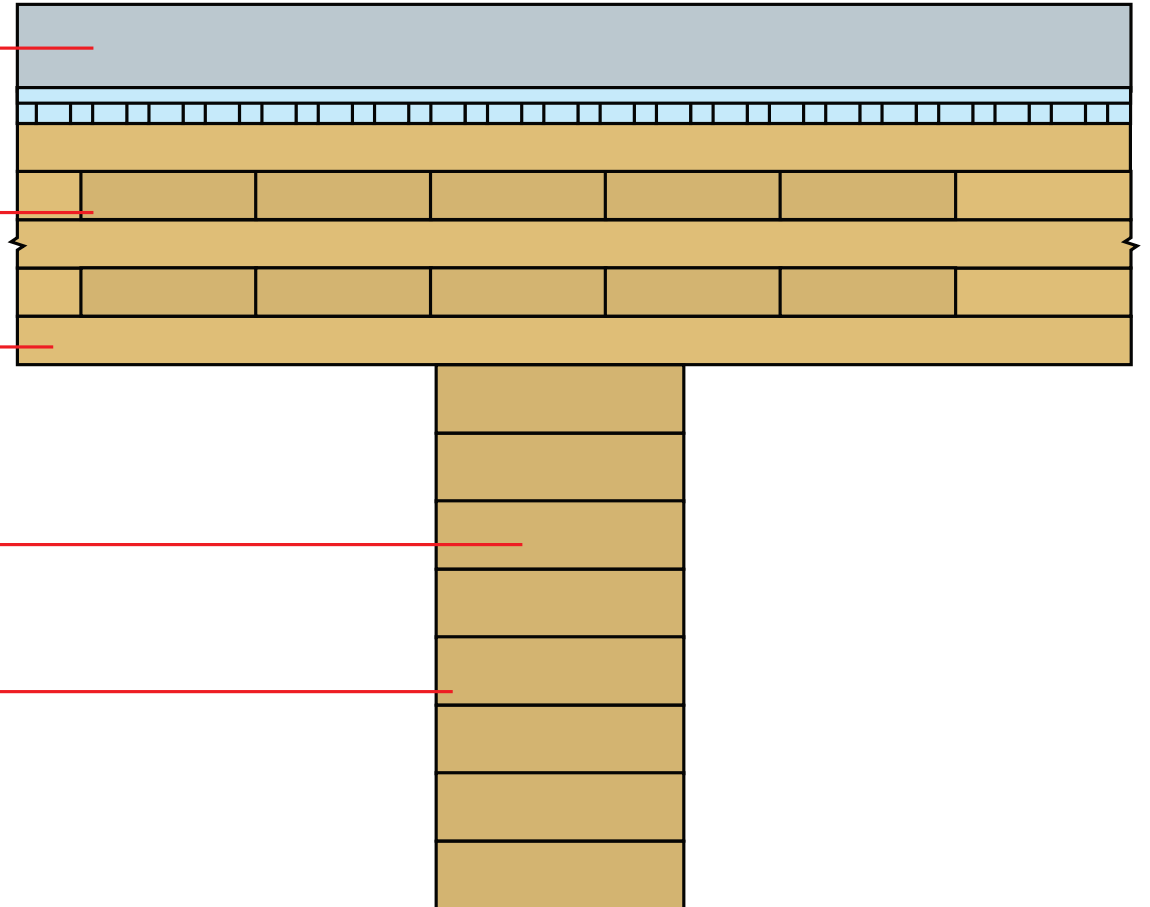
Minimum 1" noncombustible material

Mass timber floor panel

2-hr of MT FRR;
noncombustible material not required

Glulam beam (primary structural frame)

2-hr of MT FRR;
Noncombustible material not required



Type IV-C Fire Resistance Ratings (FRR)

IV-C

Primary Frame (2-hr) + Floor Panel Example (2-hr)

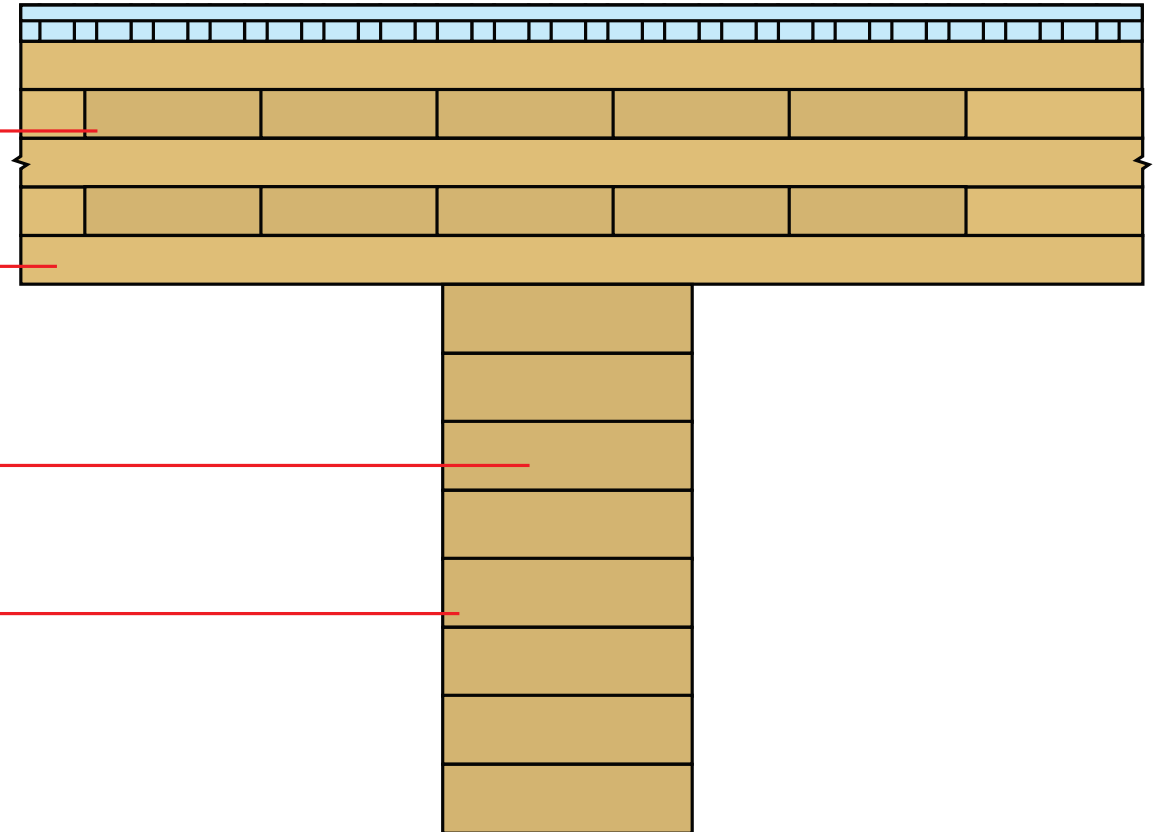
Noncombustible material not required

Mass timber floor panel

2-hr of MT FRR;
noncombustible material not required

Glulam beam (primary structural frame)

2-hr of MT FRR;
Noncombustible material not required



MT Fire Resistance Ratings (FRR)



IBC 722.7

The fire resistance rating of the mass timber elements shall consist of the fire resistance of the unprotected element (MT) added to the protection time of the noncombustible (NC) protection.

MT



NC



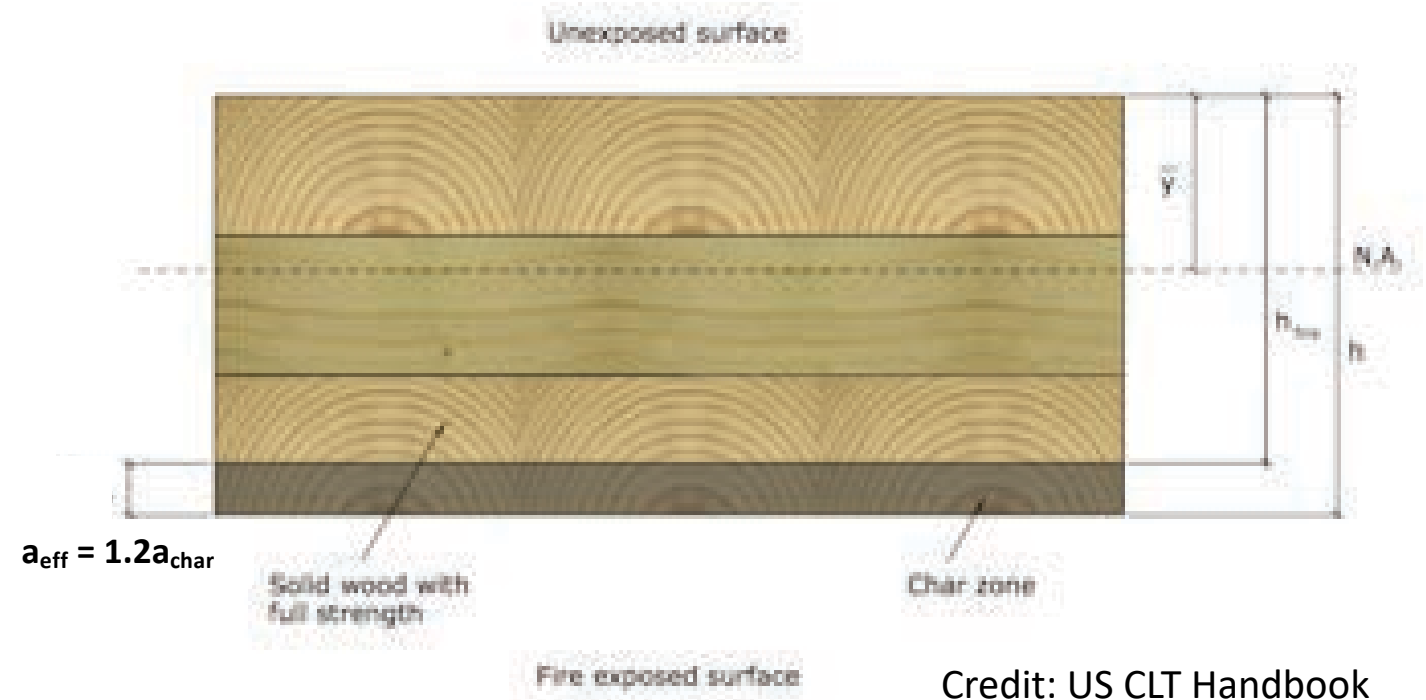
= FRR

MT Fire Resistance Ratings (FRR)

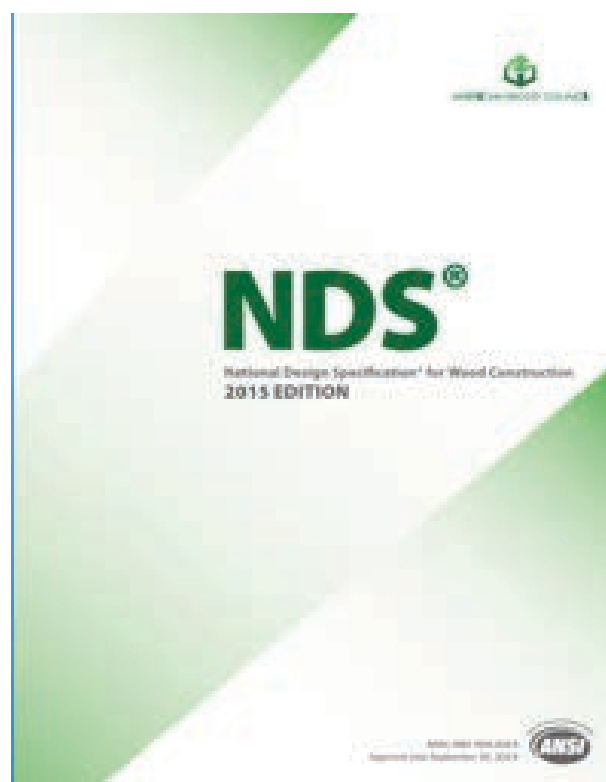
How do you determine FRR of MT?

2 Options:

1. Calculations in Accordance with IBC 722 → NDS Chapter 16
2. Tests in Accordance with ASTM E119



MT Fire Resistance Ratings (FRR)



NDS Chapter 16 includes calculation of fire resistance of NLT, CLT, Glulam, Solid Sawn and SCL wood products

Table 16.2.1B Effective Char Depths (for CLT with $\beta_s = 1.5 \text{ in./hr.}$)

Required Fire Endurance (hr.)	Effective Char Depths, a_{char} (in.)								
	lamination thicknesses, h_{lam} (in.)								
	5/8	3/4	7/8	1	1-1/4	1-3/8	1-1/2	1-3/4	2
1-Hour	2.2	2.2	2.1	2.0	2.0	1.9	1.8	1.8	1.8
1½-Hour	3.4	3.2	3.1	3.0	2.9	2.8	2.8	2.8	2.6
2-Hour	4.4	4.3	4.1	4.0	3.9	3.8	3.6	3.6	3.6



Credit: FPInnovations

MT Fire Resistance Ratings (FRR)

Nominal char rate of 1.5"/HR is recognized in NDS. Effective char depth calculated to account for duration, structural reduction in heat-affected zone



Table 16.2.1A Char Depth and Effective Char Depth (for $\beta_a = 1.5$ in./hr.)

