

An architectural rendering of a modern, multi-story building with a prominent wood-clad facade. The building features large, rectangular windows that reflect the sky and surrounding environment. The ground floor has a recessed entrance area with a wooden ceiling. The building is surrounded by trees and a sidewalk with pedestrians, suggesting an urban setting.

New Tall Wood Code Provisions: Advanced Fire Design for Exposed Timber

Presented by Ricky McLain, PE, SE, WoodWorks

NIR Center | Photo: Hennebery Eddy Architects | Architect: Hennebery Eddy Architects

Hennebery Eddy
Architects

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Questions related to specific materials, methods, and services will be addressed at the conclusion of this presentation.



Course Description

The 2021 International Building Code (IBC) includes a series of changes that significantly expand the opportunities for tall timber structures. Three new construction types—Type IV-A, IV-B and IV-C—will allow the use of mass timber or noncombustible materials in buildings up to 18 stories tall. These new types are based on the previous Heavy Timber construction type (renamed Type IV-HT) but with additional fire-resistance ratings and levels of required noncombustible protection. This presentation will take a detailed look at the new code provisions and methods of addressing requirements for fire resistance and exposed timber. Topics will include tall wood-specific high-rise and sprinkler requirements, methods of demonstrating fire-resistance ratings, fire design for penetrations, connections and abutting panels, allowances for exposed timber, exterior walls, concealed spaces, and more.

Learning Objectives

1. Explore the three new tall wood construction types and discuss related code provisions such as allowable heights and fire-resistance ratings.
2. Discuss code-compliant options for exposing mass timber, where up to 2-hour fire-resistance ratings are required, and demonstrate design methodologies for achieving these ratings.
3. Review timber exposure strategies for IV-B construction, emphasizing code compliance topics such as horizontal separation and exposure area limits.
4. Highlight resources available to designers for fire-resistance design in tall timber structures, emphasizing tested assemblies, allowances for concealed spaces and contributions of noncombustible protection layers.

Tall Timber Construction Types



18 STORIES
BUILDING HEIGHT 270'
ALLOWABLE BUILDING AREA 972,000 SF
AVERAGE AREA PER STORY 54,000SF

TYPE IV-A



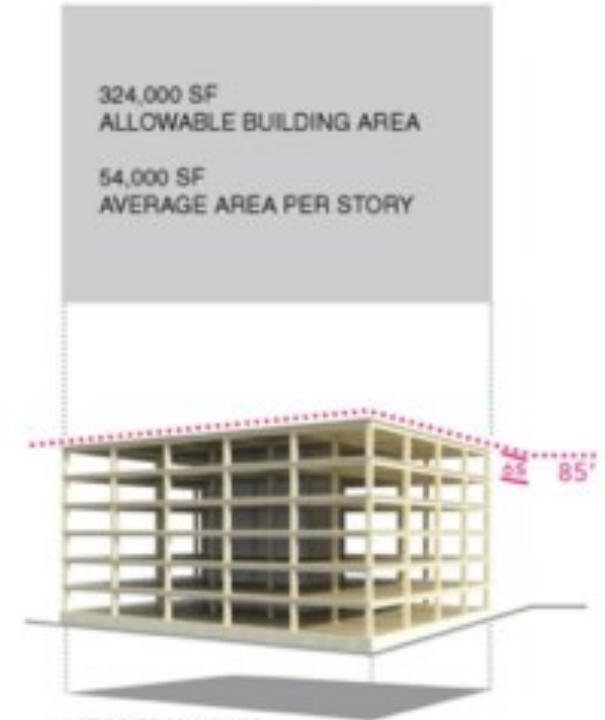
12 STORIES
BUILDING HEIGHT 180 FT
ALLOWABLE BUILDING AREA 648,000 SF
AVERAGE AREA PER STORY 54,000SF

TYPE IV-B



9 STORIES
BUILDING HEIGHT 85'
ALLOWABLE BUILDING AREA 405,000 SF
AVERAGE AREA PER STORY 45,000 SF

TYPE IV-C



6 STORIES MAXIMUM
85'-0" MAXIMUM BUILDING HEIGHT
324,00 SF MAXIMUM AREA

TYPE IV- HT

IBC 2015

BUSINESS OCCUPANCY [GROUP B]

*BUILDING FLOOR-TO-FLOOR HEIGHTS ARE SHOWN AT 12'-0" FOR ALL EXAMPLES FOR CLARITY IN COMPARISON BETWEEN 2015 TO 2021 IBC CODES.

IV-C

Type IV-C Protection vs. Exposed



9 STORIES
BUILDING HEIGHT 85'
ALLOWABLE BUILDING AREA 405,000 SF
AVERAGE AREA PER STORY 45,000 SF

TYPE IV-C

Credit: Susan Jones, atelierjones



Credit: Kaiser+Path, Ema Peter

All Mass Timber surfaces may be exposed

Exceptions: Shafts, concealed spaces, outside face of exterior walls

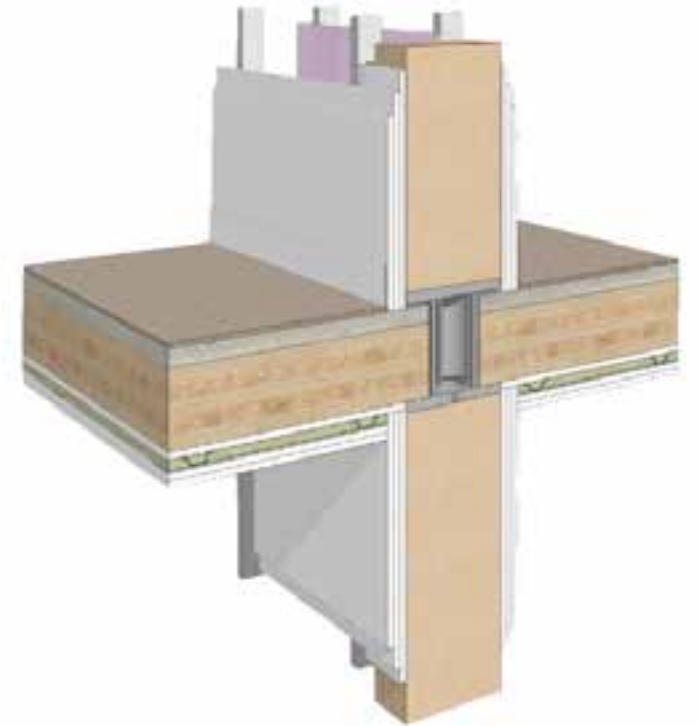
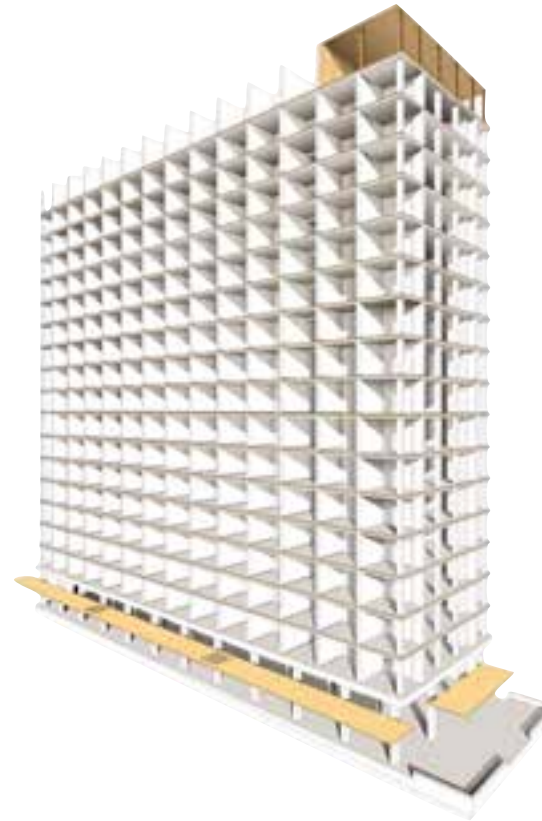
Type IV-A Protection vs. Exposed



18 STORIES
BUILDING HEIGHT 270'
ALLOWABLE BUILDING AREA 972,000 SF
AVERAGE AREA PER STORY 54,000SF

TYPE IV-A

Credit: Susan Jones, atelierjones



100% NC protection on all surfaces of
Mass Timber

Credit: Acton Ostry Architects, Fast + Epp

Type IV-B Protection vs. Exposed

IV-B



12 STORIES
BUILDING HEIGHT 180 FT
ALLOWABLE BUILDING AREA 648,000 SF
AVERAGE AREA PER STORY 54,000SF

TYPE IV-B

Credit: Susan Jones, atelierjones



Credit: Kaiser+Path

NC protection on all surfaces of Mass Timber except limited exposed areas

~20% of Ceiling or ~40% of Wall can be exposed

Type IV-B Protection vs. Exposed

IV-B

Limited Exposed MT allowed in Type IV-B for:

- **MT beams and columns which are not integral part of walls or ceilings, no area limitation applies**
- **MT ceilings and beams up to 20% of floor area in dwelling unit or fire area, or**
- **MT walls and columns up to 40% of floor area in dwelling unit or fire area, or**
- **Combination of ceilings/beams and walls/columns, calculated as follows:**



Credit: Kaiser+Path

Type IV-B Protection vs. Exposed

IV-B

Mixed unprotected areas, exposing both ceilings and walls:

- In each dwelling unit or fire area, max. unprotected area =

$$(U_{tc}/U_{ac}) + (U_{tw}/U_{aw}) \leq 1.0$$

- U_{tc} = Total unprotected MT ceiling areas
- U_{ac} = Allowable unprotected MT ceiling areas
- U_{tw} = Total unprotected MT wall areas
- U_{aw} = Allowable unprotected MT wall areas



Credit: Kaiser+Path

Type IV-B Protection vs. Exposed

IV-B

Design Example: Mixing unprotected MT walls & ceilings



Credit: AWC

800 SF dwelling unit

- $U_{ac} = (800 \text{ SF}) * (0.20) = 160 \text{ SF}$
- $U_{aw} = (800 \text{ SF}) * (0.40) = 320 \text{ SF}$
- **Could expose 160 SF of MT ceiling, OR 320 SF of MT Wall, OR**
- **If desire to expose 100 SF of MT ceiling in Living Room, determine max. area of MT walls that can be exposed**

Type IV-B Protection vs. Exposed

IV-B

Design Example: Mixing unprotected MT walls & ceilings



$$(U_{tc}/U_{ac}) + (U_{tw}/U_{aw}) \leq 1.0$$

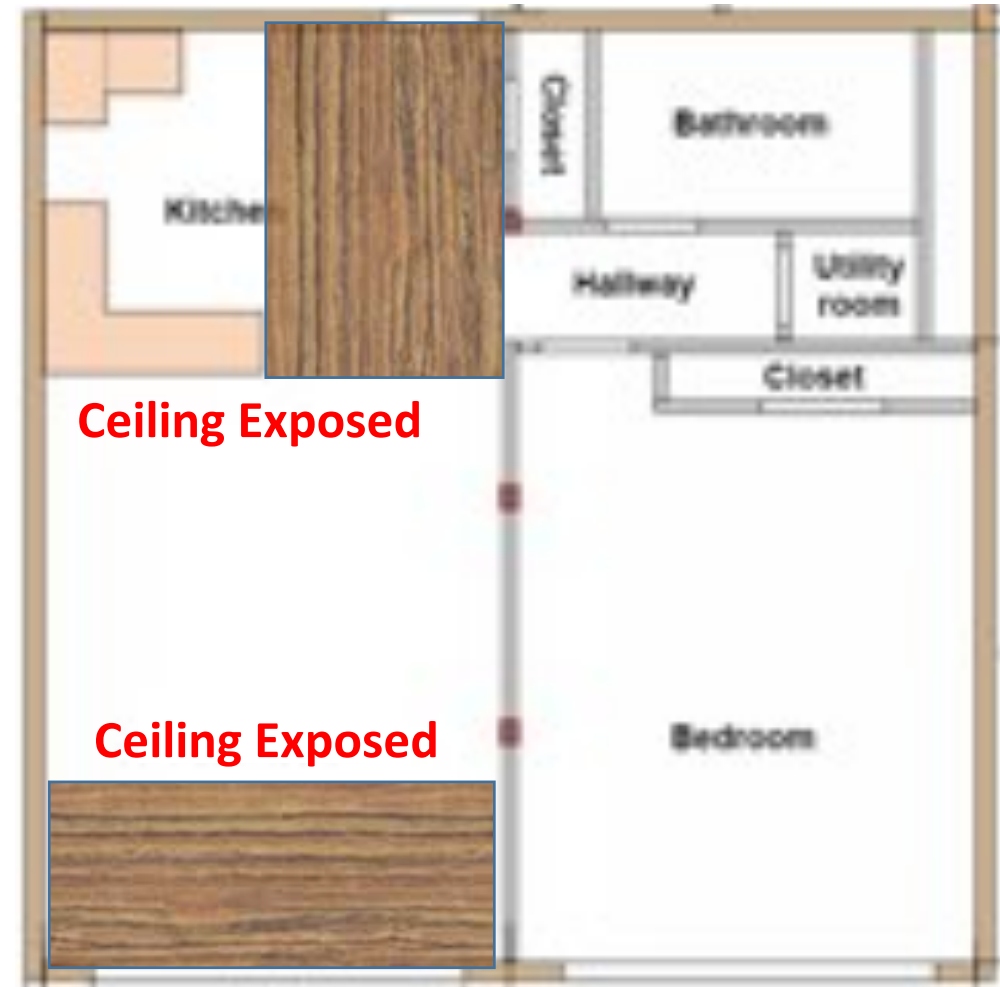
$$(100/160) + (U_{tw}/320) \leq 1.0$$

$$U_{tw} = 120 \text{ SF}$$

- Can expose 120 SF of MT walls in dwelling unit in combination with exposing 100 SF of MT ceiling

Type IV-B Protection vs. Exposed

IV-B



Type IV-B Protection vs. Exposed

IV-B

Horizontal separation of unprotected areas:

- Unprotected portions of mass timber walls and ceilings shall be not less than 15 feet from unprotected portions of other walls and ceilings, measured horizontally along the ceiling and from other unprotected portions of walls measured horizontally along the floor.