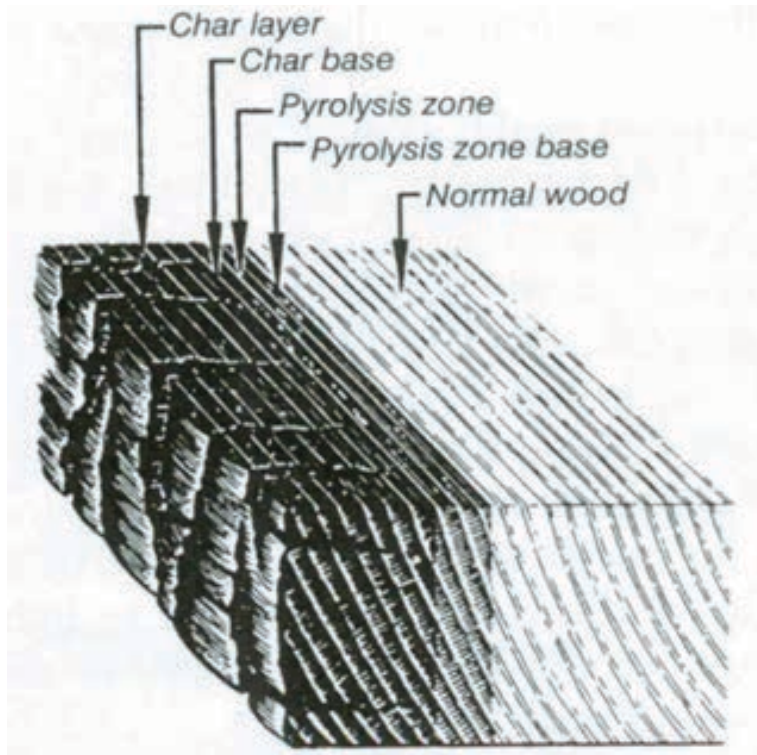
Required Fire Resistance (hr.)	Char Depth, a_{char} (in.)	Effective Char Depth, a_{eff} (in.)
1-Hour	1.5	1.8
1½-Hour	2.1	2.5
2-Hour	2.6	3.2

Table 16.2.1B Effective Char Depths (for CLT with $\beta_a=1.5$ in./hr.)

Required Fire Endurance (hr.)	Effective Char Depths, a_{char} (in.)								
	lamination thicknesses, h_{lam} (in.)								
	5/8	3/4	7/8	1	1-1/4	1-3/8	1-1/2	1-3/4	2
1-Hour	2.2	2.2	2.1	2.0	2.0	1.9	1.8	1.8	1.8
1½-Hour	3.4	3.2	3.1	3.0	2.9	2.8	2.8	2.8	2.6
2-Hour	4.4	4.3	4.1	4.0	3.9	3.8	3.6	3.6	3.6

MT Fire Resistance Ratings (FRR)

Structural capacity check performed on remaining section, with stress increases



Credit: Forest Products Laboratory

Table 16.2.2 Adjustment Factors for Fire Design¹

			ASD					
			Design Stress to Member Strength Factor	Size Factor ²	Volume Factor ³	Flat Use Factor ⁴	Beam Stability Factor ⁵	Column Stability Factor ⁶
Bending Strength	F_b	x	2.85	C_F	C_V	C_{fu}	C_L	-
Beam Buckling Strength	F_{bE}	x	2.03	-	-	-	-	-
Tensile Strength	F_t	x	2.85	C_F	-	-	-	-
Compressive Strength	F_c	x	2.58	C_F	-	-	-	C_P
Column Buckling Strength	F_{cE}	x	2.03	-	-	-	-	-

$$a_{\text{char}} = \beta_t t^{0.813}$$

Solid Sawn, Glulam, SCL

$$a_{\text{char}} = n_{\text{lam}} h_{\text{lam}} + \beta_t \left(t - (n_{\text{lam}} t_{\text{gl}}) \right)^{0.813}$$

CLT

$$a_{\text{eff}} = 1.2 a_{\text{char}}$$

Effective Char Depth

MT Fire Resistance Ratings (FRR)

Inventory of Fire Tested MT Assemblies

Table 1: North American Fire Resistance Tests of Mass Timber Floor / Roof Assemblies



CLT Panel	Manufacturer	CLT Grade or Major & Minor Grade	Ceiling Protection	Panel Connection in Test	Floor Topping	Load Rating	Fire Resistance Achieved (Hours)	Source	Testing Lab
8-ply CLT (114mm x 4000 mm)	Nordic	SPT 14.50 (E) x 1.10 (MSB) x SPT 10	2 layers 1/2" Type X gypsum	Half-Lap	None	Ballasted 14% Moment Capacity	1	1 (Test 1)	NBC Fire Laboratory
8-ply CLT (101mm x 4110 mm)	Sveinbjörn	SPT 11.02 x SPT 11.02	1 layer 1/2" Type X gypsum	Half-Lap	None	Ballasted 13% Moment Capacity	1	1 (Test 3)	NBC Fire Laboratory
8-ply CLT (171mm x 4700")	Nordic	EL	None	Top-side Splice	2 staggered layers of 1/2" cement boards	Loaded, See Manufacturer	2	2	NBC Fire Laboratory March 2016
8-ply CLT (171mm x 4700")	Nordic	EL	1 layer of 1/2" Type X gypsum under 2 channels and flooring strips with 3 5/8" dimension studs	Top-side Splice	2 staggered layers of 1/2" cement boards	Loaded, See Manufacturer	2	2	NBC Fire Laboratory Nov 2014
8-ply CLT (171mm x 4700")	Nordic	EL	None	Top-side Splice	3/4 in. proprietary gypsum over Mass on acoustic insulation	Ballasted 10% Moment Capacity	1.5	3	UL
8-ply CLT (171mm x 4700")	Nordic	EL	1 layer 5/8" normal gypsum	Top-side Splice	3/4 in. proprietary gypsum over Mass on acoustic insulation or proprietary metal board	Ballasted 10% Moment Capacity	2	4	UL
8-ply CLT (171mm x 4700")	Nordic	EL	2 layers 5/8" Type X Gypsum under Redken/Channel under 3 7/8" 4-layers with 1 1/2" Insulated Wood between Joists	Half-Lap	None	Loaded, See Manufacturer	2	21	Intertek 8/24/2012
8-ply CLT (171mm x 4700")	Sveinbjörn	ELMS MSB 2100 x SPT 12	None	Top-side Splice	1 x 1/2" Masson Type G over 2000 or Masson Insulating Mat	Loaded, See Manufacturer	2.5	4	Intertek, 2/22/2016
8-ply CLT (171mm x 4700")	DR Johnson	VI	None	Half-Lap & Top-side Splice	2" gypsum topping	Loaded, See Manufacturer	2	7	SwRI (May 2016)
8-ply CLT (171mm x 4700")	Nordic	SPT 14.50 (E) MSB x SPT 10	None	Half-Lap	None	Ballasted 10% Moment Capacity	1.5	1 (Test 3)	NBC Fire Laboratory
8-ply CLT (171mm x 4700")	Sveinbjörn	SPT 11.02 x SPT 11.02	1 layer 5/8" Type X gypsum	Half-Lap	None	Unballasted 10% Moment Capacity	2	1 (Test 6)	NBC Fire Laboratory
8-ply CLT (141mm x 4800")	Sveinbjörn	SPT 11.02 x SPT 11.02	None	Half-Lap	None	Unballasted 10% Moment Capacity	2.5	1 (Test 7)	NBC Fire Laboratory
8-ply CLT (171mm x 4700")	SmartLam	SL-V4	None	Half-Lap	nominal 1/2" plywood with 3/4" nails	Loaded, See Manufacturer	2	12 (Test 4)	Western Fire Center 10/26/2016
8-ply CLT (171mm x 4700")	SmartLam	VI	None	Half-Lap	nominal 1/2" plywood with 3/4" nails	Loaded, See Manufacturer	2	12 (Test 3)	Western Fire Center 10/28/2016
8-ply CLT (171mm x 4700")	DR Johnson	VI	None	Half-Lap	nominal 1/2" plywood with 3/4" nails	Loaded, See Manufacturer	2	12 (Test 6)	Western Fire Center 11/01/2016
8-ply CLT (114mm x 4000 mm)	KTH	(V1M1)	None	Half-Lap & Top-side Splice	None	Loaded, See Manufacturer	1	16	SwRI

MT Fire Resistance Ratings (FRR)



Fire-Resistive Design of Mass Timber Members

Code Applications, Construction Types and Fire Ratings

Robert J. Lujan, PE, SE • Senior Technical Director • WoodWorks
Scott Steinman, PhD, PE, SE • Senior Technical Director • WoodWorks

For many years, exposed heavy timber framing elements have been permitted in U.S. buildings due to their inherent fire-resistance properties. The predictability of wood's char rate has been well established for decades and has long been recognized in building codes and standards.

Today, one of the exciting trends in building design is the growing use of mass timber—i.e., large solid wood panel products such as cross-laminated timber (CLT) and nail-laminated timber (NLT)—for floor, wall and roof construction. Like heavy timber, mass timber products have inherent fire resistance that allows them to be left exposed and still achieve a fire-resistance rating. Because of their strength and dimensional stability, these products also offer a low-carbon alternative to steel, concrete, and masonry for many applications. It is this combination of exposed structure and strength that developers and designers across the country

are leveraging to create innovative designs with a warm, yet modern aesthetic, often for projects that go beyond traditional norms of wood design.

This paper has been written to support architects and engineers exploring the use of mass timber for commercial and multi-family construction. It focuses on how to meet fire-resistance requirements in the International Building Code (IBC), including calculation and testing-based methods. Unless otherwise noted, references refer to the 2018 IBC.

Mass Timber & Construction Type

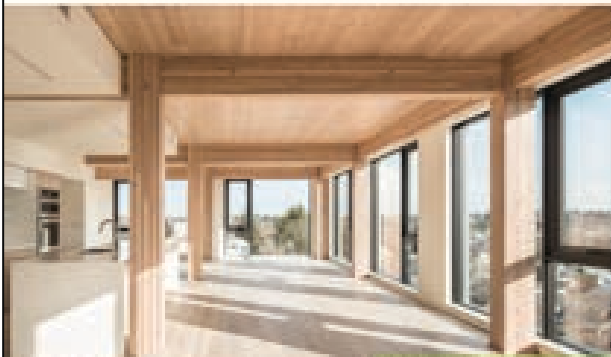
Before demonstrating fire-resistance ratings of exposed mass timber elements, it's important to understand under what circumstances the code currently allows the use of mass timber in commercial and multi-family construction.

A building's assigned construction type is the main indicator of where and when all wood systems can be used. IBC Section 602 defines five main options (Type I through V) with all but Type IV having subcategories A and B. Types III and V permit the use of wood framing throughout much of the structure and both are used extensively for modern mass timber buildings.

Type III IBC 602.3 – Timber elements can be used in floors, roofs and interior walls. Fire-retardant-treated wood (FRTW) framing is permitted in exterior walls with a fire-resistance rating of 2 hours or less.

Type V IBC 602.5 – Timber elements can be used throughout the structure, including floors, roofs and both interior and exterior walls.

Type IV IBC 602.4 – Commonly referred to as "Heavy Timber" construction, this option



Carlentz | Portland, Oregon
Riser Group | Feb Architecture
Manning Structural Engineering

Mass Timber Fire Design Resource

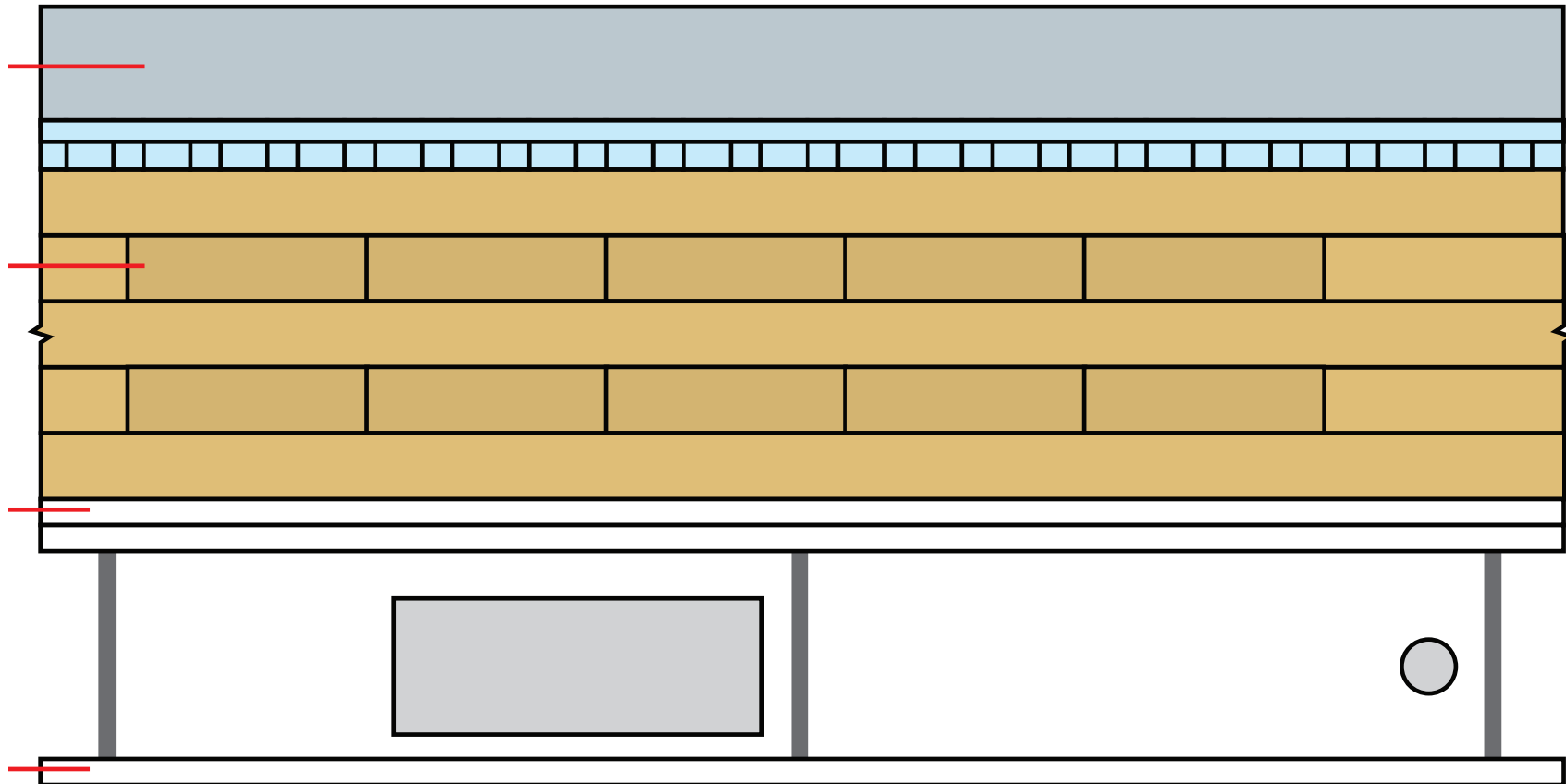
- Code compliance options for demonstrating FRR
- Updated as new tests are completed
- Free download at woodworks.org