Credit: Kaiser+Path

Type IV-B Protection vs. Exposed

IV-B



Tall Wood Building Size Limits

	Construction Type (All <u>Sprinklered Values</u>)						
	I-A	I-B	<u>IV-A</u>	<u>IV-B</u>	<u>IV-C</u>	IV-HT	III-A
Occupancies	Allowable Building Height above Grade Plane, Feet (IBC Table 504.3)						
A, B, R	Unlimited	180	<u>270</u>	<u>180</u>	<u>85</u>	85	85
	Allowable Number of Stories above Grade Plane (IBC Table 505.4)						
A-2, A-3, A-4	Unlimited	12	<u>18</u>	<u>12</u>	<u>6</u>	4	4
B	Unlimited	12	<u>18</u>	<u>12</u>	<u>9</u>	6	6
R-2	Unlimited	12	<u>18</u>	<u>12</u>	<u>8</u>	5	5
	Allowable Area Factor (At) for SM, Feet ² (IBC Table 506.2)						
A-2, A-3, A-4	Unlimited	Unlimited	<u>135,000</u>	<u>90,000</u>	<u>56,250</u>	45,000	42,000
B	Unlimited	Unlimited	<u>324,000</u>	<u>216,000</u>	<u>135,000</u>	108,000	85,500
R-2	Unlimited	Unlimited	<u>184,500</u>	<u>123,000</u>	<u>76,875</u>	61,500	72,000

Non-Tall Opportunities – Large Area

	Construction Type (All <u>Sprinklered Values</u>)						
	I-A	I-B	<u>IV-A</u>	<u>IV-B</u>	<u>IV-C</u>	IV-HT	III-A
Occupancies	Allowable Building Height above Grade Plane, Feet (IBC Table 504.3)						
A, B, R	Unlimited	180	<u>270</u>	<u>180</u>	<u>85</u>	85	85
	Allowable Number of Stories above Grade Plane (IBC Table 505.4)						
A-2, A-3, A-4	Unlimited	12	<u>18</u>	<u>12</u>	<u>6</u>	4	4
B	Unlimited	12	<u>18</u>	<u>12</u>	<u>9</u>	6	6
R-2	Unlimited	12	<u>18</u>	<u>12</u>	<u>8</u>	5	5
	Allowable Area Factor (At) for SM, Feet ² (IBC Table 506.2)						
A-2, A-3, A-4	Unlimited	Unlimited	<u>135,000</u>	<u>90,000</u>	<u>56,250</u>	45,000	42,000
B	Unlimited	Unlimited	<u>324,000</u>	<u>216,000</u>	<u>135,000</u>	108,000	85,500
R-2	Unlimited	Unlimited	<u>184,500</u>	<u>123,000</u>	<u>76,875</u>	61,500	72,000

What's the 'Sweet Spot' for Tall Mass Timber?

Depends on many factors:

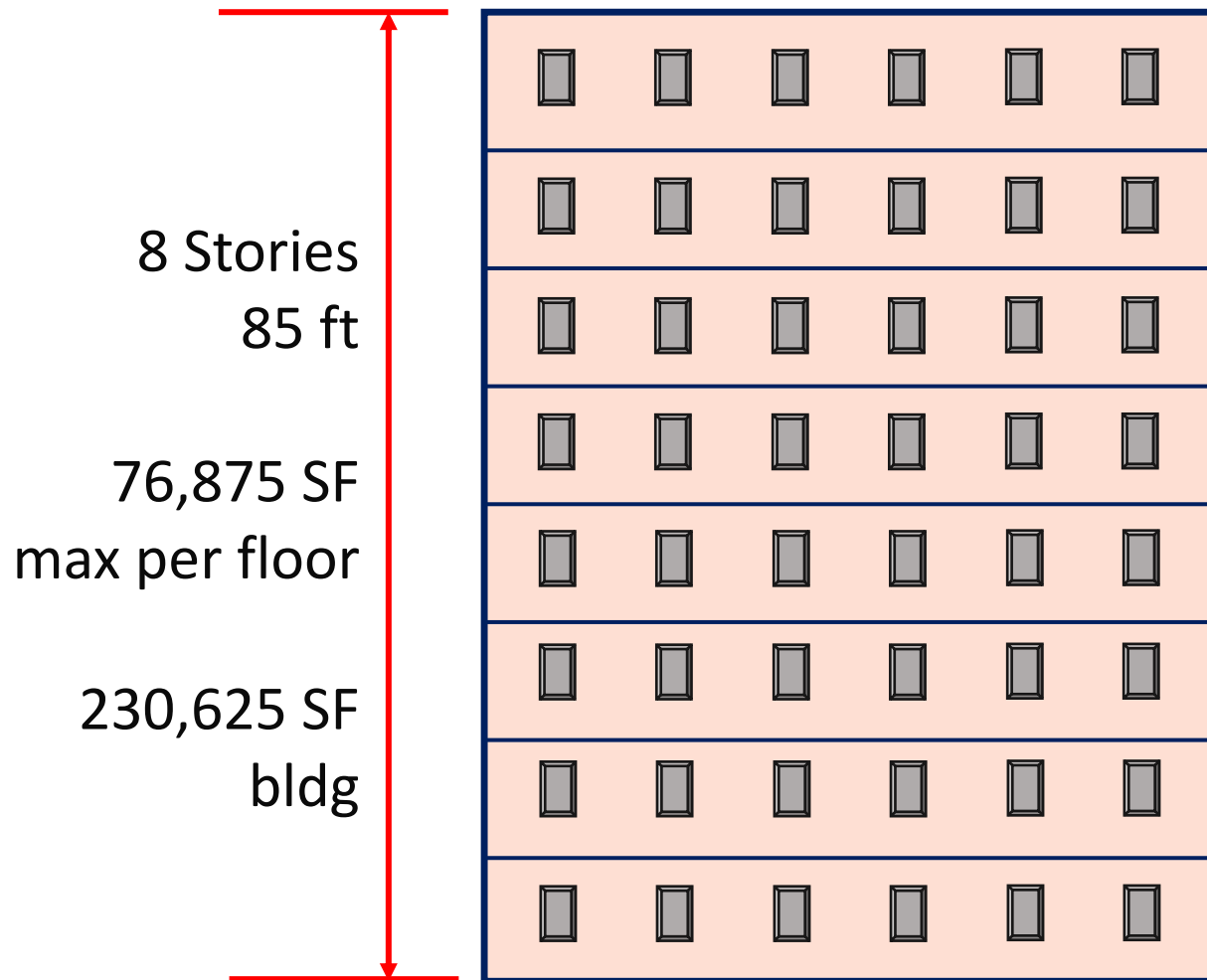
- **Project Use**
- **Site Constraints**
- **Local Zoning & FAR Limitations**
- **Budget**
- **Client Objectives for Sustainability, Exposed Timber**
- **And More...**

But Some General Trends Could Be:

80 M Street, SE, Washington, DC
Photo: Hickok Cole | Architect: Hickok Cole

Type IV-C Tall Mass Timber

Example R-2, Type IV-C Building



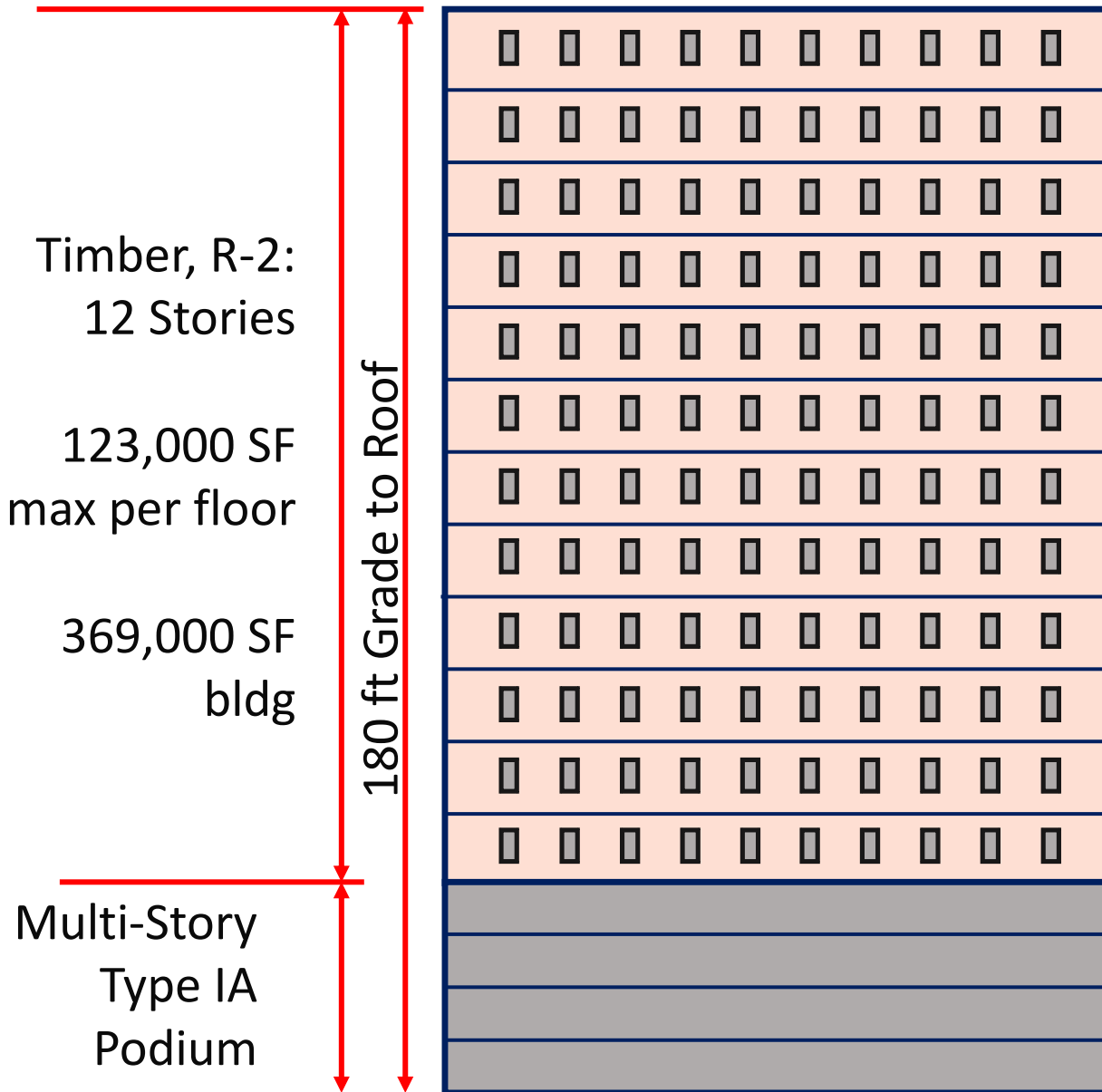
Not Likely to Utilize Podium Due to Overall Building Height Limit (85 ft) Relative to # of Timber Stories (8)

Same Overall Building Height Limit as IV-HT (85 ft) but higher Fire-Resistance Ratings Req'd