Credit: WoodWorks

Concealed Spaces in Type IV

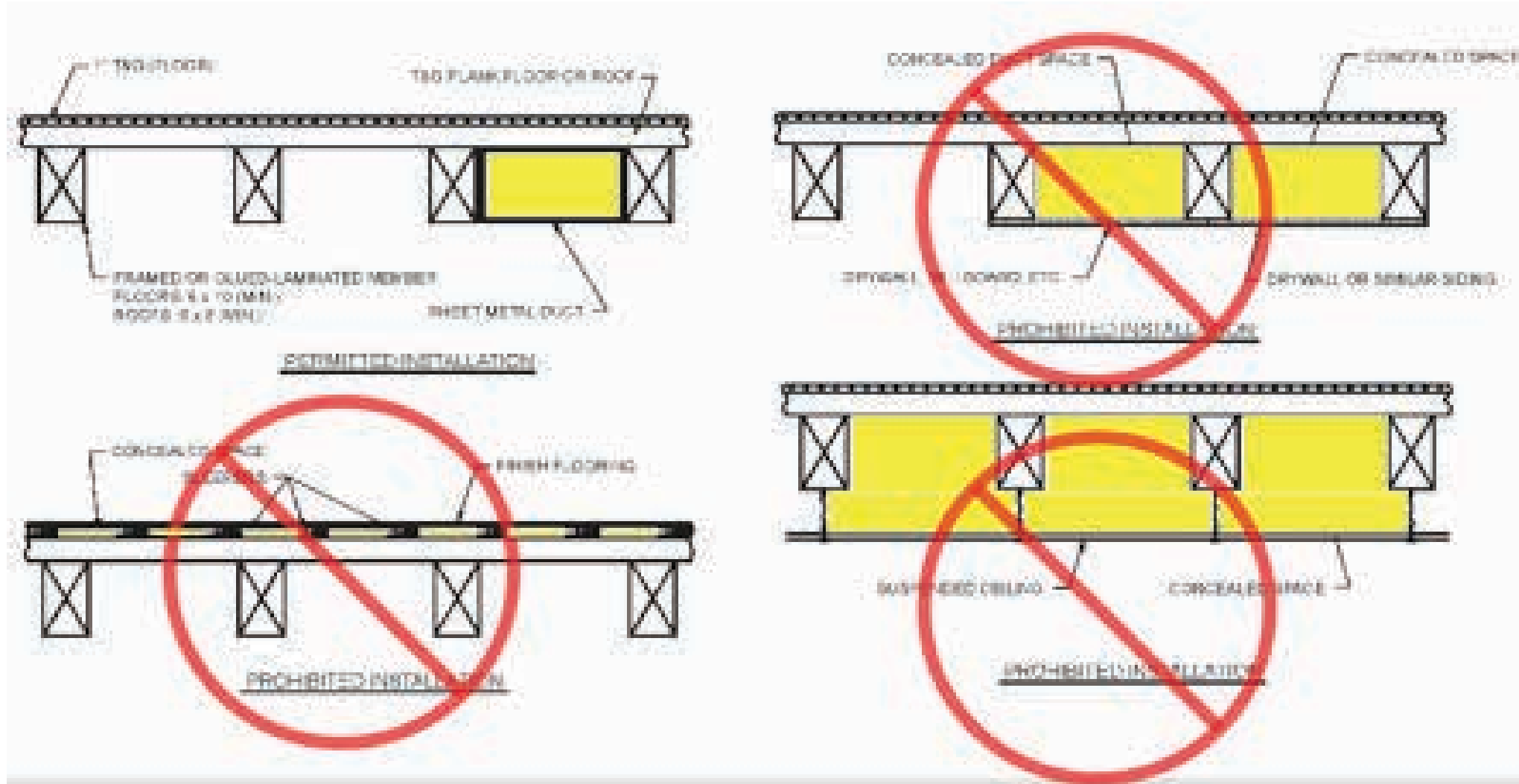
What if I have a dropped ceiling? Can I have a dropped ceiling?

- **Impact on FRR, NC placement, sprinkler requirements**



Concealed Spaces in Type IV

Previous Type IV (now IV-HT) provisions prohibited concealed spaces



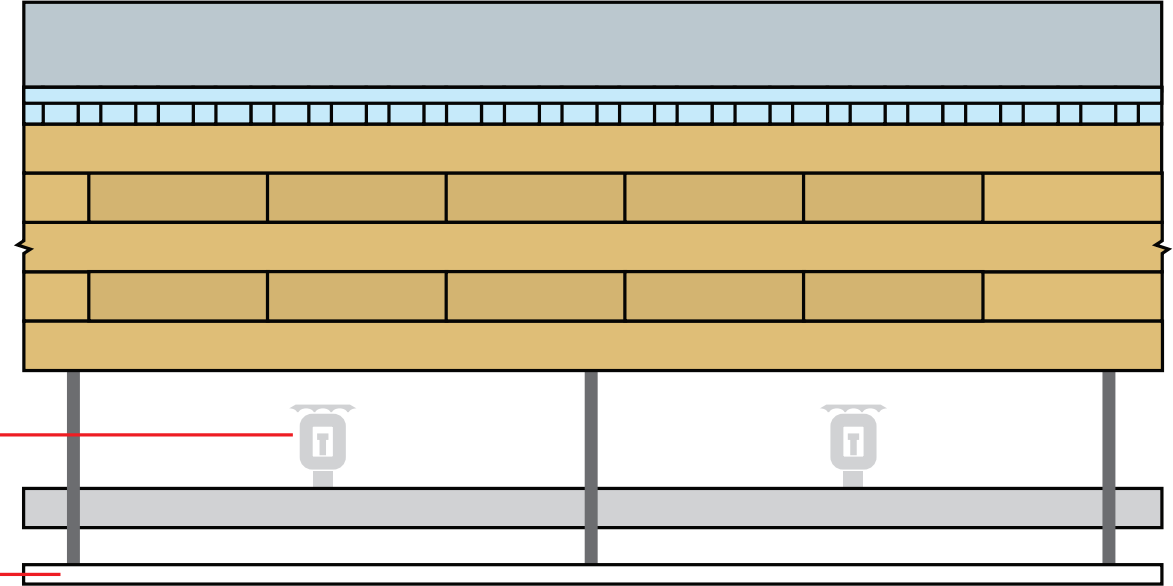
Concealed Spaces in Type IV-HT – 2021 IBC

CONCEALED SPACES: TYPE IV-HT

Option 1:

Sprinklers in concealed spaces

Dropped ceiling



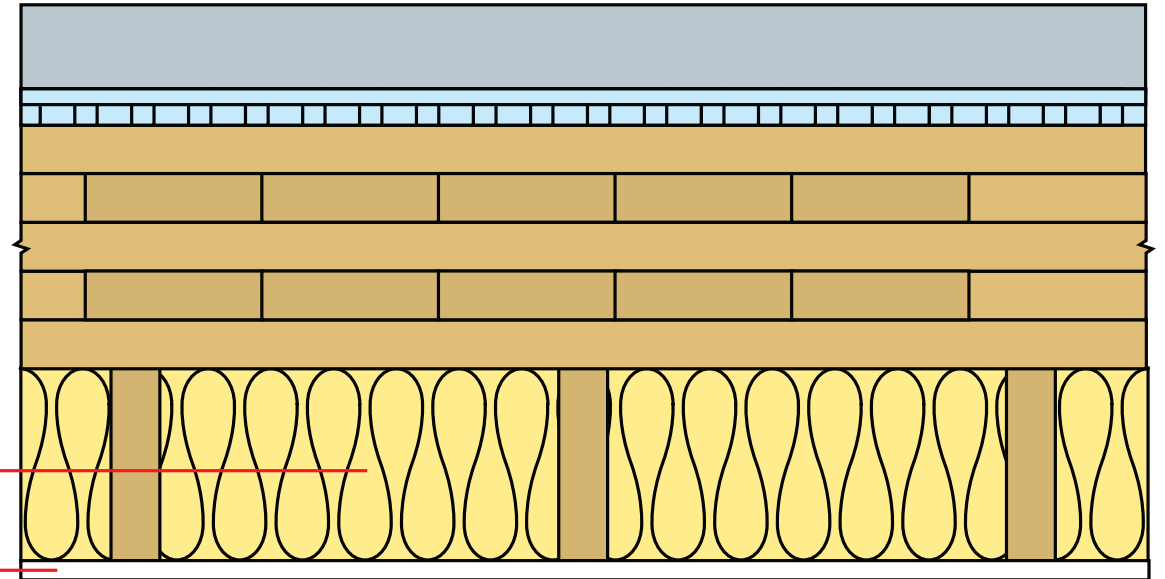
Concealed Spaces in Type IV-HT – 2021 IBC

CONCEALED SPACES: TYPE IV-HT

Option 2:

Noncombustible insulation

Dropped ceiling



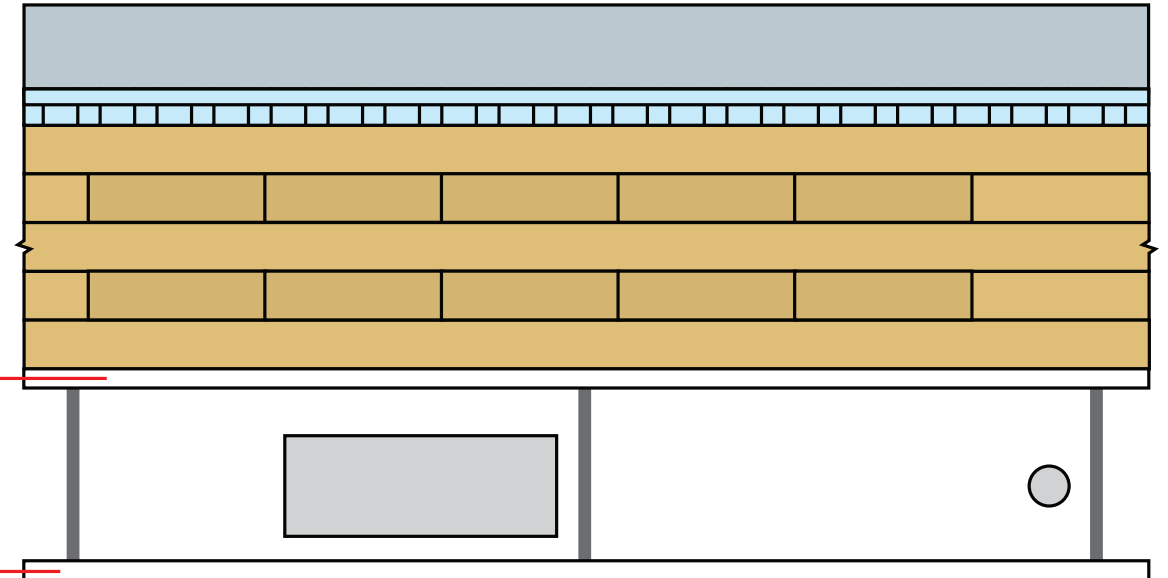
Concealed Spaces in Type IV-HT – 2021 IBC

CONCEALED SPACES: TYPE IV-HT

Option 3:

5/8" Type X gypsum on all mass timber surfaces within concealed space

Dropped ceiling



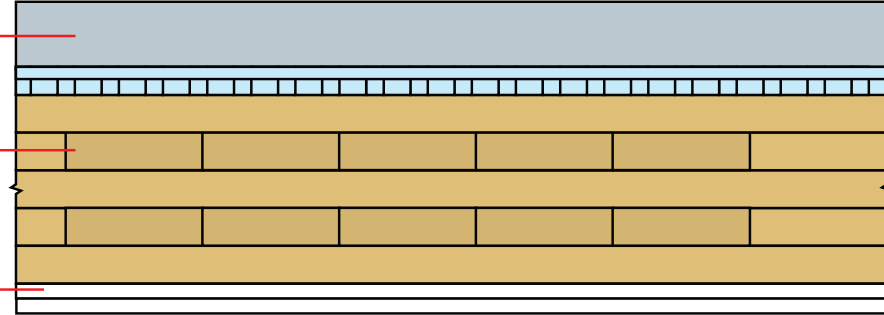
Concealed Spaces in Type IV-A, IV-B

Without Dropped Ceiling

Minimum 1" noncombustible material

Mass timber floor panel

Two layers 5/8" Type X gypsum*



**Applicable to most locations; limited exposed mass timber permitted in IV-B*

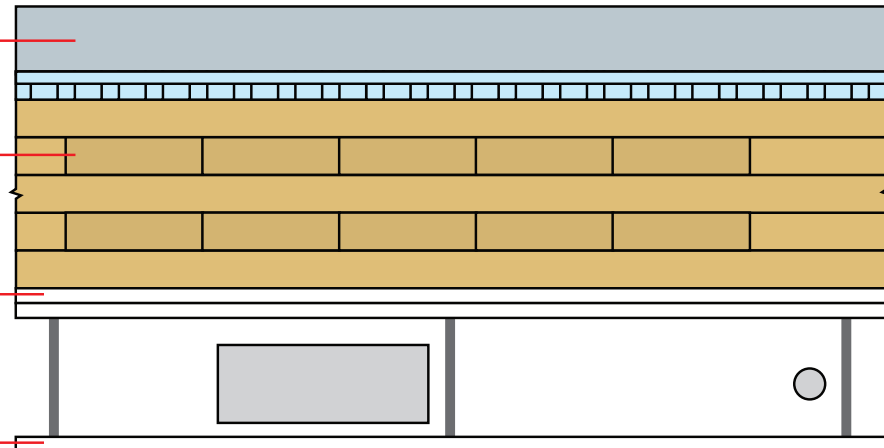
With Dropped Ceiling

Minimum 1" noncombustible material

Mass timber floor panel

Two layers 5/8" Type X gypsum

Dropped ceiling



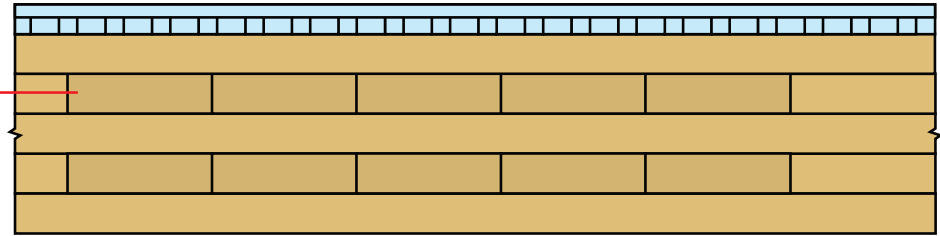
Concealed Spaces in Type IV-C

Without Dropped Ceiling

Noncombustible material not required

Mass timber floor panel

Noncombustible material not required



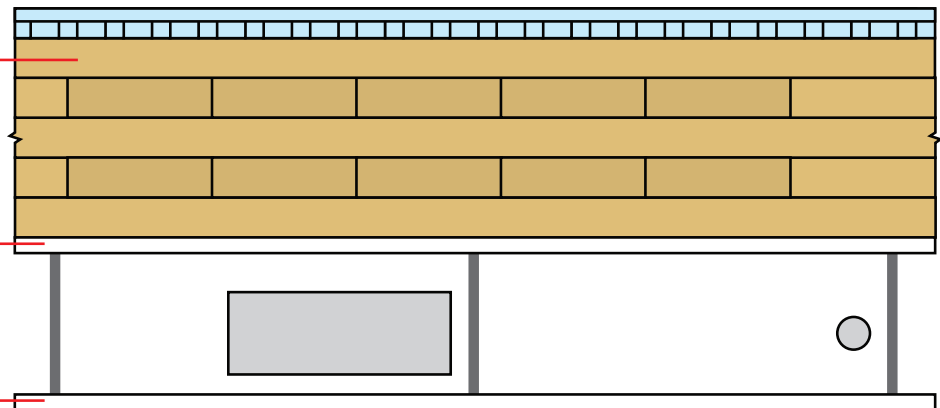
With Dropped Ceiling

Noncombustible material not required

Mass timber floor panel

One layer 5/8" Type X gypsum covering all mass timber surfaces within concealed space

Dropped ceiling

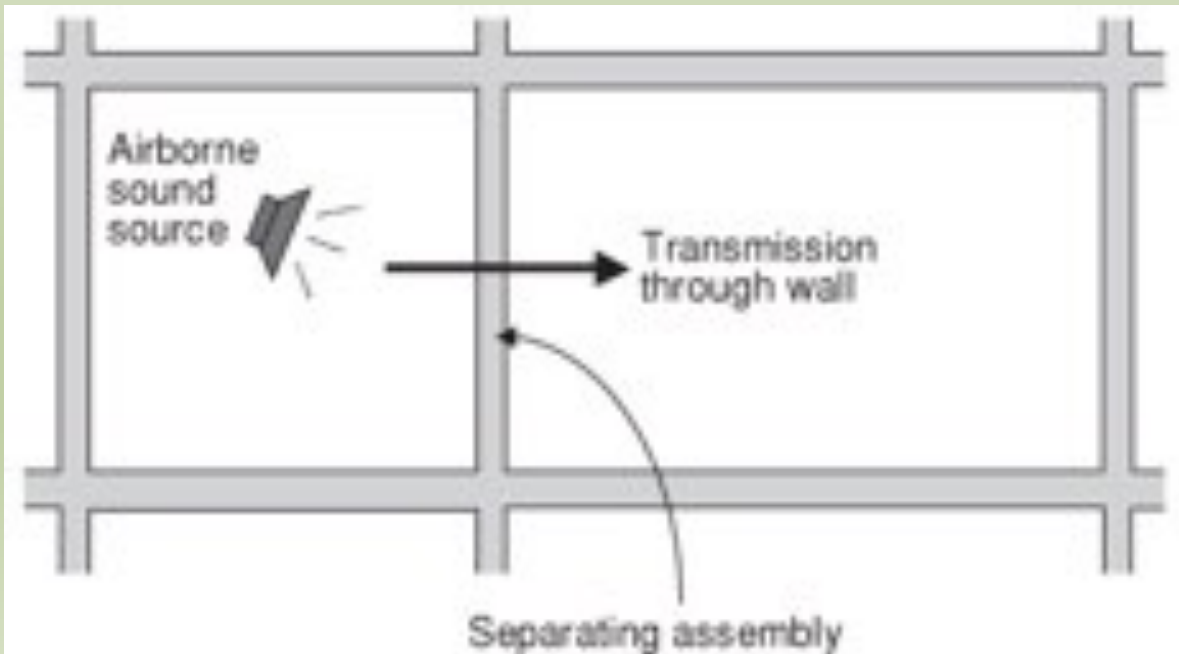


Acoustical Design

Air-Borne Sound:

Sound Transmission Class (STC)

- Measures how effectively an assembly isolates air-borne sound and reduces the level that passes from one side to the other
- Applies to walls and floor/ceiling assemblies

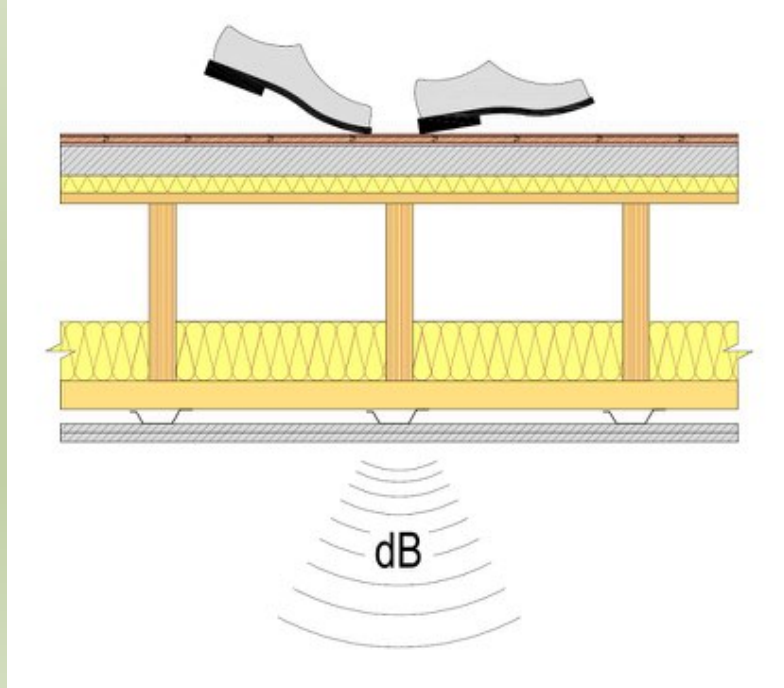


Acoustical Design

Structure-borne sound:

Impact Insulation Class (IIC)

- Evaluates how effectively an assembly blocks impact sound from passing through it
- Only applies to floor/ceiling assemblies



Acoustical Criteria

IBC 1207

Code requirements only address residential occupancies:

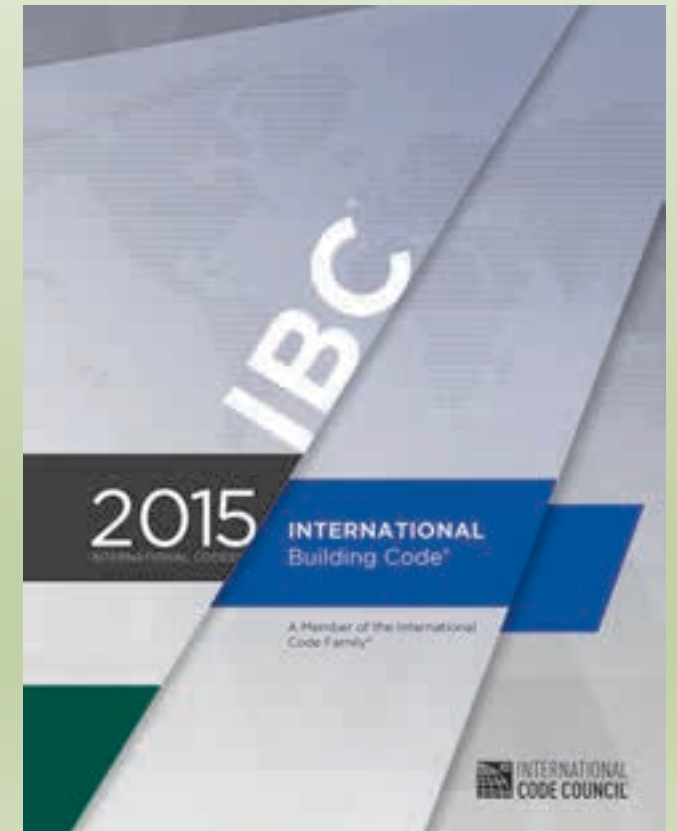
For unit to unit or unit to public or service areas:

Min. STC of 50 (45 if field tested):

- Walls, Partitions, and Floor/Ceiling Assemblies

Min. IIC of 50 (45 if field tested) for:

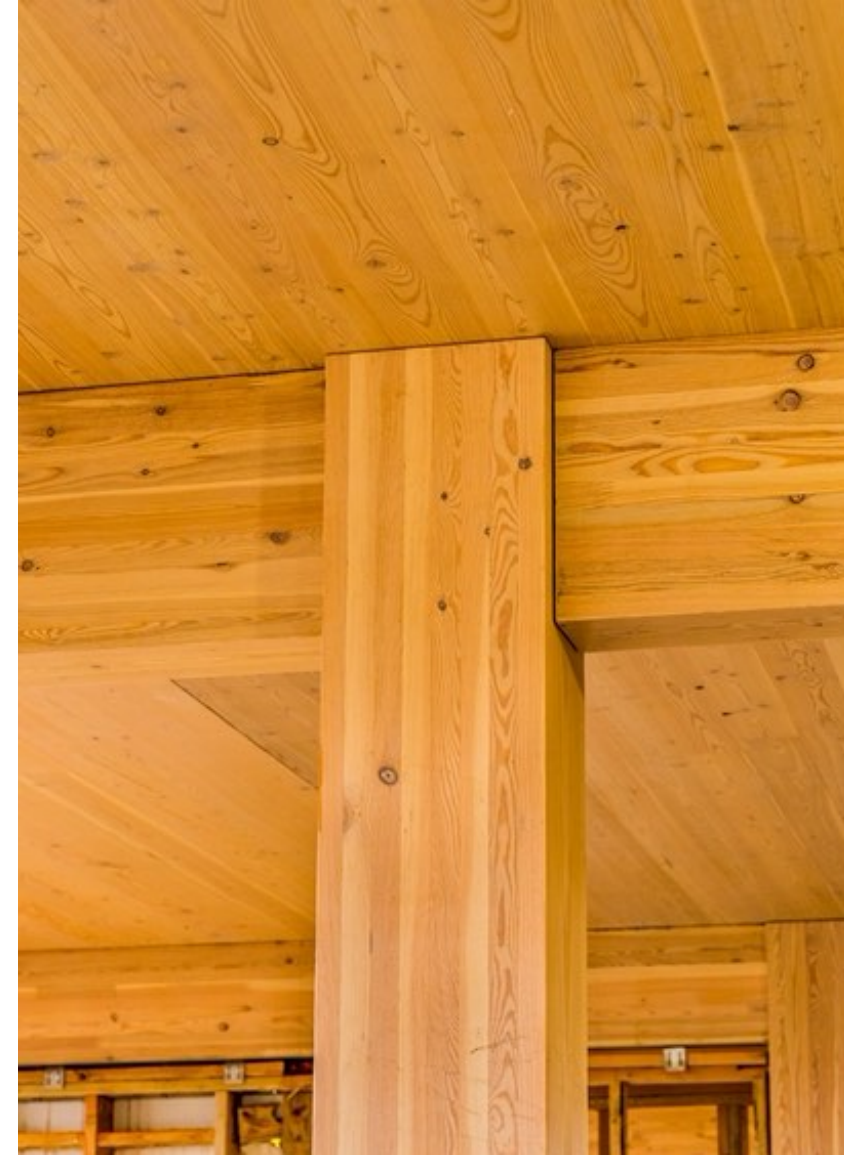
- Floor/Ceiling Assemblies



Acoustical Criteria

STC	What can be heard
25	Normal speech can be understood quite easily and distinctly through wall
30	Loud speech can be understood fairly well, normal speech heard but not understood
35	Loud speech audible but not intelligible
40	Onset of "privacy"
42	Loud speech audible as a murmur
45	Loud speech not audible; 90% of statistical population not annoyed
50	Very loud sounds such as musical instruments or a stereo can be faintly heard; 99% of population not annoyed.
60+	Superior soundproofing; most sounds inaudible

Mass Timber: Structure Often is Finish



Photos: Baumberger Studio/PATH Architecture/Marcus Kauffman | Architect: PATH Architecture

But by Itself, Not Adequate for Acoustics



Mass Timber Acoustics

TABLE 1:
Examples of Acoustically-Tested Mass Timber Panels

Mass Timber Panel	Thickness	STC Rating	IIC Rating
3-ply CLT wall ⁴	3.07"	33	N/A
5-ply CLT wall ⁴	6.875"	38	N/A
5-ply CLT floor ⁶	5.1875"	39	22
5-ply CLT floor ⁴	6.875"	41	25
7-ply CLT floor ⁴	9.65"	44	30
2x4 NLT wall ⁶	3-1/2" bare NLT 4-1/4" with 3/4" plywood	24 bare NLT 29 with 3/4" plywood	N/A
2x6 NLT wall ⁶	5-1/2" bare NLT 6-1/4" with 3/4" plywood	22 bare NLT 31 with 3/4" plywood	N/A
2x6 NLT floor + 1/2" plywood ²	6" with 1/2" plywood	34	33

Source: Inventory of Acoustically-Tested Mass Timber Assemblies, WoodWorks⁷

Acoustical Detailing

Regardless of the structural materials used in a wall or floor ceiling assembly, there are 3 effective methods of improving acoustical performance:

1. Add Mass
2. Add noise barriers
3. Add decouplers

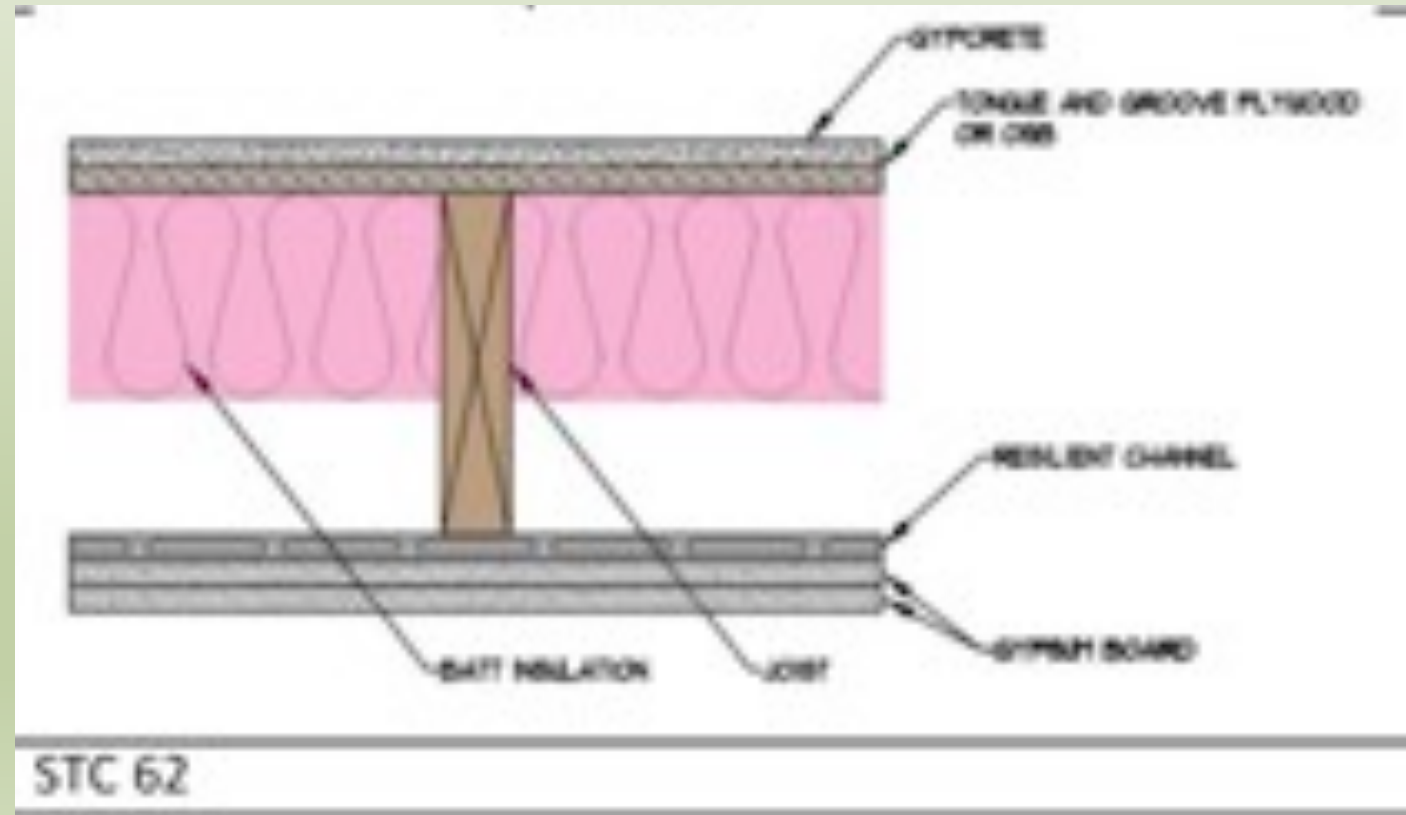


Image credit: Christian Columbres

Acoustical Detailing

What does this look like in typical wood-frame construction:

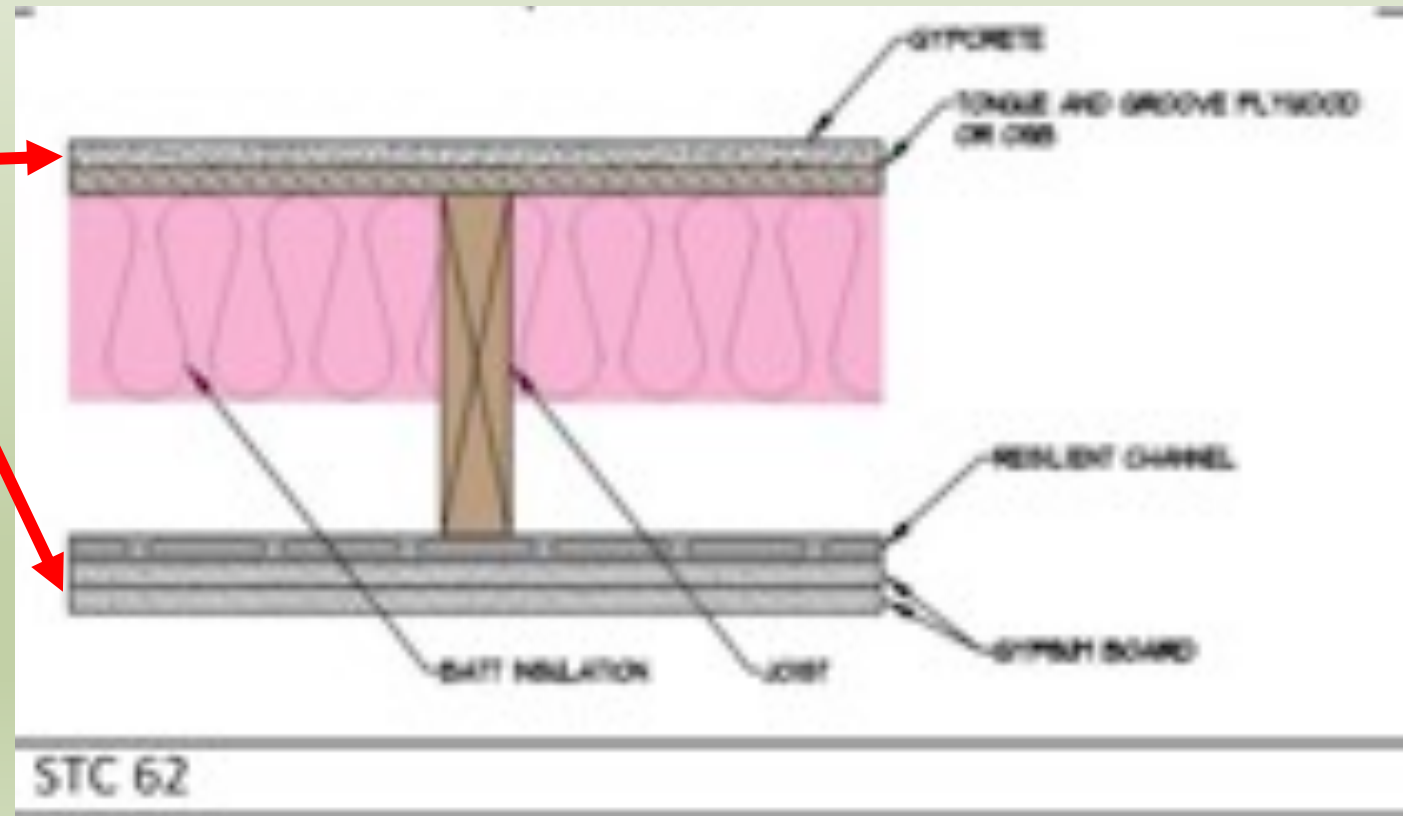
1. Add Mass
2. Add noise barriers
3. Add decouplers



Acoustical Detailing

What does this look like in typical wood-frame construction:

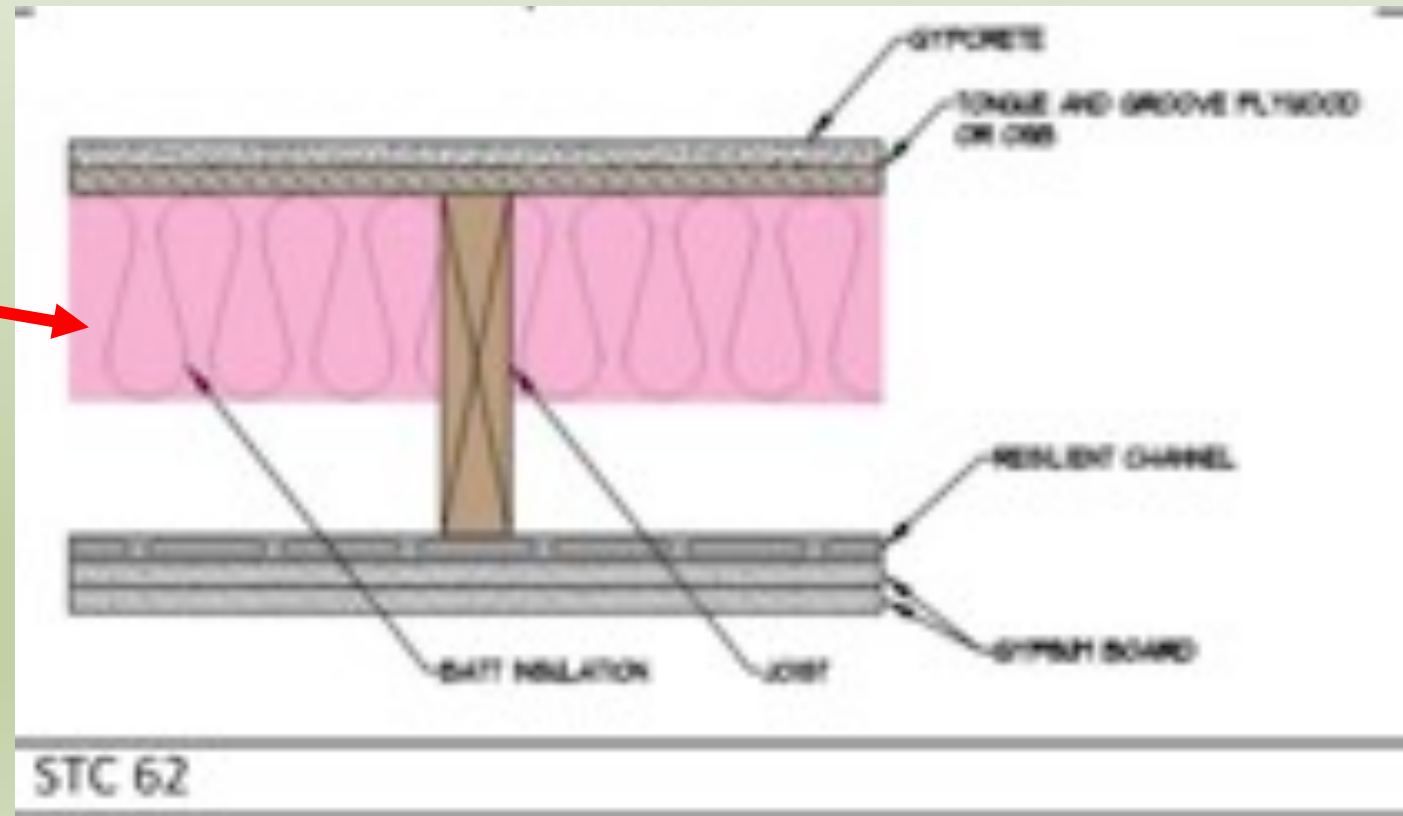
1. Add Mass
2. Add noise barriers
3. Add decouplers



Acoustical Detailing

What does this look like in typical wood-frame construction:

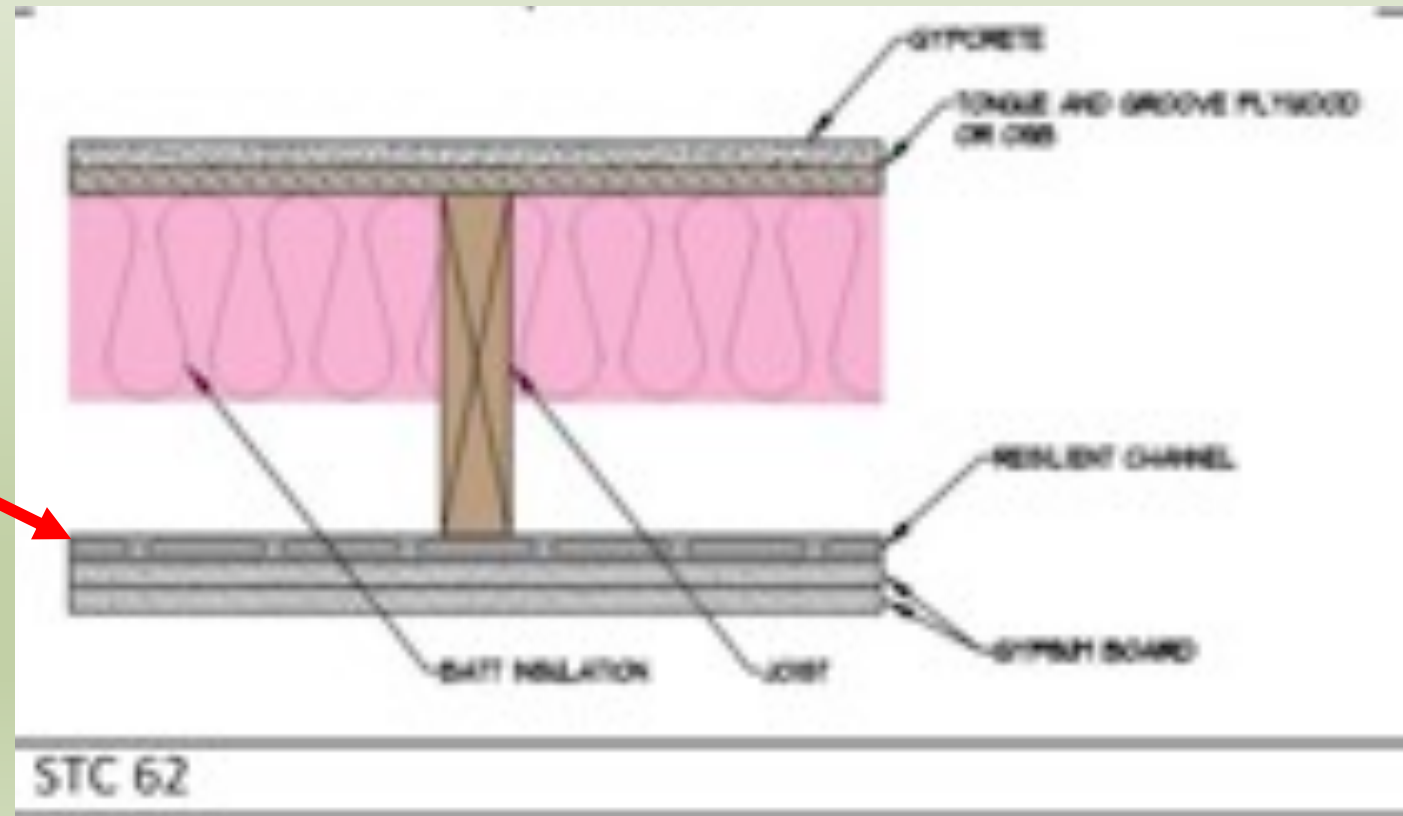
1. Add Mass
2. Add noise barriers
3. Add decouplers



Acoustical Detailing

What does this look like in typical wood-frame construction:

1. Add Mass
2. Add noise barriers
3. Add decouplers



Mass Timber Acoustics

Mass timber has relatively low “mass”

Recall the three ways to increase acoustical performance:

1. **Add Mass**
2. Add noise barriers
3. Add decouplers



Image credit: Christian Columbres

Mass Timber Acoustics



Concrete Slab:

6" Thick

80 PSF

STC 53



CLT Slab:

6-7/8" Thick

18 PSF

STC 41



Mass Timber Acoustics

There are three main ways to improve an assembly's acoustical performance:

1. Add mass
2. Add noise barriers
3. Add decouplers



Mass Timber Acoustics

There are three main ways to improve an assembly's acoustical performance:

1. Add mass
2. Add noise barriers
3. Add decouplers



Acoustical Mat:

- Typically roll out or board products
- Thicknesses vary: Usually $\frac{1}{4}$ " to 1" +



Image credit: Maxxon

Mass Timber Acoustics

Common mass timber floor assembly:

- Finish floor (if applicable)
- Underlayment (if finish floor)
- 1.5'' to 4'' thick concrete/gypcrete topping
- Acoustical mat
- WSP (if applicable)
- Mass timber floor panels



Solutions Paper

Mass Timber Acoustics



Acoustics and Mass Timber: Room-to-Room Noise Control

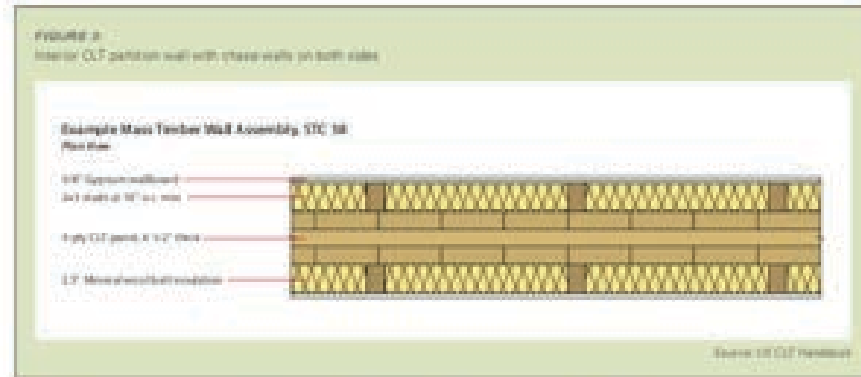
Perford McCann, P.E., SE • Senior Technical Director • Minneapolis



TS Minnesota
Assistant: MJJ / Michael Owen Architecture, CLT Core
Structural Engineer: Magnusson Klemencic Associates
Design Team: + Burt (Shawcraft)

The growing availability and code acceptance of mass timber—a large solid wood panel product such as cross-laminated timber (CLT) and nail-laminated timber (NLT)—for floor, wall and roof construction has given designers a low-carbon alternative to steel, concrete, and masonry for many applications. However, the use of mass timber in multi-family and commercial buildings presents unique acoustic challenges.

While laboratory measurements of the impact and airborne sound isolation of traditional building assemblies such as light wood frame, steel and concrete are widely available, fewer resources exist that quantify the acoustic performance of mass timber assemblies. Additionally, one of the most desired aspects of mass timber construction is the ability to leave a building's structure exposed as finish, which creates the need for appropriate assemblies. With careful design and detailing, mass timber buildings can meet the acoustic performance expectations of most building types.



Mass Timber Assembly Options: Walls

Mass timber panels can also be used for interior and exterior walls—both bearing and non-bearing. For interior walls, the need to conceal services such as electrical and plumbing is an added consideration. Common approaches include building a chase wall in front of the mass timber wall or installing gypsum wallboard on resilient channels that are attached to the mass timber wall. As with bare mass timber floor panels, bare mass timber walls don't typically provide adequate noise control, and chase walls also function as acoustical improvements. For example, a 3-ply CLT wall panel with a thickness of 3.07" has an STC rating of 33⁺. In contrast, Figure 3 shows an interior CLT partition wall with chase walls on both sides. This assembly achieves an STC rating of 58, exceeding the IBC's acoustical requirements for multi-family construction. Other examples are included in the inventory of tested assemblies noted above.

Acoustical Differences between Mass Timber Panel Options

The majority of acoustically-tested mass timber assemblies include CLT. However, tests have also been done on other mass timber panel options such as NLT and dowel-laminated timber (DLT), as well as traditional heavy timber options such as tongue and groove decking. Most tests have concluded that CLT acoustical performance is slightly better than that of other mass timber options, largely because the cross-lamination of laminations in a CLT panel limits sound flanking.

For those interested in comparing similar assemblies and mass timber panel types and thicknesses, the inventory noted above contains tested assemblies using CLT, NLT, glued-laminated timber panels (GLT), and tongue and groove decking.

Improving Performance by Minimizing Flanking

Even when the assemblies in a building are carefully designed and installed for high acoustical performance, consideration of flanking paths—in areas such as assembly intersections, beam-to-column/wall connections, and NRP penetrations—is necessary for a building to meet overall acoustical performance objectives.

One way to minimize flanking paths at these connections and interfaces is to use resilient connection isolation and resilient strips. These products are capable of resisting structural loads in compression between structural members and connections while providing isolation and breaking hard, direct connections between members. In the context of the three methods for improving acoustical performance noted above, these strips act as decouplers. With straight connections, interfaces and penetrations, there is a much greater chance that the acoustical performance of a mass timber building will meet expectations.



Acoustical isolation strips

Photo: Perford

Inventory of Tested Assemblies



Acoustically-Tested Mass Timber Assemblies

Following is a list of mass timber assemblies that have been acoustically tested as of January 23, 2019. Sources are noted at the end of this document. For free technical assistance on any questions related to the acoustical design of mass timber assemblies, or free technical assistance related to any aspect of the design, engineering or construction of a commercial or multi-family wood building in the U.S., email help@woodworks.org or contact the WoodWorks Regional Director nearest you: <http://www.woodworks.org/project-assistance>

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<http://bit.ly/mass-timber-assemblies>

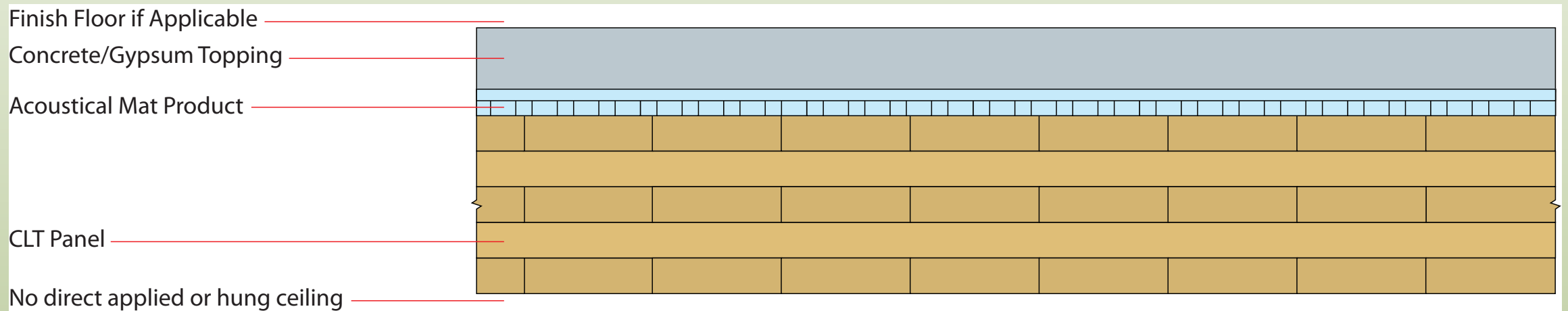
Table 1: CLT Floor Assemblies with Concrete/Gypsum Topping, Ceiling Side Exposed

(4)

						
CLT Panel	Concrete/Gypsum Topping	Acoustical Mat Product Between CLT and Topping	Finish Floor	STC ¹	IC ²	Source
CLT 5-ply (6.875")	1-1/2" Gyp-Crete [®]	Maxxon Acousti-Mat [®] 3/4	None	47 ¹ ASTC	47 ¹ AHC	1
			LVT	-	49 ¹ AHC	
			Carpet + Pad	-	75 ¹ AHC	
			LVT on Acousti-Top [®]	-	52 ¹ AHC	
			Eng Wood on Acousti-Top [®]	-	51 ¹ AHC	
		Maxxon Acousti-Mat [®] N Premium	None	49 ¹ ASTC	45 ¹ AHC	
			LVT	-	47 ¹ AHC	
			LVT on Acousti-Top [®]	-	49 ¹ AHC	
	1-1/2" Levelock [®] Brand 2500	USG SAM N75 Ultra	None	45 ¹	39 ¹	15
			LVT	48 ¹	47 ¹	16
			LVT Plus	48 ¹	49 ¹	58
			Eng Wood	47 ¹	47 ¹	59
			Carpet + Pad	45 ¹	67 ¹	60
			Ceramic Tile	50 ¹	46 ¹	61
		Soprema [®] Innomat	None	45 ¹	42 ¹	15
			LVT	48 ¹	44 ¹	16
			LVT Plus	48 ¹	47 ¹	58
			Eng Wood	47 ¹	45 ¹	59
			Carpet + Pad	45 ¹	71 ¹	60
			Ceramic Tile	50 ¹	46 ¹	61
		USG SAM N75 Ultra	None	45 ¹	38 ¹	15
			LVT	48 ¹	47 ¹	16
			LVT Plus	48 ¹	49 ¹	58
			Eng Wood	47 ¹	49 ¹	59

MT Acoustics Inventory

5-Ply (6.875") CLT Floor Assemblies with Concrete/Gypsum Topping, Ceiling Side Exposed



86 Tests Completed. Of these:

32 Have STC & IIC 50 or greater

7 Have STC & IIC 55 or greater

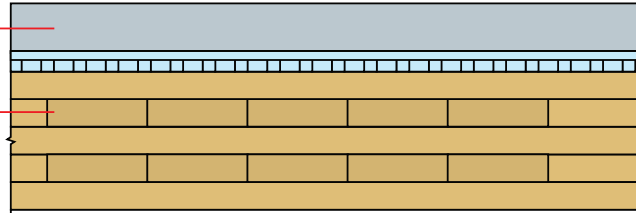
1" Bare Gypsum (no finish floor)