3 Additional Stories Permitted Compared to IV-HT

All Timber Exposed

Type IV-B Tall Mass Timber



Example Mixed-Use, Type IV-B Building

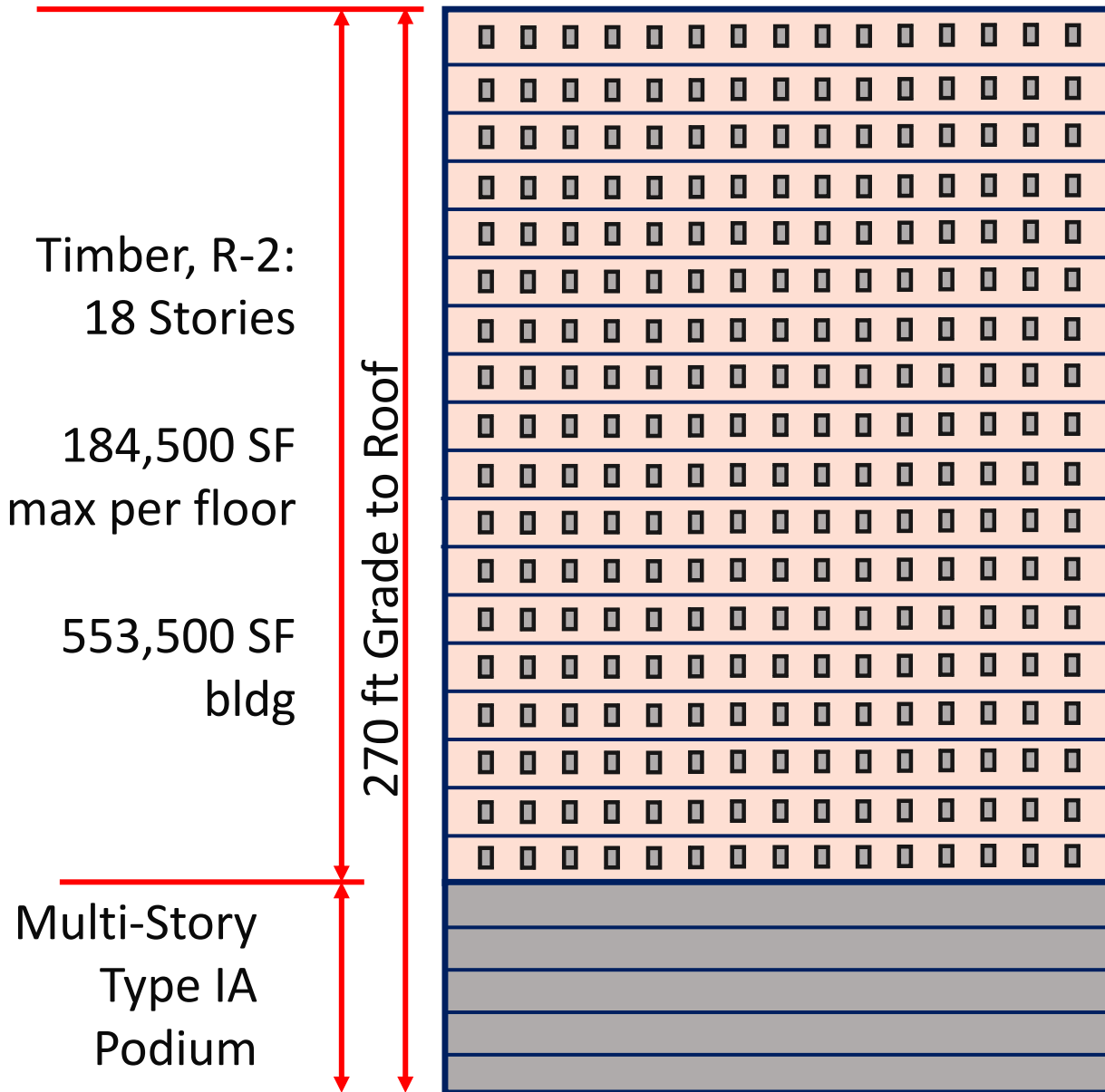
Likely to Utilize Podium Due to Overall Building Height Limit (180 ft) Relative to # of Timber Stories (12)

Same Fire-Resistance Ratings Req'd as IV-C But Limitations on Timber Exposed

4 Additional Stories Permitted Compared to IV-C

Limited Timber Exposed

Type IV-A Tall Mass Timber



Example Mixed-Use, Type IV-A Building

Likely to Utilize Podium Due to Overall Building Height Limit (270 ft) Relative to # of Timber Stories (18)

Higher Fire-Resistance Ratings Req'd than IV-B For Primary Frame

6 Additional Stories Permitted Compared to IV-B

No Exposed Timber Permitted

Materials Permitted

602.4 Type IV. Type IV construction is that type of construction in which the building elements are mass timber or noncombustible materials and have fire resistance ratings in accordance with Table 601. Mass timber elements shall meet the fire resistance rating requirements of this section based on either the fire resistance rating of the noncombustible protection, the mass timber, or a combination of both and shall be determined in accordance with Section 703.2 or 703.3. The minimum dimensions and permitted materials for building elements shall comply with the provisions of this section and Section 2304.11. Mass timber

Exterior load-bearing walls and nonload-bearing walls shall be mass timber construction, or shall be of noncombustible construction.

Exception: Type IV-HT Construction in accordance with Section 602.4.4.

The interior building elements, including nonload-bearing walls and partitions, shall be of mass timber construction or of noncombustible construction.

Exception: Type IV-HT Construction in accordance with Section 602.4.4..

MT Type IV Minimum Sizes

In addition to meeting FRR, all MT elements must also meet minimum sizes

These minimum sizes have been in place for old type IV (current type IV-HT) construction and the same minimums sizes also apply to MT used in new types IV-A, IV-B and IV-C

Contained in IBC 2304.11



Type IV Minimum Sizes - Framing

Framing		Solid Sawn (nominal)	Glulam (actual)	SCL (actual)
Floor	Columns	8 x 8	6 ³ / ₄ x 8 ¹ / ₄	7 x 7 ¹ / ₂
	Beams	6 x 10	5 x 10 ¹ / ₂	5 ¹ / ₄ x 9 ¹ / ₂
Roof	Columns	6 x 8	5 x 8 ¹ / ₄	5 ¹ / ₄ x 7 ¹ / ₂
	Beams*	4 x 6	3 X 6 ⁷ / ₈	3 ¹ / ₂ X 5 ¹ / ₂

Minimum Width by Depth in Inches
See IBC 2018 2304.11 or IBC 2015 602.4 for Details

*3" nominal width allowed where sprinklered



Photo: WoodWorks

Interior Wall Construction Recap



IV-A

IV-B

IV-C

IV-HT

Fire Rating (bearing wall)

3 Hr

2 Hr

2 Hr

1 Hr or HT*

Construction – MT

Laminated construction 4" thick (CLT, NLT, etc)
Solid wood construction min. 2 layers of 1" matched boards

NC Protection

Per Interior Requirements

No

Noncombustible non-bearing wall

0 Hr

1 Hr

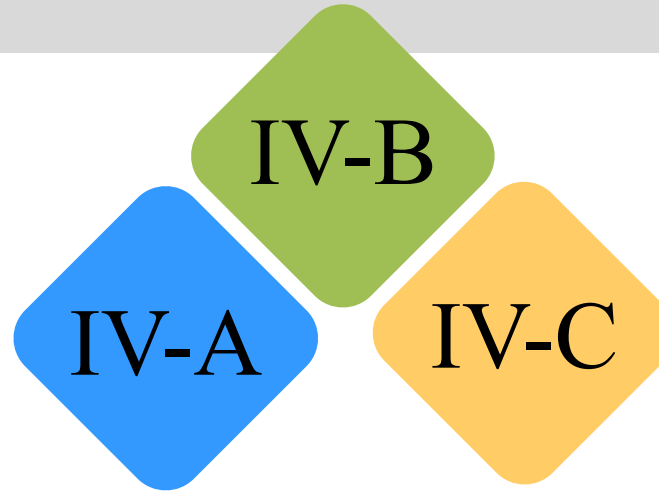
Wood Stud Wall

No

1 Hr

*IBC 2021 requires at least 1 Hr FRR for HT walls supporting 2 levels

Exterior Wall Construction Recap



IBC 2021

IBC 2018

Fire Rating (bearing wall)

Mass Timber

Exterior NC Protection

Interior NC Protection

Light Frame FRTW

3 Hr	2 Hr	2 Hr	2 Hr	2Hr
Mass Timber/CLT			4" min thick <u>CLT</u> *	6" <u>Wall</u> *
40 Min NC & No Exterior Combustible Coverings			FRT Sheathing, Gyp or other NC	
Per Interior Requirements			Not Required	
No			Yes*	6" Wall*

*Changes in IBC 2015, 2018, and 2021 editions

Tall Wood Fire Resistance Ratings (FRR)

FRR Requirements for Tall Mass Timber Structures (hours)

Building Element	IV-A	IV-B	IV-C
Primary Frame	3	2	2
Exterior Bearing Walls	3	2	2
Interior Bearing Walls	3	2	2
Roof Construction	1.5	1	1
Primary Frame at Roof	2	1	1
Floor Construction	2	2	2

Source: 2021 IBC Table 601

Noncombustible Protection (NC)

Where timber is required to be protected, NC must contribute at least 2/3 FRR

Required Noncombustible Contribution to FRR

FRR of Building Element (hours)	Minimum from Noncombustible Protection (minutes)
1	40
2	80
3 or more	120

Source: 2021 IBC Section 722.7

Noncombustible Protection (NC)

Prescriptive Noncombustible Contributions to FRR

Type of Protection	Contribution per Layer (minutes)
1/2" Type X gypsum board	25
5/8" Type X gypsum board	40

Source: 2021 IBC Section 722.7.1

Required Noncombustible Contribution to FRR

FRR of Building Element (hours)	Minimum from Noncombustible Protection (minutes)
1	40
2	80
3 or more	120

1 layer 5/8 Type X

2 layers 5/8 Type X

3 layers 5/8 Type X

Source: 2021 IBC Section 722.7

Floor Surface Protection



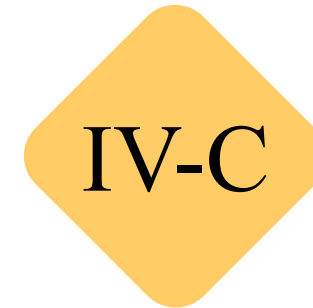
**Min. 1" thick NC protection required
on mass timber floors in IV-A and IV-B.
Not required in IV-C**



Noncombustible Protection



Noncombustible Protection Required



Roof below Mass Timber

Primary Frame @ Roof

Primary Frame

Below Mass Timber Floor

Above Mass Timber Floor

IV-A	IV-B	IV-C	IV-HT
60 min	40 min*	Not Req.	Not Req.
80 min	40 min*	Not Req.	Not Req.
120 min	80 min*	Not Req.	Not Req.
80 min	80 min*	Not Req.	Not Req.
1" Min NC Material	1" Min NC Material	Not Req.	Not Req.

Requirements Per new 602.4. * Some MT permitted to be exposed.

MT Fire Resistance Ratings (FRR)



IBC 722.7

The fire resistance rating of the mass timber elements shall consist of the fire resistance of the unprotected element (MT) added to the protection time of the noncombustible (NC) protection.



= FRR

MT Fire Resistance Ratings (FRR)



However, FRR Doesn't always need to be from a combination of MT + NC. In some cases, just NC can be used, in other cases, just MT can be used:

IBC 602.4

Mass timber elements shall meet the fire resistance rating requirements of this section based on either the fire resistance rating of the noncombustible protection, the mass timber, or a combination of both.

MT



NC



Credit: Urban One

Type IV-A Fire Resistance Ratings (FRR)

IV-A

Primary Frame (3-hr) + Floor Panel Example (2-hr):

Minimum 1" noncombustible material

Mass timber floor panel

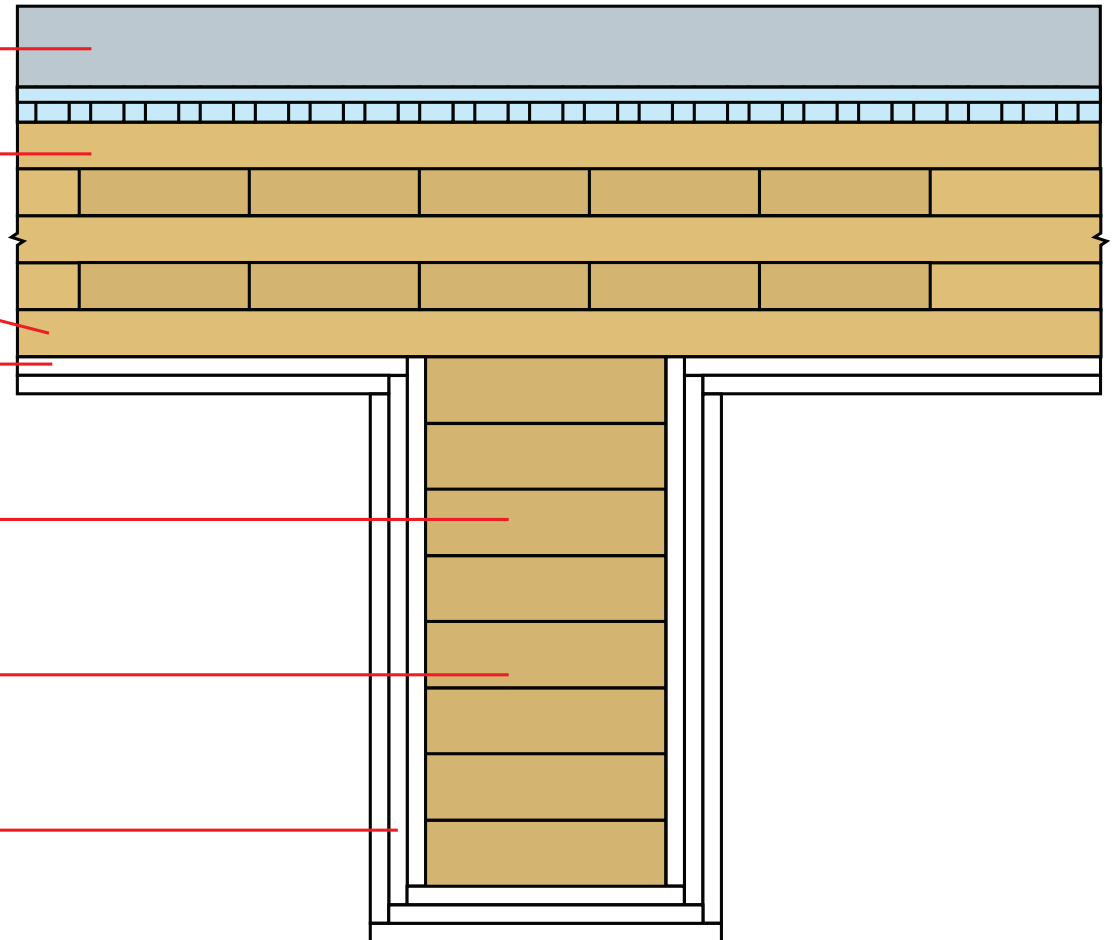
40 minutes of MT FRR

Two layers 5/8" Type X gypsum

Glulam beam (primary structural frame)

60 minutes of MT FRR

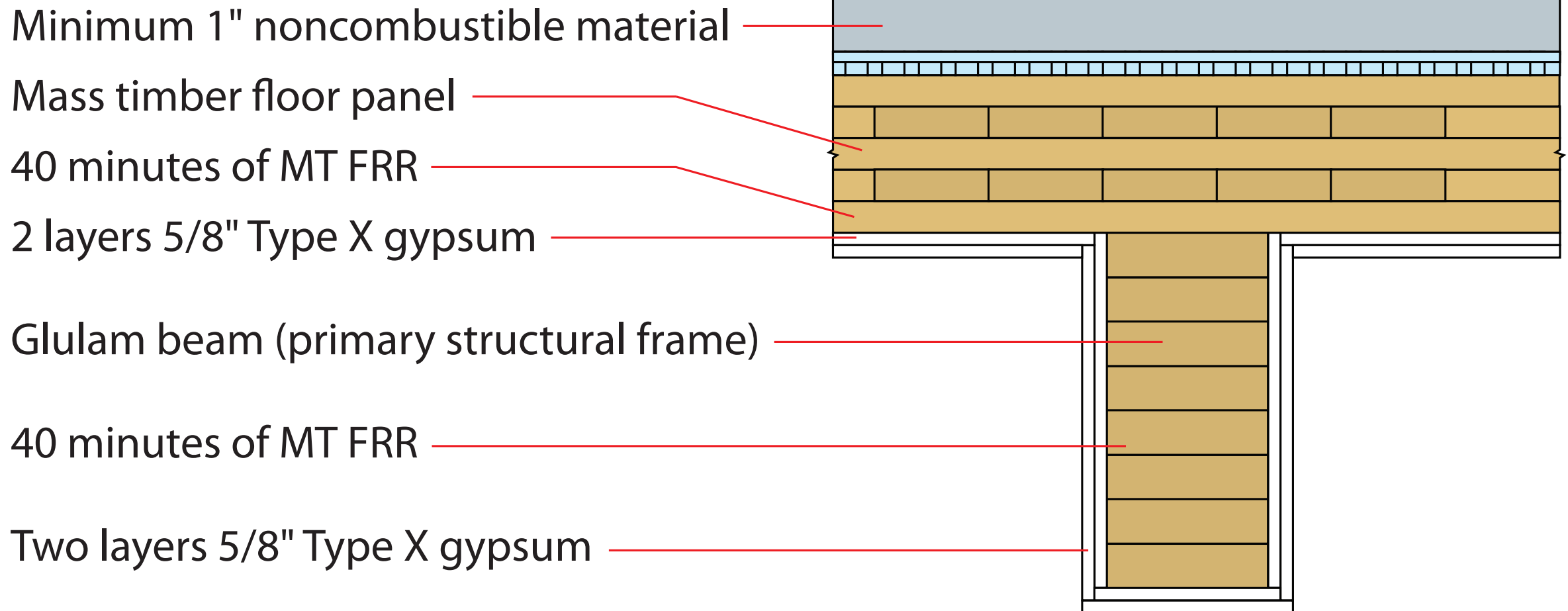
Three layers 5/8" Type X gypsum



Type IV-B Fire Resistance Ratings (FRR)

IV-B

Primary Frame (2-hr) + Floor Panel (2-hr)



Type IV-B Fire Resistance Ratings (FRR)

IV-B

Primary Frame (2-hr) + Floor Panel Example (2-hr)

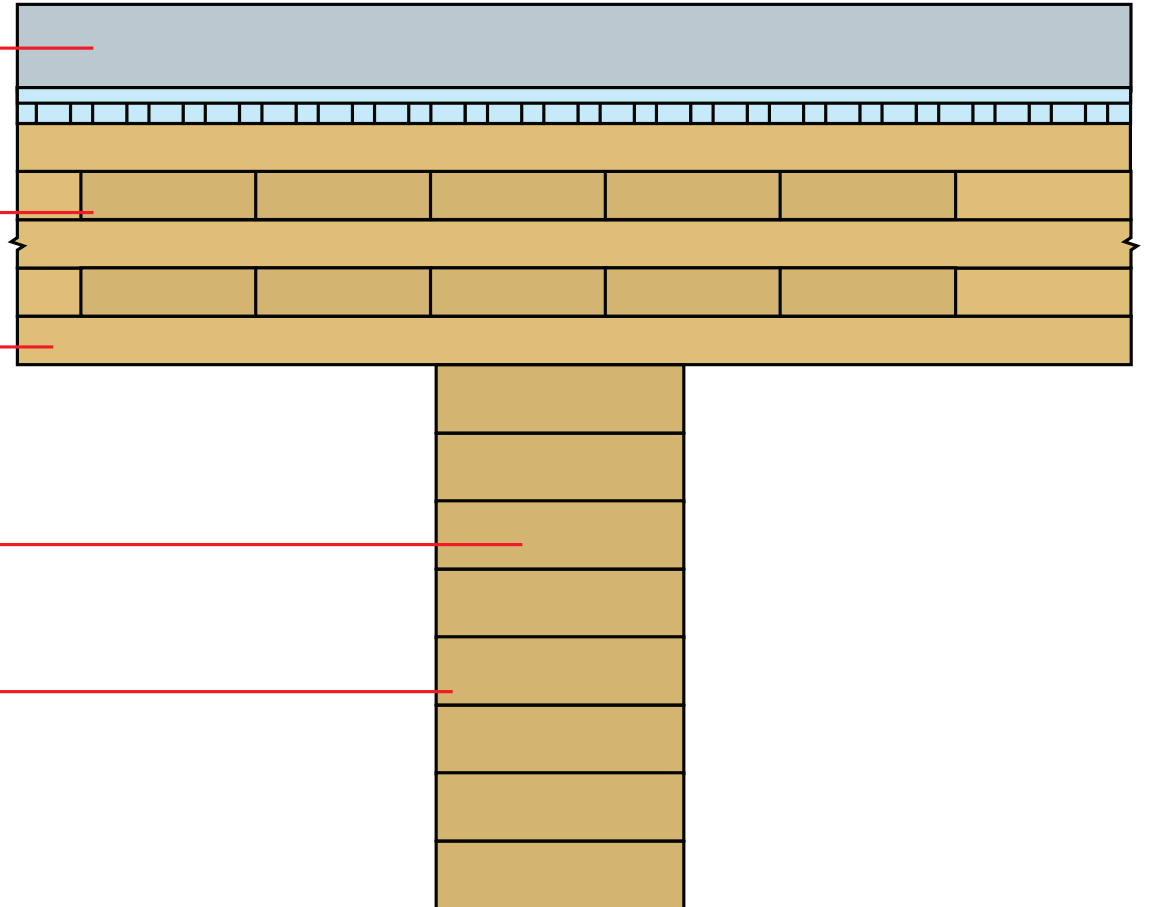
Minimum 1" noncombustible material

Mass timber floor panel

2-hr of MT FRR;
noncombustible material not required

Glulam beam (primary structural frame)

2-hr of MT FRR;
Noncombustible material not required



Type IV-C Fire Resistance Ratings (FRR)

IV-B

Primary Frame (2-hr) + Floor Panel Example (2-hr)

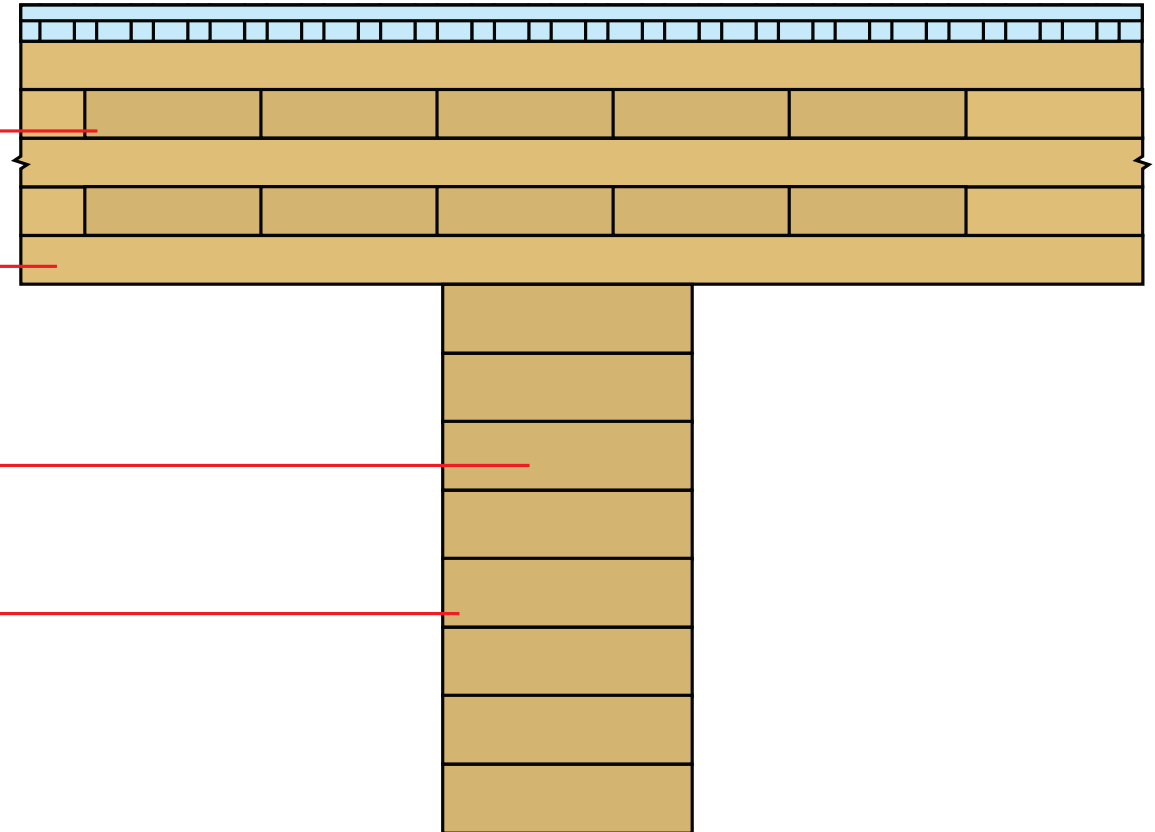
Noncombustible material not required

Mass timber floor panel

2-hr of MT FRR;
noncombustible material not required

Glulam beam (primary structural frame)

2-hr of MT FRR;
Noncombustible material not required

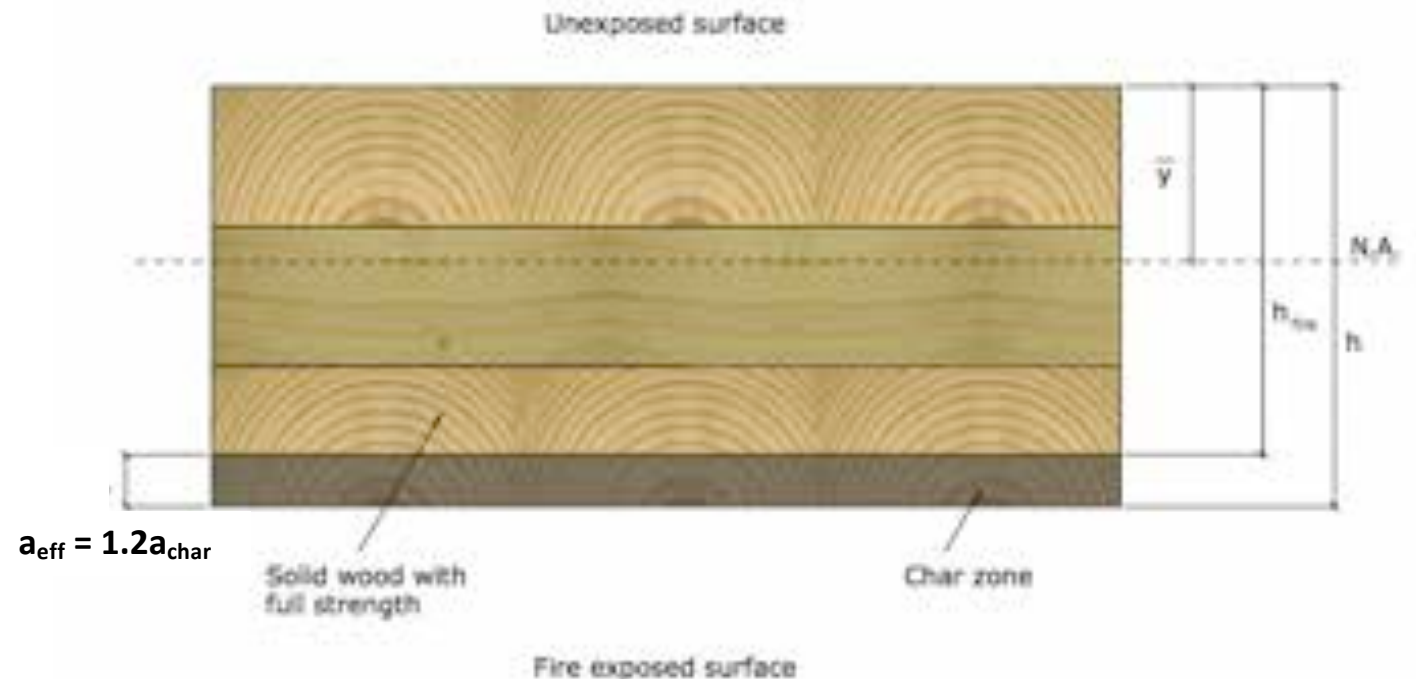


MT Fire Resistance Ratings (FRR)

How do you determine FRR of MT?