Tall Timber Assemblies

Without Dropped Ceiling

Minimum 1" noncombustible material

Mass timber floor panel



STC 50

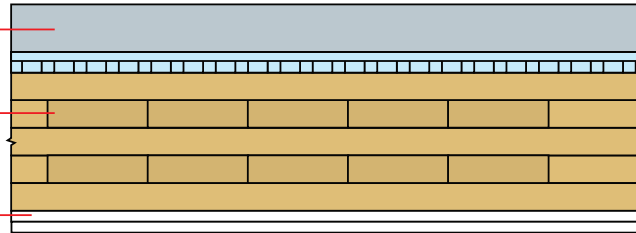
IIC 40

Without Dropped Ceiling

Minimum 1" noncombustible material

Mass timber floor panel

Two layers 5/8" Type X gypsum*



**Applicable to most locations; limited exposed mass timber permitted in IV-B*

STC 52

IIC 46

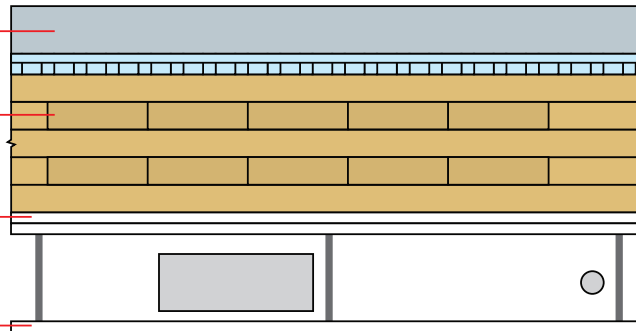
With Dropped Ceiling

Minimum 1" noncombustible material

Mass timber floor panel

Two layers 5/8" Type X gypsum

Dropped ceiling



STC 63

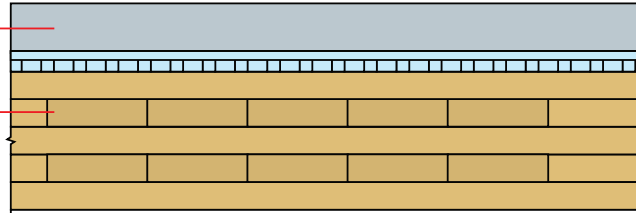
IIC 60

LVT on 1" Gypsum

Without Dropped Ceiling

Minimum 1" noncombustible material

Mass timber floor panel



STC 51

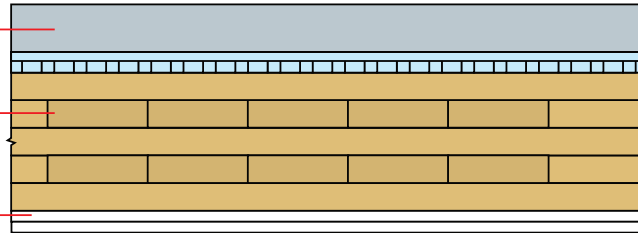
IIC 43

Without Dropped Ceiling

Minimum 1" noncombustible material

Mass timber floor panel

Two layers 5/8" Type X gypsum*



**Applicable to most locations; limited exposed mass timber permitted in IV-B*

STC 52

IIC 48

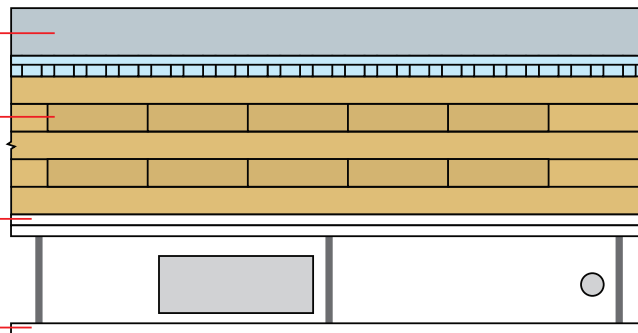
With Dropped Ceiling

Minimum 1" noncombustible material

Mass timber floor panel

Two layers 5/8" Type X gypsum

Dropped ceiling



STC 63

IIC 63

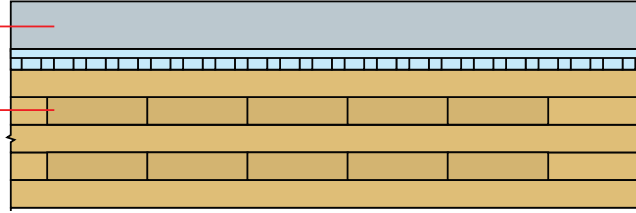
2" Bare Concrete (no finish floor)

Tall Timber Assemblies

Without Dropped Ceiling

Minimum 1" noncombustible material

Mass timber floor panel



STC 52

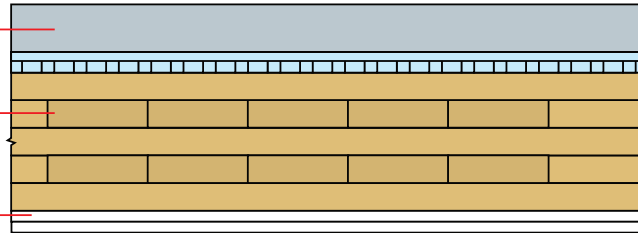
IIC 46

Without Dropped Ceiling

Minimum 1" noncombustible material

Mass timber floor panel

Two layers 5/8" Type X gypsum*



STC 59

IIC 52

**Applicable to most locations; limited exposed mass timber permitted in IV-B*

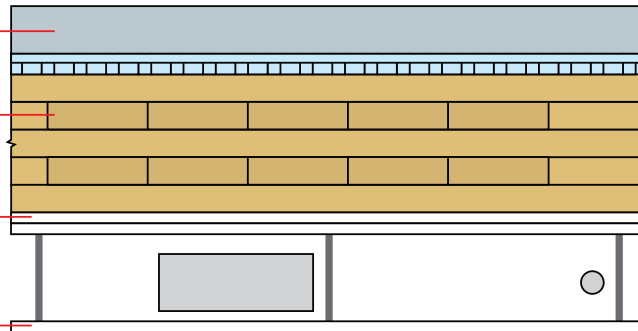
With Dropped Ceiling

Minimum 1" noncombustible material

Mass timber floor panel

Two layers 5/8" Type X gypsum

Dropped ceiling



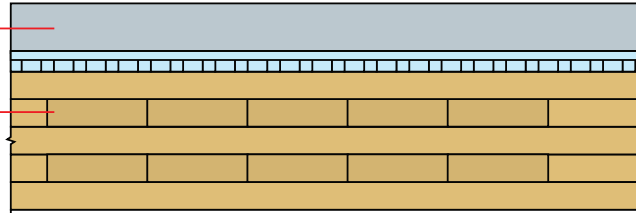
NA

LVT on 2" Concrete

Without Dropped Ceiling

Minimum 1" noncombustible material

Mass timber floor panel



STC 53

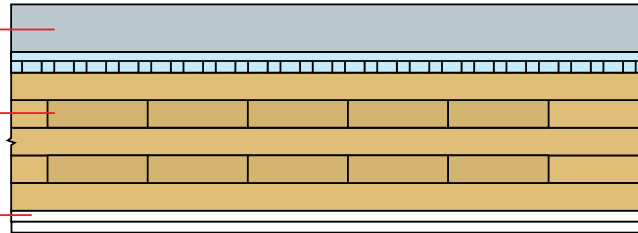
IIC 52

Without Dropped Ceiling

Minimum 1" noncombustible material

Mass timber floor panel

Two layers 5/8" Type X gypsum*



STC 58

IIC 55

**Applicable to most locations; limited exposed mass timber permitted in IV-B*

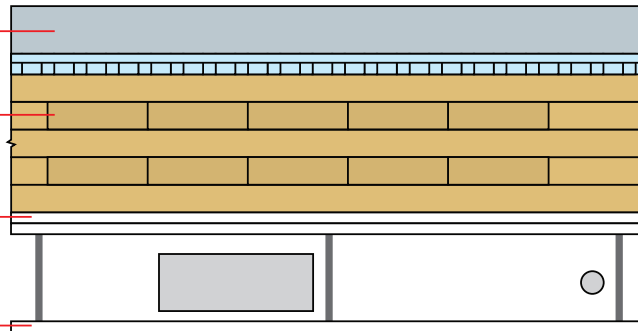
With Dropped Ceiling

Minimum 1" noncombustible material

Mass timber floor panel

Two layers 5/8" Type X gypsum

Dropped ceiling



NA



CONNECTIONS IN TALL WOOD

Photo: Structurlam

Connection Fire Protection

In Construction Types IV-A, IV-B & IV-C, building elements are required to be FRR as specified in IBC Tables 601 and 602. Connections between these building elements must be able to maintain FRR no less than that required of the connected members.



Photo: MyTiCon

16.3 Wood Connections

Wood connections, including connectors, fasteners, and portions of wood members included in the connection design, shall be protected from fire exposure for the required fire resistance time. Protection shall be provided by wood, fire-rated gypsum board, other approved materials, or a combination thereof.

Source: NDS

Connection Fire Protection

Many ways to demonstrate connection fire protection: calculations, prescriptive NC, test results, others as approved by AHJ



Photo: John Stamets



Photo: Josh Partee



Photo: Christian Columbres

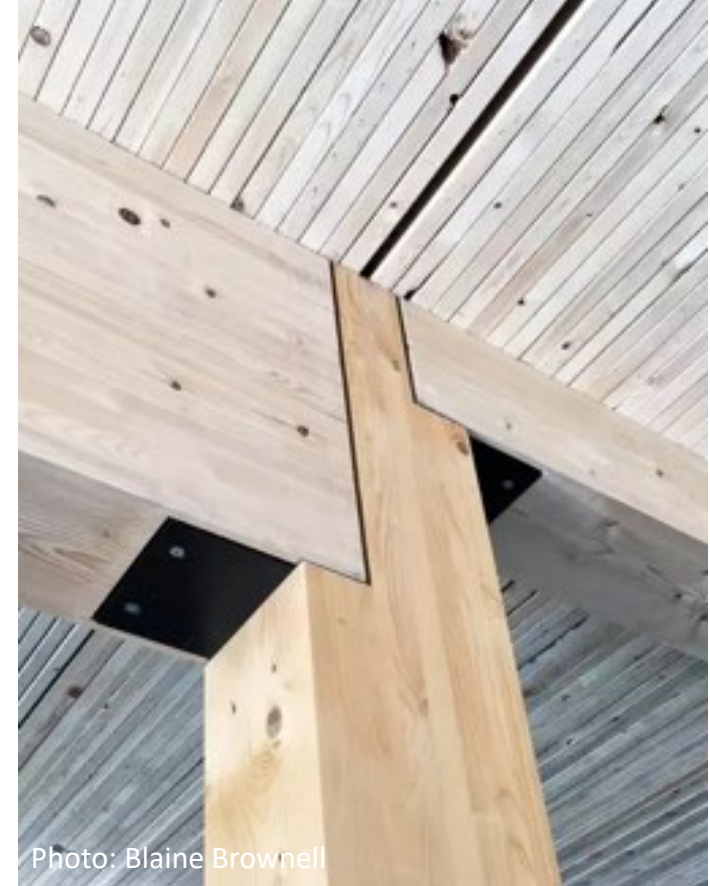


Photo: Blaine Brownell

Connection Fire Protection

**2017 Glulam Beam to Column Connection
Fire Tests under standard ASTM E119
time-temperature exposure**



Connection Fire Protection

Softwood Lumber Board Glulam Connection Fire Test Summary Report

Issue | June 5, 2017

Full Report Available at:

<https://www.thinkwood.com/wp-content/uploads/2018/01/reThink-Wood-Arup-SLB-Connection-Fire-Testing-Summary-web.pdf>





PENETRATIONS IN TALL WOOD

Photo: Alex Schreyer

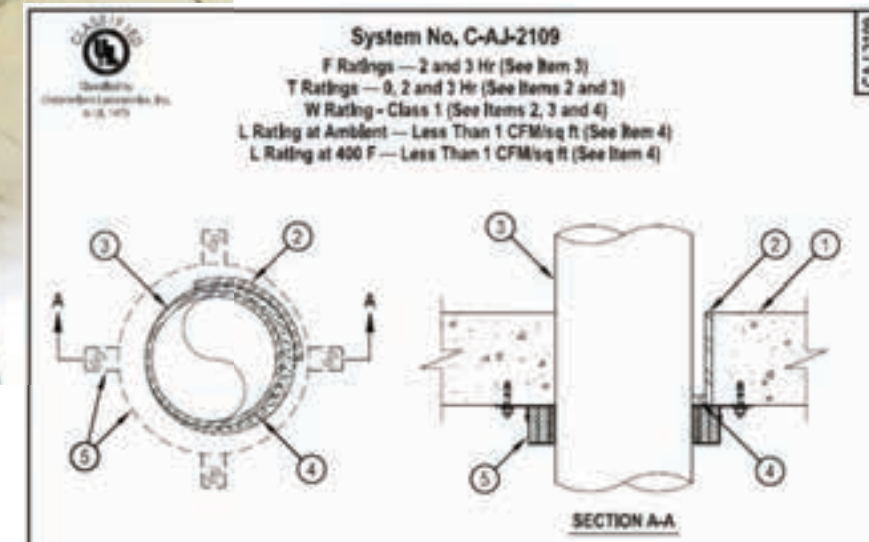
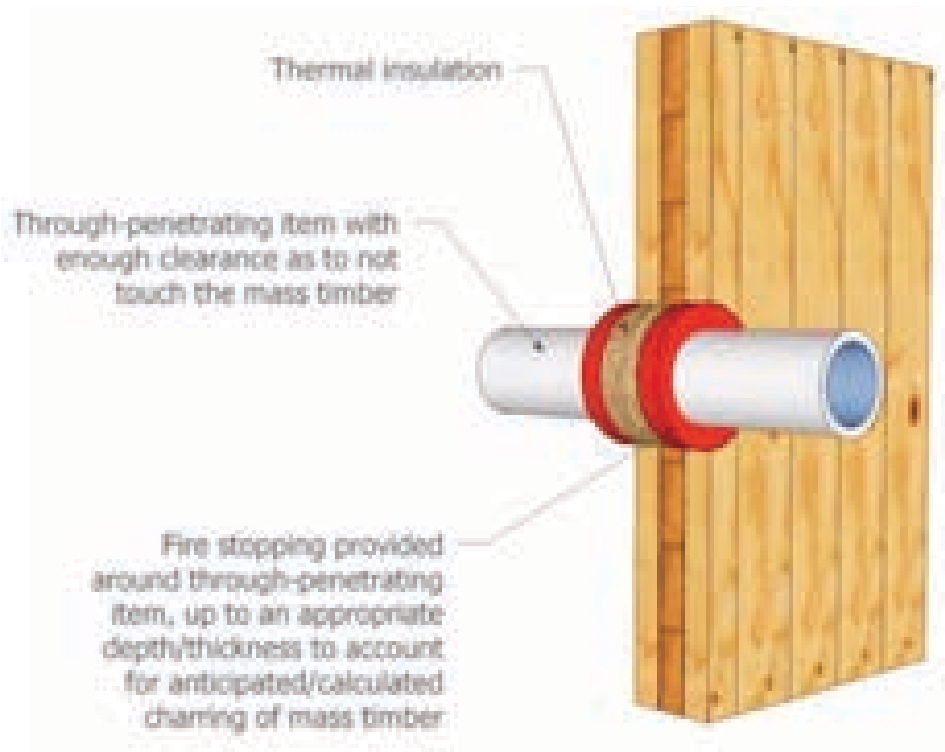
Penetration Fire Protection