2 Options:

1. Calculations in Accordance with IBC 722 → NDS Chapter 16
2. Tests in Accordance with ASTM E119



MT Fire Resistance Ratings (FRR)

MT FRR Calculations Method:

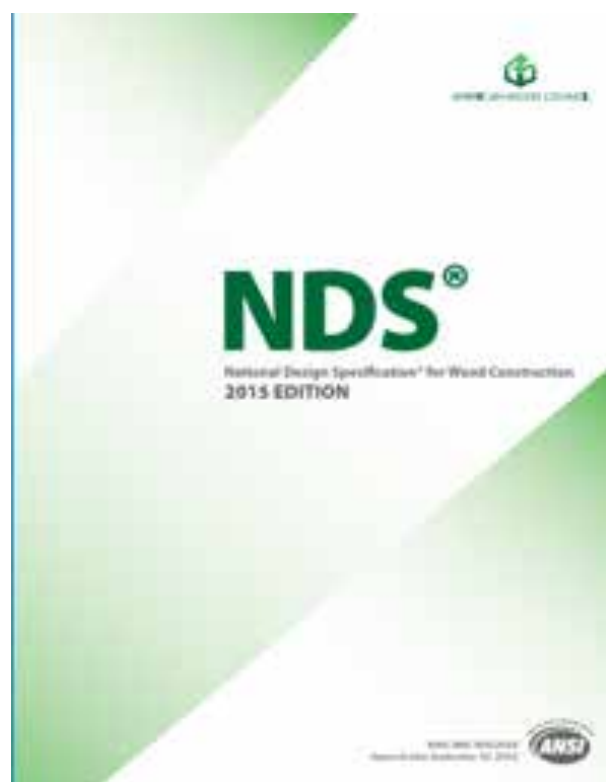
- IBC 703.3 allows several methods of determining FRR. One is calculations per 722.
- 722.1 refers to NDS Chpt 16 for exposed wood FRR

703.3 Methods for determining fire resistance. The application of any of the methods listed in this section shall be based on the fire exposure and acceptance criteria specified in ASTM E119 or UL 263. The required *fire resistance* of a building element, component or assembly shall be permitted to be established by any of the following methods or procedures:

3. Calculations in accordance with Section 722.

722.1 General. The provisions of this section contain procedures by which the *fire resistance* of specific materials or combinations of materials is established by calculations. These procedures apply only to the information contained in this section and shall not be otherwise used. The calculated *fire resistance* of concrete, concrete masonry and clay masonry assemblies shall be permitted in accordance with ACI 216.1/TMS 0216. The calculated *fire resistance* of steel assemblies shall be permitted in accordance with Chapter 5 of ASCE 29. The calculated *fire resistance* of exposed wood members and wood decking shall be permitted in accordance with Chapter 16 of ANSI/AF&PA *National Design Specification for Wood Construction (NDS)*.

MT Fire Resistance Ratings (FRR)



NDS Chapter 16 includes calculation of fire resistance of NLT, CLT, Glulam, Solid Sawn and SCL wood products

Table 16.2.1B Effective Char Depths (for CLT with $\beta_s=1.5\text{in./hr.}$)

Required Fire Endurance (hr.)	Effective Char Depths, a_{char} (in.)								
	lamination thicknesses, h_{lam} (in.)								
	5/8	3/4	7/8	1	1-1/4	1-3/8	1-1/2	1-3/4	2
1-Hour	2.2	2.2	2.1	2.0	2.0	1.9	1.8	1.8	1.8
1½-Hour	3.4	3.2	3.1	3.0	2.9	2.8	2.8	2.8	2.6
2-Hour	4.4	4.3	4.1	4.0	3.9	3.8	3.6	3.6	3.6



Credit: FPInnovations

MT Fire Resistance Ratings (FRR)

Nominal char rate of 1.5"/HR is recognized in NDS. Effective char depth calculated to account for duration, structural reduction in heat-affected zone



Credit: ARUP

Table 16.2.1A Char Depth and Effective Char Depth (for $\beta_n = 1.5$ in./hr.)

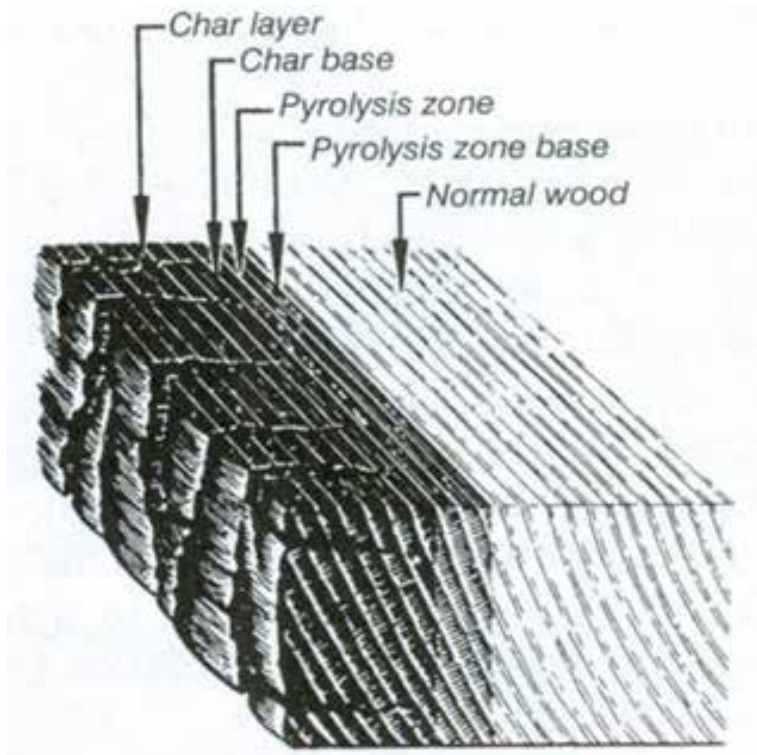
Required Fire Resistance (hr.)	Char Depth, a_{char} (in.)	Effective Char Depth, a_{eff} (in.)
1-Hour	1.5	1.8
1½-Hour	2.1	2.5
2-Hour	2.6	3.2

Table 16.2.1B Effective Char Depths (for CLT with $\beta_n = 1.5$ in./hr.)

Required Fire Endurance (hr.)	Effective Char Depths, a_{char} (in.)								
	lamination thicknesses, h_{lam} (in.)								
	5/8	3/4	7/8	1	1-1/4	1-3/8	1-1/2	1-3/4	2
1-Hour	2.2	2.2	2.1	2.0	2.0	1.9	1.8	1.8	1.8
1½-Hour	3.4	3.2	3.1	3.0	2.9	2.8	2.8	2.8	2.6
2-Hour	4.4	4.3	4.1	4.0	3.9	3.8	3.6	3.6	3.6

MT Fire Resistance Ratings (FRR)

Structural capacity check performed on remaining section, with stress increases



Credit: Forest Products Laboratory

Table 16.2.2 Adjustment Factors for Fire Design¹

			ASD					
			Design Stress to Member Strength Factor	Size Factor ²	Volume Factor ³	Flat Use Factor ³	Beam Stability Factor ³	Column Stability Factor ³
Bending Strength	F_b	x	2.85	C_F	C_V	C_{Fu}	C_L	-
Beam Buckling Strength	F_{bE}	x	2.03	-	-	-	-	-
Tensile Strength	F_t	x	2.85	C_F	-	-	-	-
Compressive Strength	F_c	x	2.58	C_F	-	-	-	C_P
Column Buckling Strength	F_{cE}	x	2.03	-	-	-	-	-

$$a_{\text{char}} = \beta_t t^{0.813}$$

Solid Sawn, Glulam, SCL

$$a_{\text{char}} = n_{\text{lam}} h_{\text{lam}} + \beta_t \left(t - (n_{\text{lam}} t_g) \right)^{0.813}$$

CLT







$$a_{\text{eff}} = 1.2a_{\text{char}}$$

Effective Char Depth

MT Fire Resistance Ratings (FRR)

Tested Assemblies Method:

- Many successful Mass Timber ASTM E119 fire tests have been completed by industry & manufacturers

 <p>Fire Testing Laboratory</p>  <p>Page 1 of 53</p> <p>TEST REPORT for American Wood Council 222 Catotlin Circle SE, Suite 201 Leesburg, VA 20175</p> <p>Standard Methods of Fire Tests of Building Construction and Materials ASTM E 119 – 11a</p> <p>Test Report No: WP-1950 Assignment No: K-1289 Subject Material: Cross-Laminated Timber and Gypsum Board Wall Assembly (Load-Bearing) Test Date: October 4, 2012 Report Date: October 16, 2012</p> <p>Prepared by:  Michael J. Ridge Test Engineer</p> <p>Reviewed by:  Robert J. Marshett Director, Laboratory Facilities and Testing Services</p>	<p>TEST REPORT</p>  <p>REPORT NUMBER: 102891256SAT-001 ORIGINAL ISSUE DATE: February 27, 2017 REVISED DATE: N/A</p> <p>EVALUATION CENTER 16015 Shady Falls Road Elmendorf, TX 78112 Phone: (210) 635-8100 Fax: (210) 635-8101 www.intertek.com</p> <p>RENDERED TO Structurlam Products LP 2176 Government Street Penticton, BC V2A 8B5 Canada</p>	 <p>Project No. 301006155 Final Report 2012/13</p> <p>Preliminary CLT Fire Resistance Testing Report</p> <p>by Lindsay Osborne, M.A.Sc. Christian Dagenais, Eng., M.Sc. Scientists Advanced Building Systems – Serviceability and Fire Group</p>
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Contact WoodWorks for Inventory of Tests

MT Fire Resistance Ratings (FRR)



Fire-Resistive Design of Mass Timber Members

Code Applications, Construction Types and Fire Ratings

Kenneth L. Lutz, P.E., S.E. • Senior Technical Director • WoodWorks
Scott Eisenman, Ph.D., P.E., S.E. • Senior Technical Director • WoodWorks

For many years, exposed heavy timber framing elements have been permitted in U.S. buildings due to their inherent fire-resistance properties. The predictability of wood's char rate has been well-established for decades and has long been recognized in building codes and standards.

Today, one of the existing trends in building design is the growing use of mass timber—i.e., large solid wood panel products such as cross-laminated timber (CLT) and nail-laminated timber (NLT)—for floor, wall and roof construction. Like heavy timber, mass timber products have inherent fire resistance that allows them to be left exposed and still achieve a fire-resistance rating. Because of their strength and dimensional stability, these products also offer a low-carbon alternative to steel, concrete, and masonry for many applications. It is this combination of exposed structure and strength that developers and designers across the country

are leveraging to create innovative designs with a warm yet modern aesthetic, often for projects that go beyond traditional forms of wood design.

This paper has been written to support architects and engineers exploring the use of mass timber for commercial and multi-family construction. It focuses on how to meet fire-resistance requirements in the International Building Code (IBC), including calculation and testing-based methods. Unless otherwise noted, references refer to the 2018 IBC.

Mass Timber & Construction Type

Before demonstrating fire-resistance ratings of exposed mass timber elements, it's important to understand under what circumstances the code currently allows the use of mass timber in commercial and multi-family construction.

A building's assigned construction type is the main indicator of where and when all wood systems can be used. IBC Section 602 defines five main options (Type I through V) with all but Type IV having subcategories A and B. Types III and V permit the use of wood framing throughout much of the structure and both are used extensively for modern mass timber buildings.

Type III (IBC 602.3) – Timber elements can be used in floors, roofs and interior walls. Fire-retardant-treated wood (FRTW) framing is permitted in exterior walls with a fire-resistance rating of 2 hours or less.

Type V (IBC 602.5) – Timber elements can be used throughout the structure, including floors, roofs and both interior and exterior walls.

Type IV (IBC 602.4) – Commonly referred to as "Heavy Timber" construction, this option



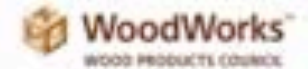
Calentini 1 Portland, Oregon
Kaiser Group 1, Park Architecture
Manning Structural Engineering

- Mass Timber Fire Design Resource
- Code compliance options for demonstrating FRR
- Updated as new tests are completed
- Free download at woodworks.org

MT Fire Resistance Ratings (FRR)

Inventory of Fire Tested MT Assemblies

Table 1: North American Fire Resistance Tests of Mass Timber Floor / Roof Assemblies



CLT Panel	Manufacturer	CLT Grade or Major & Minor Grade	Ceiling Protection	Panel Connection in Test	Floor Topping	Load Rating	Fire Resistance Achieved (Hours)	Source	Testing Lab
3-ply CLT (114mm x 409 in.)	Nordic	SPP 1650-16 1.15 MBR x SPP #3	23mm 1/2" Type X gypsum	Half-Lap	None	Reduced 34% Moment Capacity	1	1 (Test 1)	NRC Fire Laboratory
3-ply CLT (104mm x 413 in.)	Emucation	SPP #1.02 x SPP #1.02	1 layer 5/8" Type X gypsum	Half-Lap	None	Reduced 73% Moment Capacity	1	1 (Test 1)	NRC Fire Laboratory
3-ply CLT (173mm x 479")	Nordic	II	None	Top-side Spline	2 staggered layers of 1/2" acoustical board	Loaded, See Manufacturer	2	2	NRC Fire Laboratory March 2016
3-ply CLT (173mm x 479")	Nordic	II	1 layer 5/8" Type X gypsum under 2- channels and furring strips with 1.5-0" flashed joints	Top-side Spline	2 staggered layers of 1/2" acoustical board	Loaded, See Manufacturer	2	2	NRC Fire Laboratory Nov 2014
3-ply CLT (173mm x 479")	Nordic	II	None	Top-side Spline	3/4 in. proprietary gypsum over Mass on acoustical mat	Reduced 10% Moment Capacity	0.5	3	UL
3-ply CLT (173mm x 479")	Nordic	II	1 layer 5/8" normal gypsum	Top-side Spline	3/4 in. proprietary gypsum over Mass on acoustical mat or proprietary sound board	Reduced 10% Moment Capacity	1	4	UL
3-ply CLT (173mm x 479")	Nordic	II	1 layer 5/8" Type X Gypsum under Resilient Channel under 7/8" furring strips with 1.5" Minus Wood flashed joints	Half-Lap	None	Loaded, See Manufacturer	2	21	Intertek 8/24/2012
3-ply CLT (173mm x 479")	Emucation	II M5 MBR 2100 x SPP #2	None	Top-side Spline	1-1/2" Masonry Cyp Gips 2000 over Mason Reinforcing Mesh	Loaded, See Manufacturer	2.5	6	Intertek, 2/22/2016
3-ply CLT (173mm x 479")	DR Johnson	VI	None	Half-Lap & Top-side Spline	2" gypsum topping	Loaded, See Manufacturer	2	7	SwRI (May 2016)
3-ply CLT (173mm x 479")	Nordic	SPP 1650-16 MBR x SPP #3	None	Half-Lap	None	Reduced 19% Moment Capacity	0.5	1 (Test 3)	NRC Fire Laboratory
3-ply CLT (173mm x 479")	Emucation	SPP #1.02 x SPP #1.02	1 layer 5/8" Type X gypsum	Half-Lap	None	Unreduced 100% Moment Capacity	2	1 (Test 6)	NRC Fire Laboratory
3-ply CLT (243mm x 6.6")	Emucation	SPP #1.02 x SPP #1.02	None	Half-Lap	None	Unreduced 100% Moment Capacity	2.5	1 (Test 7)	NRC Fire Laboratory
3-ply CLT (173mm x 479")	SmartLam	III-V4	None	Half-Lap	nominal 1/2" plywood with 3/4" nails	Loaded, See Manufacturer	2	12 (Test 6)	Western Fire Center 10/26/2016
3-ply CLT (173mm x 479")	SmartLam	VI	None	Half-Lap	nominal 1/2" plywood with 3/4" nails	Loaded, See Manufacturer	2	12 (Test 7)	Western Fire Center 10/28/2016
3-ply CLT (173mm x 479")	DR Johnson	VI	None	Half-Lap	nominal 1/2" plywood with 3/4" nails	Loaded, See Manufacturer	2	12 (Test 8)	Western Fire Center 11/01/2016
3-ply CLT (114mm x 409 in.)	RIB	CV3M1	None	Half-Lap & Top-side Spline	None	Loaded, See Manufacturer	1	18	SwRI

TECHNICAL BRIEF

Demonstrating Fire-Resistance Ratings for Mass Timber Elements in Tall Wood Structures

Richard McLain, PE, SE • Senior Technical Director – Tall Wood, WoodWorks

Changes to the 2021 International Building Code (IBC) have created opportunities for wood buildings that are much larger and taller than prescriptively allowed in past versions of the code. Occupant safety, and the need to ensure fire performance in particular, was a fundamental consideration as the changes were developed and approved. The result is three new construction types—Type IV-A, IV-B and IV-C—which are based on the previous Heavy Timber construction type (renamed Type IV-HT), but with additional fire protection requirements.

One of the main ways to demonstrate that a building will meet the required level of passive fire protection, regardless of structural materials, is through hourly fire-resistance ratings (FRRs) of its elements and assemblies. The IBC defines an FRR as *the period of time a building element, component or assembly maintains the ability to confine a fire, continues to perform a given structural function, or both, as determined by the tests, or the methods based on tests, prescribed in Section 703.*

FRRs for the new construction types are similar to those required for Type I construction, which is primarily steel and concrete.¹ (See Table 1.) They are found in IBC Table 601, which includes FRR requirements for all construction types and building elements; however, other code sections should be checked for overriding provisions (e.g., occupancy separation, shaft enclosures, etc.) that may alter the requirement.

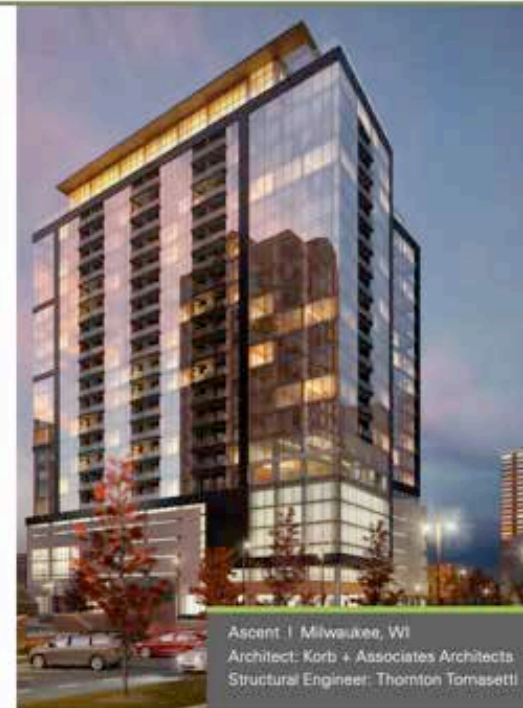


TABLE 1:
FRR Requirements (Hours) for Tall Mass Timber Construction Types and Existing Type I

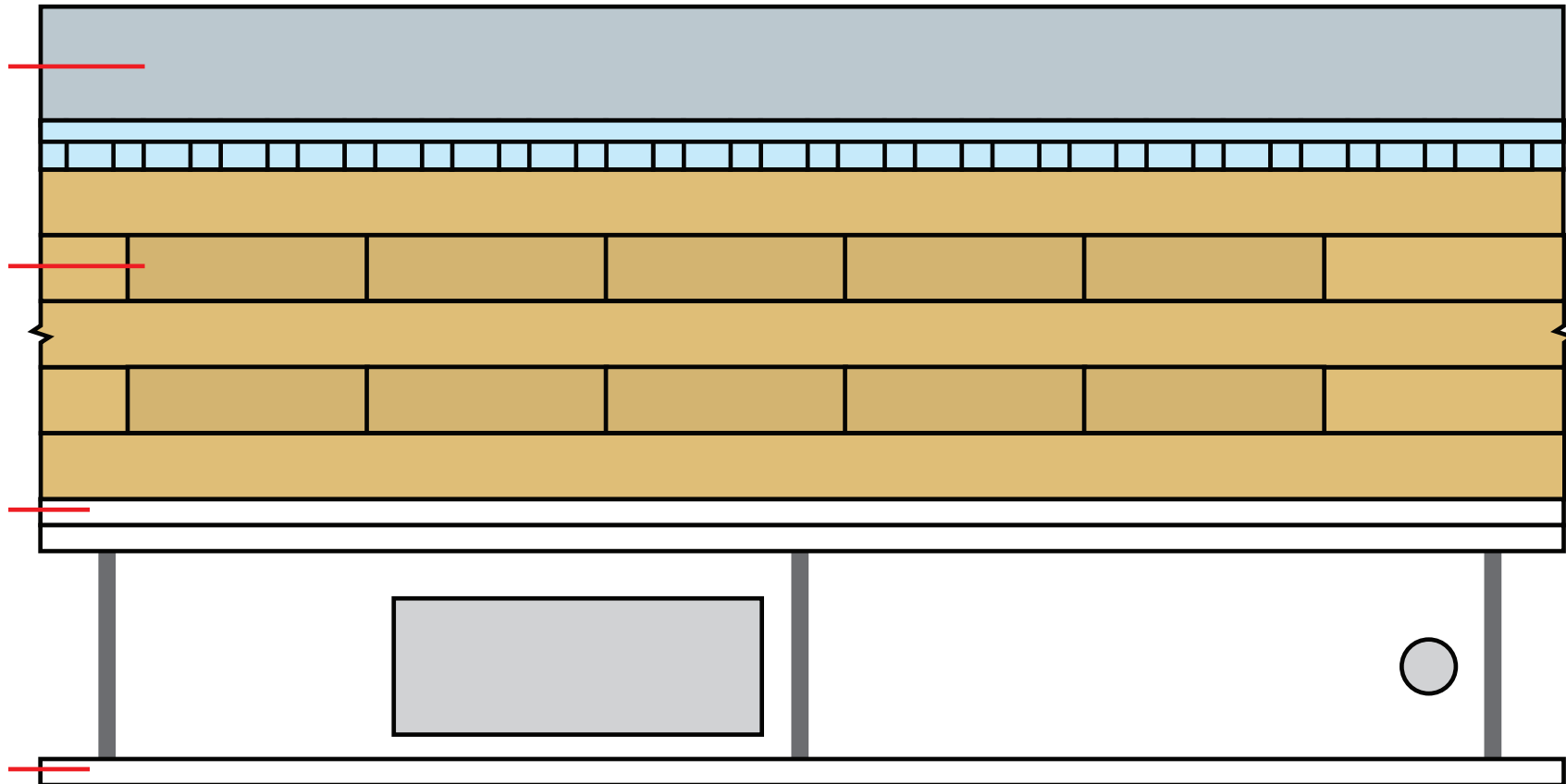
Building Element	I-A Unlimited stories, max. 18 stories	IV-A Max. 18 stories, max. 18 stories	I-B Max. 12 stories, max. 12 stories	IV-B Max. 12 stories, max. 12 stories	IV-C Max. 9 stories, max. 9 stories
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Tall Timber Fire-Resistance Design

Concealed Spaces in Type IV

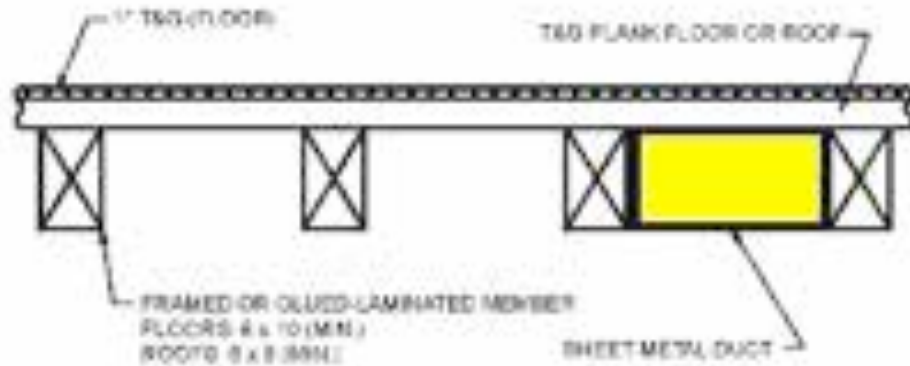
What if I have a dropped ceiling? Can I have a dropped ceiling?