Although not a new code requirement or specific to tall wood, more testing & information is becoming available on firestopping of penetrations through MT assemblies



Penetration Fire Protection

Most firestopping systems include combination of fire safing (eg. noncombustible materials such as mineral wool insulation) plus fire caulk



Penetration Fire Protection

Inventory of Fire Tested Penetrations in MT Assemblies



Table 3: North American Fire Tests of Penetrations and Fire Stops in CLT Assemblies

CLT Panel	Exposed Side Protection	Penetrating Item	Penetration Condition or Offset in Hole	Firestopping System Description	F Rating	T Rating	Related Test Protocol	Source	Testing Lab
3-ply (Thomson 3.07'')	None	1.5" diameter data/cable bundle	Centered	1.5 in diameter hole. Mineral wool was installed in the 1 in. annular space around the data cable to a total depth of approximately 2 - 3.6 in. The remaining 1 in. annular space from the top of the mineral wool to the top of the floor assembly was filled with Hilti PS-One Max caulking.	1 hour	0.5 hour	CANULC 510.1	24	Intertek March 30, 2016
3-ply (Thomson 3.07'')	None	2" copper pipe	Centered	4.975 in diameter hole. Pipe wrap was installed around the copper pipe to a total depth of approximately 2 - 3.6 in. The remaining 1 in. annular space starting at the top of the mineral wool to the top of the floor assembly was filled with Hilti PS-One Max caulking.	1 hour	NA	CANULC 510.1	24	Intertek March 30, 2016
3-ply (Thomson 3.07'')	None	2.3" schedule 40 pipe	Centered	4.92 in diameter hole. Pipe wrap was installed around the schedule 40 pipe to a total depth of approximately 2 - 3.6 in. The remaining 1 in. annular space starting at the top of the pipe wrap to the top of the floor assembly was filled with Hilti PS-One Max caulking.	1 hour	NA	CANULC 510.1	24	Intertek March 30, 2016
3-ply (Thomson 3.07'')	None	6" cast iron pipe	Centered	6.31 in diameter hole. Mineral wool was installed in the 1 in. annular space around the cast iron pipe to a total depth of approximately 2 - 3.6 in. The remaining 1 in. annular space starting at the top of the pipe wrap to the top of the floor assembly was filled with Hilti PS-One Max caulking.	1 hour	NA	CANULC 510.1	24	Intertek March 30, 2016
3-ply (Thomson 3.07'')	None	Hilti 4 in drop in device System No. F-B-2049	Centered	6.01" diameter hole. Mineral wool was installed in the 1 - 1.6 in. annular space around the drop-in device to a total depth of approximately 1 - 3.6 in and the remaining 1 in. annular space from the top of the mineral wool to the top edge of the 9 - 1.6 in. hole in the CLT was filled with Hilti PS-One Max caulking.	1 hour	0.75 hour	CANULC 510.1	24	Intertek March 30, 2016
3-ply CLT (131 mm 5.16'')	None	1.5" diameter data/cable bundle	Centered	1.5" diameter hole. Mineral wool was installed in the 1 in. annular space around the data cable to a total depth of approximately 4 - 3.32 in. The remaining 1 in. annular space from the top of the mineral wool to the top of the floor assembly was filled with Hilti PS-One Max caulking.	2 hours	1.5 hours	CANULC 510.1	24	Intertek March 30, 2016
3-ply CLT (131 mm 5.16'')	None	2" copper pipe	Centered	4.975 in diameter hole. Pipe wrap was installed around the copper pipe to a total depth of approximately 4 - 3.32 in. The remaining 1 in. annular space starting at the top of the mineral wool to the top of the floor assembly was filled with Hilti PS-One Max caulking.	2 hours	NA	CANULC 510.1	24	Intertek March 30, 2016
3-ply CLT (131 mm 5.16'')	None	2.3" schedule 40 pipe	Centered	4.92 in diameter hole. Pipe wrap was installed around the schedule 40 pipe to a total depth of approximately 4 - 3.32 in. The remaining 1 in. annular space starting at the top of the pipe wrap to the top of the floor assembly was filled with Hilti PS-One Max caulking.	2 hours	0.5 hour	CANULC 510.1	24	Intertek March 30, 2016
3-ply CLT (131 mm 5.16'')	None	6" cast iron pipe	Centered	6.31 in diameter hole. Mineral wool was installed in the 1 in. annular space around the cast iron pipe to a total depth of approximately 4 - 3.32 in. The remaining 1 in. annular space starting at the top of the pipe wrap to the top of the floor assembly was filled with Hilti PS-One Max caulking.	2 hours	NA	CANULC 510.1	24	Intertek March 30, 2016
3-ply CLT (131 mm 5.16'')	None	Hilti 4 in drop in device System No. F-B-2049	Centered	6.01" diameter hole. Mineral wool was installed in the 1 - 1.6 in. annular space around the drop-in device to a total depth of approximately 1 - 3.6 in and the remaining 1 in. annular space from the top of the mineral wool to the top edge of the 9 - 1.6 in. hole in the CLT was filled with Hilti PS-One Max caulking.	2 hours	1.5 hours	CANULC 510.1	24	Intertek March 30, 2016
3-ply (1 Thomson 3.07'')	None	1" nominal PVC pipe	Centered	6.21 in diameter with a 3/4 in plywood and steel bush with the top of the slab reducing the opening to 2.24 in. Two wraps of Hilti CP-entel WR11 1.5x4' Firestop wrap wrap at two locations with a 30 gauge steel plate which extended from the top of the slab to 1 in below the slab. The first location was with the bottom of the wrap wrap flush with the bottom of the steel plate and the second was with the bottom of the wrap wrap 7 in. from the bottom of the slab. The void between the steel plate and the CLT and between the steel plate and pipe at the top was filled with Rammed Cellulose mineral wool leaving a 1/8 in deep void at the top of the assembly. Hilti PS-One Max for concrete Penetration Sealant was applied to a depth of 3/4 in on the top of the assembly, between the plywood and steel plate as well as the steel plate and pipe.	2 hours	2 hours	ASTM D814	24	QAI Laboratory March 3, 2017

Tall Wood Buildings in the 2021 IBC *Up to 18 Stories of Mass Timber*

By: Beneman, PhD, PE, WoodWorks • Wood Products Council • Matt Timmers, SE, John A. Martin & Associates
• Dennis Richardson, PE, CBC, CMAA, American Wood Council

In January 2019, the International Code Council (ICC) approved a set of proposals to allow tall wood buildings as part of the 2021 International Building Code (IBC). Based on these proposals, the 2021 IBC will include three new construction types—Type IV-A, IV-B and IV-C—allowing the use of mass timber or noncombustible materials. These new types are based on the previous Heavy Timber construction type (renamed Type IV-HT) but with additional fire-resistance ratings and levels of required noncombustible protection. The code will include provisions for up to 18 stories of Type IV-A construction for Business and Residential Occupancies.

Based on information first published in the Structural Engineers Association of California (SEAOC) 2018 Conference Proceedings, this paper summarizes the background to these proposals, technical research that supported their adoption, and resulting changes to the IBC and product-specific standards.

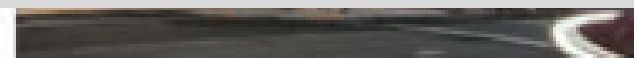
Background: ICC Tall Wood Building Ad Hoc Committee

Over the past 10 years, there has been a growing interest in tall buildings constructed from mass timber materials (Beneman 2013, Timmers 2016). Around the world there



WoodWorks Tall Wood Design Resources

http://www.woodworks.org/wp-content/uploads/wood_solution_paper-TALL-WOOD.pdf



TECHNICAL BRIEF

Demonstrating Fire-Resistance Ratings for Mass Timber Elements in Tall Wood Structures

Richard McLain, PE, SE • Senior Technical Director – Tall Wood, WoodWorks

Changes to the 2021 International Building Code (IBC) have created opportunities for wood buildings that are much larger and taller than prescriptively allowed in past versions of the code. Occupant safety, and the need to ensure fire performance in particular, was a fundamental consideration as the changes were developed and approved. The result is three new construction types—Type IV-A, IV-B and IV-C—which are based on the previous Heavy Timber construction type (renamed Type IV-HT), but with additional fire protection requirements.

One of the main ways to demonstrate that a building will meet the required level of passive fire protection, regardless of structural materials, is through hourly fire-resistance ratings (FRRs) of its elements and assemblies. The IBC defines an FRR as *the period of time a building element, component or assembly maintains the ability to confine a fire, continues to perform a given structural function, or both, as determined by the tests, or the methods based on tests, prescribed in Section 703.*

FRRs for the new construction types are similar to those required for Type I construction, which is primarily steel and concrete.¹ (See Table 1.) They are found in IBC Table 601, which includes FRR requirements for all construction types and building elements; however, other code sections should be checked for overriding provisions (e.g., occupancy separation, shaft enclosures, etc.) that may alter the requirement.



Image: Korb + Associates Architects

TABLE 1:

FRR Requirements (Hours) for Tall Mass Timber Construction Types and Existing Type I

Building Element	I-A Unlimited stories, max. 12 ft. clear height	IV-A Max. 18 stories, max. 12 ft. clear height	I-B Max. 12 stories, max. 12 ft. clear height	IV-B Max. 12 stories, max. 12 ft. clear height	IV-C Max. 9 stories, max. 12 ft. clear height
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Tall Timber Fire-Resistance Design

TECHNICAL BRIEF

Shaft Wall Requirements in Tall Mass Timber Buildings

Richard McLain, PE, SE • Senior Technical Director • Tall Wood, WoodWorks

The 2021 International Building Code (IBC) introduced three new construction types—Type IV-A, IV-B and IV-C—which allow tall mass timber buildings. For details on the new types and their requirements, see the WoodWorks paper, *Tall Wood Buildings in the 2021 IBC – Up to 18 Stories of Mass Timber*.² This paper builds on that document with an in-depth look at the requirements for shaft walls, including when and where wood can be used.

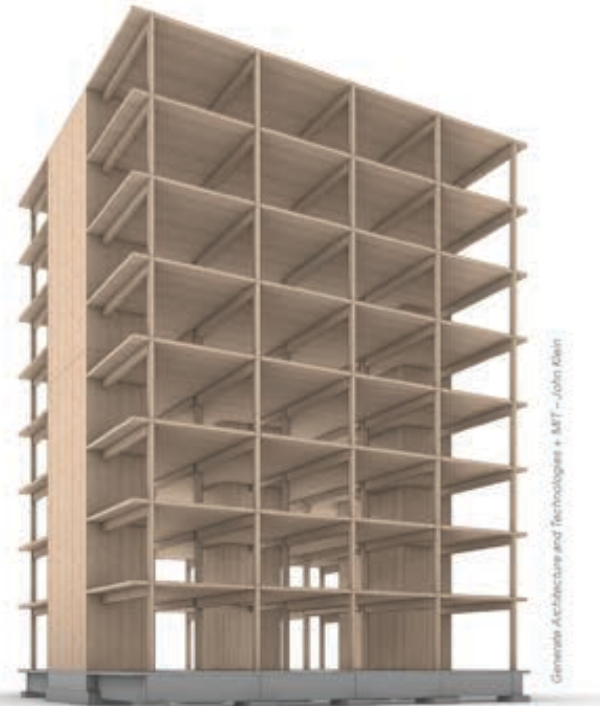
Shaft Enclosure Requirements in the 2021 IBC

A shaft is defined in Section 202 of the 2021 IBC as “an enclosed space extending through one or more stories of a building, connecting vertical openings in successive floors, or floors and roof.” Therefore, shaft enclosure requirements apply to stairs, elevators, and mechanical/electrical/plumbing (MEP) chases in multi-story buildings. While these applications may be similar in their fire design requirements, they tend to differ in terms of their assemblies, detailing, and construction constraints.

Shaft enclosures are specifically addressed in IBC Section 713. However, because shaft enclosure walls must be constructed as fire barriers per Section 713.2, many shaft wall requirements reference provisions for fire barriers found in Section 707.

Allowable Shaft Wall Materials

Provisions addressing materials permitted in shaft wall



Generative Architecture and Technologies • MIT • John Klein

A relatively new category of wood products, mass timber can

Shaft Enclosure Design in Tall Timber

utilizing construction Types IV-A, IV-B, or IV-C is that they
be constructed of either mass timber or noncombustible

Structural elements of Type IV construction primarily of

QUESTIONS?

This concludes The
American Institute of
Architects Continuing
Education Systems
Course

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