- **Impact on FRR, NC placement, sprinkler requirements**



Concealed Spaces in Type IV

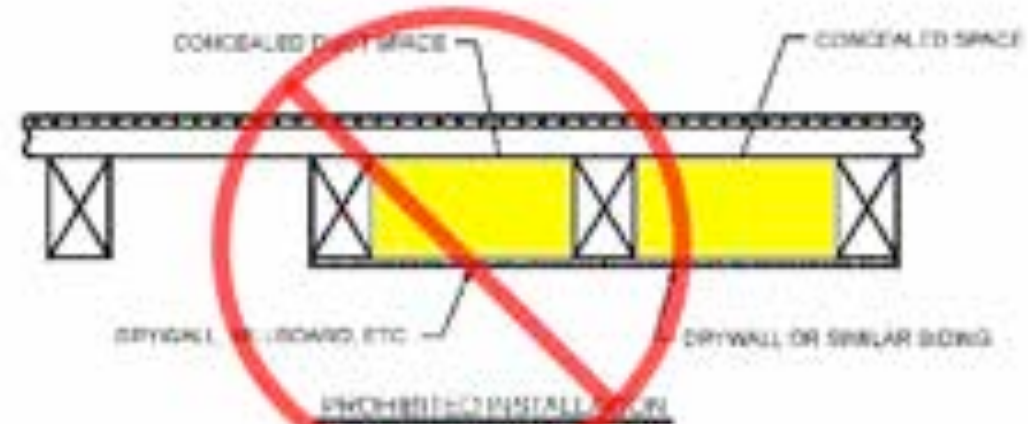
Previous Type IV (now IV-HT) provisions prohibited concealed spaces



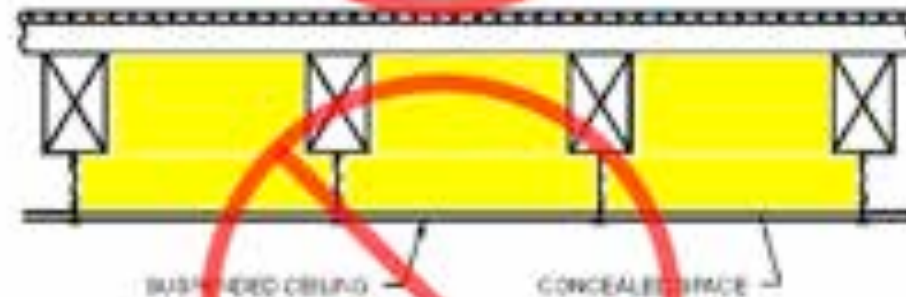
PERMITTED INSTALLATION



PROHIBITED INSTALLATION



PROHIBITED INSTALLATION



PROHIBITED INSTALLATION

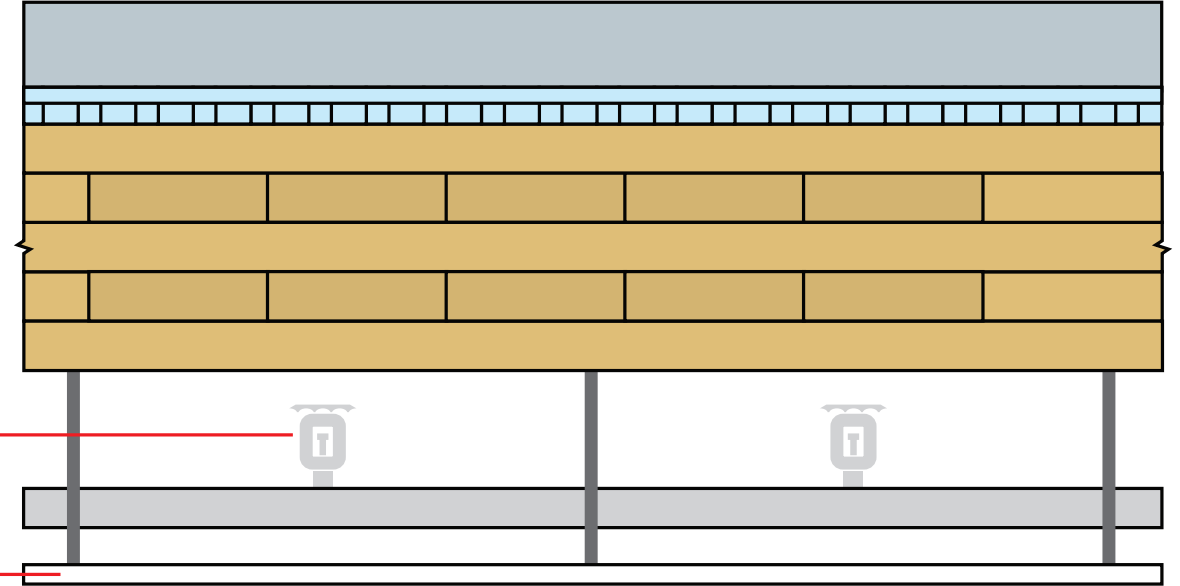
Concealed Spaces in Type IV-HT – 2021 IBC

CONCEALED SPACES: TYPE IV-HT

Option 1:

Sprinklers in concealed spaces

Dropped ceiling



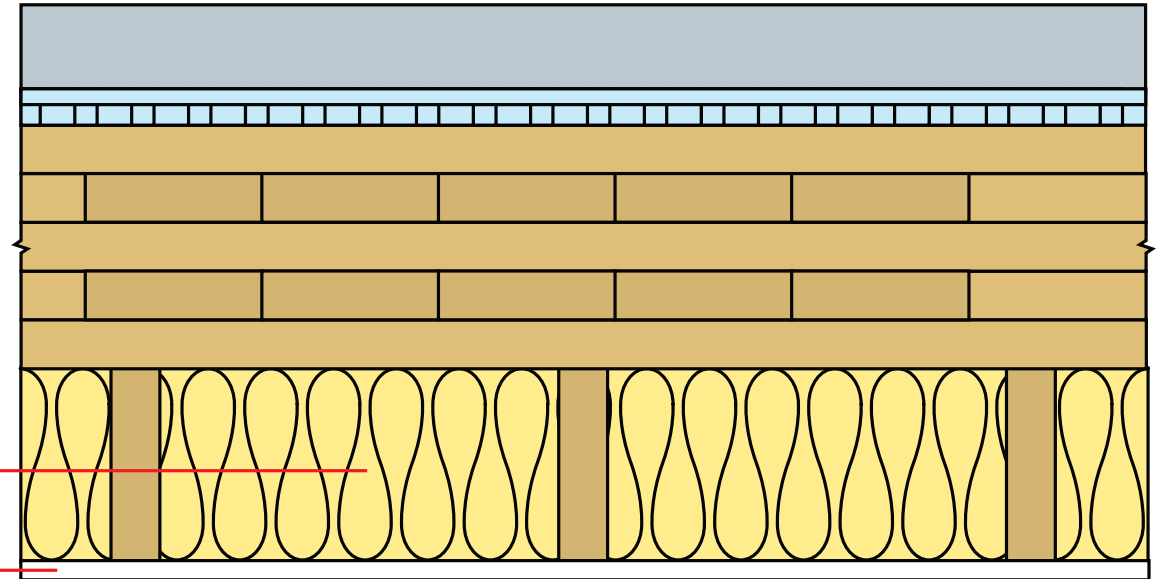
Concealed Spaces in Type IV-HT – 2021 IBC

CONCEALED SPACES: TYPE IV-HT

Option 2:

Noncombustible insulation

Dropped ceiling



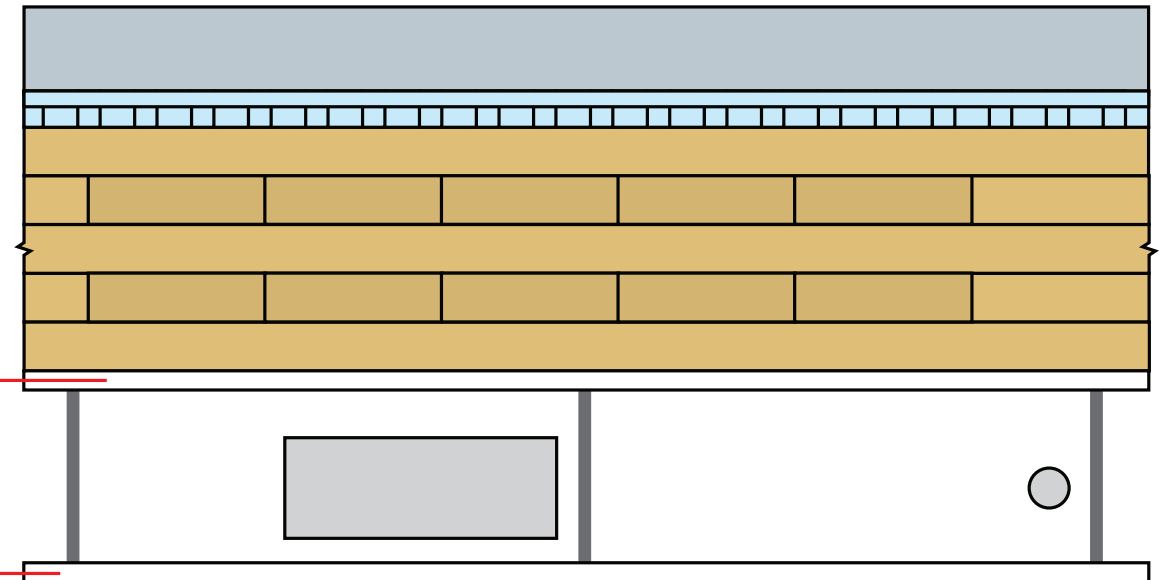
Concealed Spaces in Type IV-HT – 2021 IBC

CONCEALED SPACES: TYPE IV-HT

Option 3:

5/8" Type X gypsum on all mass timber surfaces within concealed space

Dropped ceiling



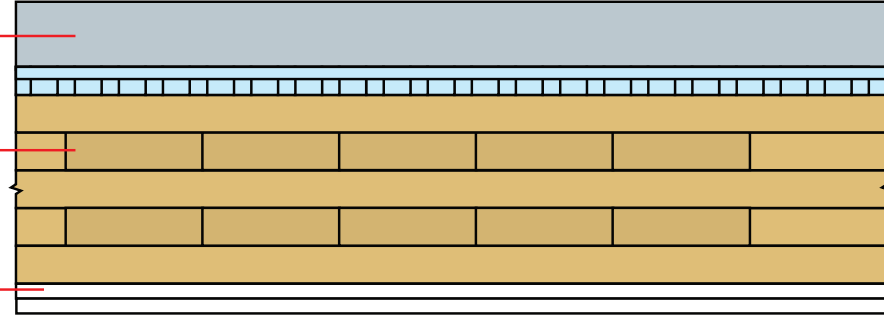
Concealed Spaces in Type IV-A, IV-B

Without Dropped Ceiling

Minimum 1" noncombustible material

Mass timber floor panel

Two layers 5/8" Type X gypsum*



**Applicable to most locations; limited exposed mass timber permitted in IV-B*

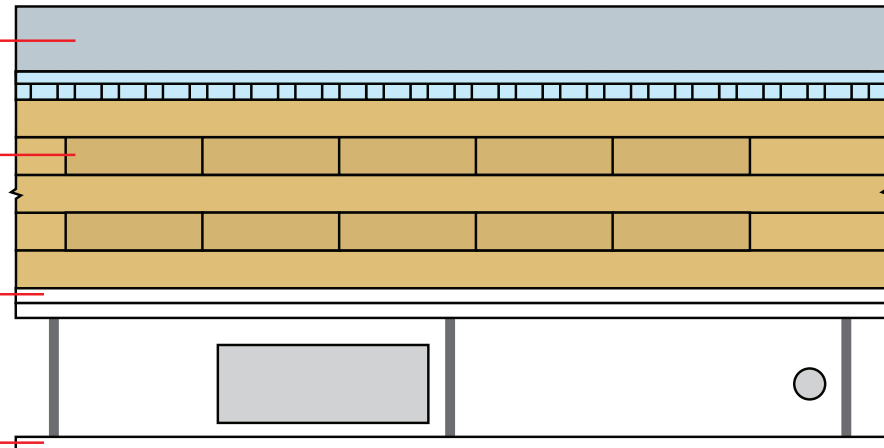
With Dropped Ceiling

Minimum 1" noncombustible material

Mass timber floor panel

Two layers 5/8" Type X gypsum

Dropped ceiling



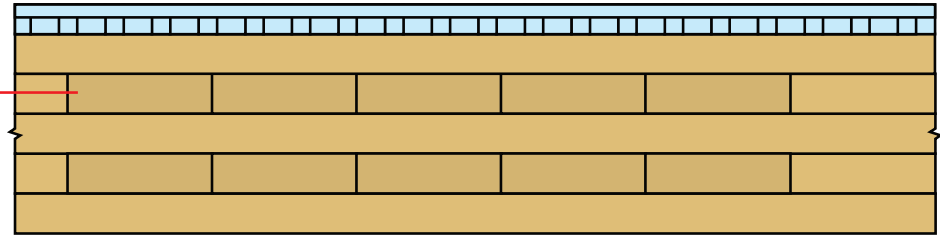
Concealed Spaces in Type IV-C

Without Dropped Ceiling

Noncombustible material not required

Mass timber floor panel

Noncombustible material not required



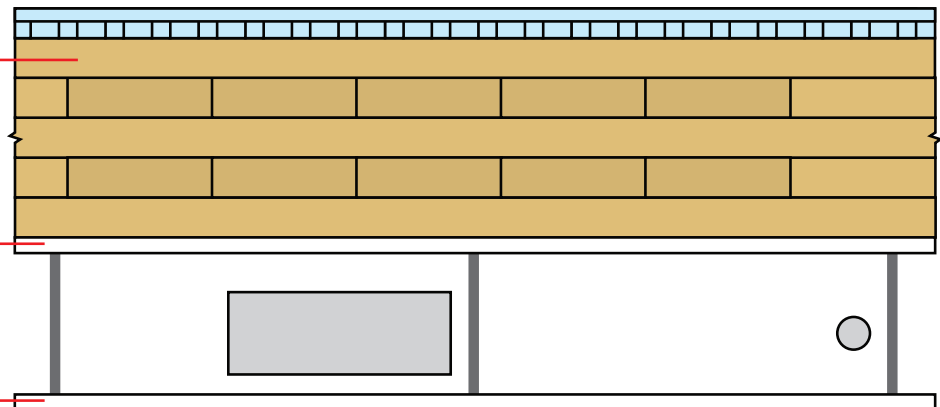
With Dropped Ceiling

Noncombustible material not required

Mass timber floor panel

One layer 5/8" Type X gypsum covering all mass timber surfaces within concealed space

Dropped ceiling



Concealed Spaces in Mass Timber and Heavy Timber Structures

Richard M. Olson, PE, SE • Senior Technical Director • Tall Wood@WoodWorks

Concealed spaces, such as those created by a dropped ceiling in a floor/ceiling assembly or by a stud wall assembly, have unique requirements in the International Building Code (IBC) to address the potential of fire spread in non-visible areas of a building. Section 718 of the 2018 IBC includes prescriptive requirements for protection and/or compartmentalization of concealed spaces through the use of draft stopping, fire blocking, sprinklers, and other means. For information on these requirements, see the WoodWorks Q&A, *Are sprinklers required in concealed spaces such as floor and roof cavities in multi-family wood-frame buildings?*

For mass timber building elements, the choice of construction type can have a significant impact on concealed space requirements. Because mass timber products such as cross-laminated timber (CLT) are prescriptively recognized for Type IV construction, there is a common misperception that exposed mass timber building elements cannot be used or exposed in

other construction types. This is not the case. In addition to Type IV buildings, structural mass timber elements—including CLT, glued laminated timber (glulam), nail laminated timber (NLT), structural composite lumber (SCL), and tongue-and-groove (T&G) decking—can be utilized and exposed in the following construction types, whether or not a fire-resistance rating is required:

- **Type III** – Floors, roofs and interior walls may be any material permitted by code, including mass timber; exterior walls are required to be noncombustible or fire-retarded treated wood.
- **Type V** – Floors, roofs, interior walls, and exterior walls (i.e., the entire structure) may be constructed of mass timber.
- **Types I and II** – Mass timber may be used in select circumstances such as roof construction—including the primary frame—in the 2021 IBC—in Types I-A, II-A or II-B, exterior columns and arches when 20 feet or more of horizontal separation is provided, and balconies, canopies, and similar projections.

WIND, Division 1 (Denver, Colo.)
Master Key Real Estate Services
with Architecture



Concealed Space Protection in Mass Timber



LATERAL SYSTEMS IN TALL WOOD

This aerial photograph captures the upper floors of a tall wood building under construction. The structure features a dense grid of vertical and horizontal wooden members. A complex lateral bracing system is visible, consisting of numerous yellow vertical posts and blue horizontal cross-braces that provide stability. The construction is set against a backdrop of other urban buildings and greenery.

Market Square
Cleveland, OH

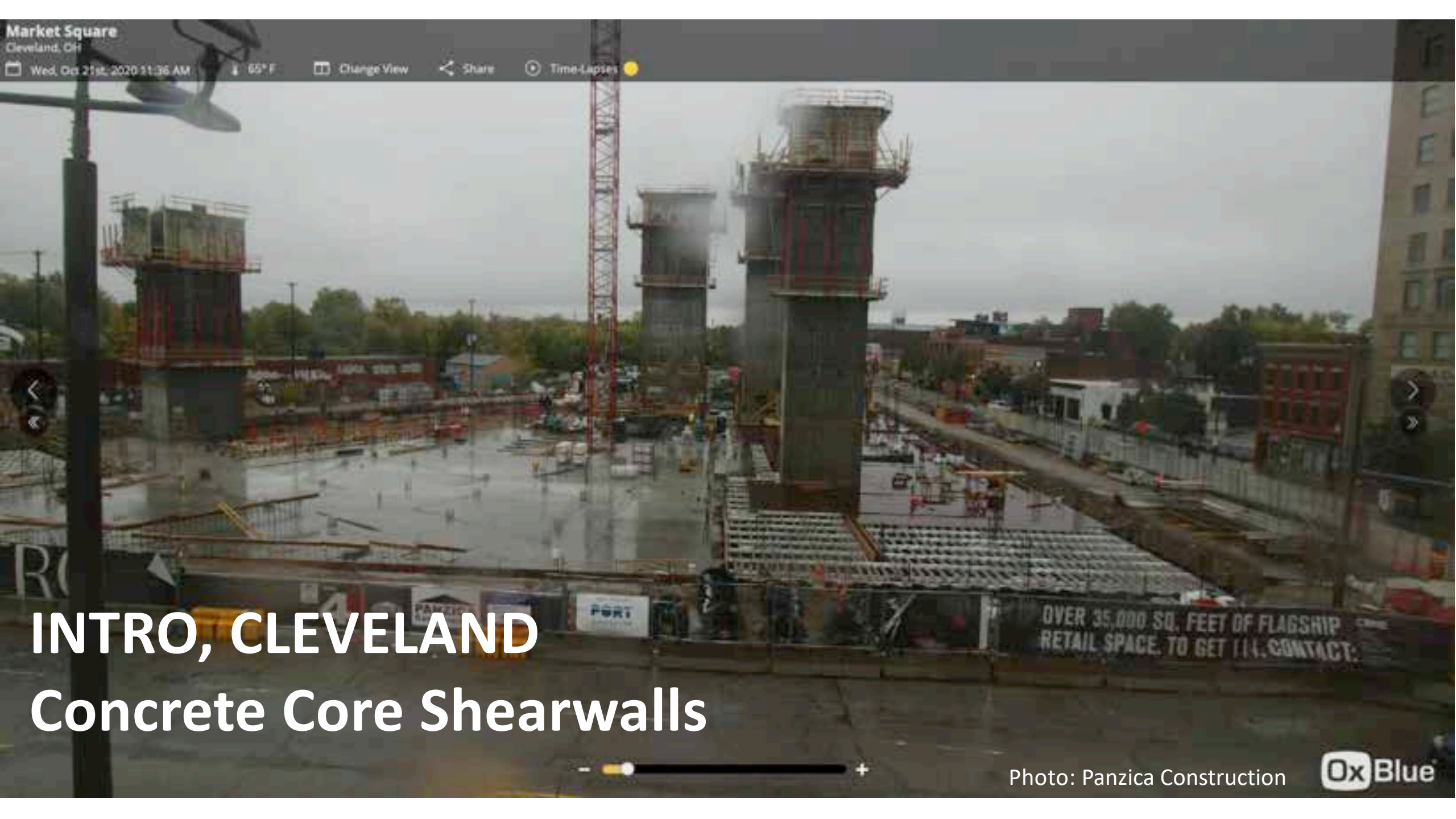
Wed, Oct 21st, 2020 11:36 AM

65° F

Change View

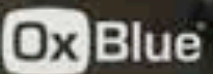
Share

Time-Lapses

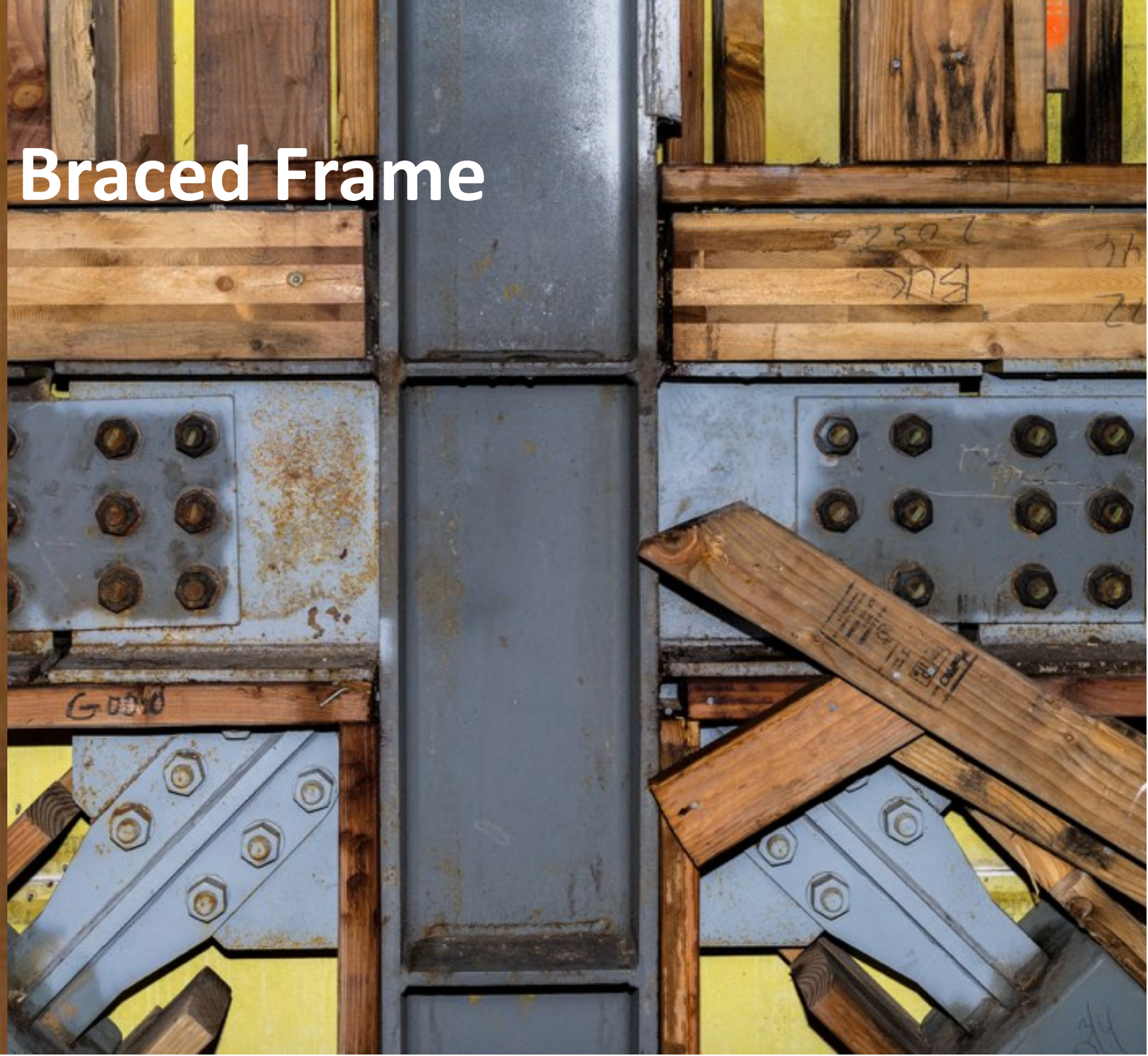


INTRO, CLEVELAND Concrete Core Shearwalls

Photo: Panzica Construction



CARBON12, PORTLAND Buckling-Restrained Braced Frame

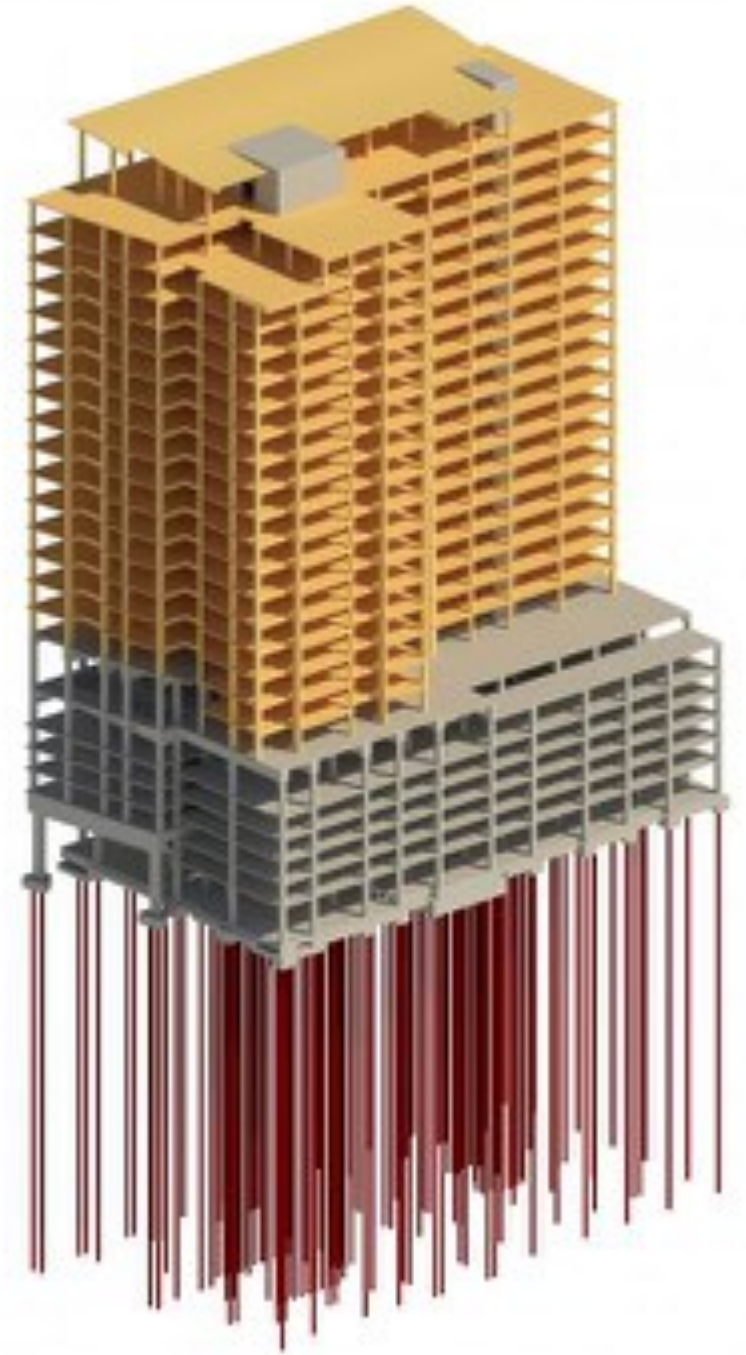


ASCENT, MILWAUKEE

Concrete Core Shearwalls



Photos: Korb + Associates, Thornton Tomasetti



BROCK COMMONS, VANCOUVER

Concrete Core Shearwalls



Photos: Acton Ostry Architects

FUTURE POTENTIAL LATERAL SYSTEM FOR TALL WOOD



Photo: WoodWorks

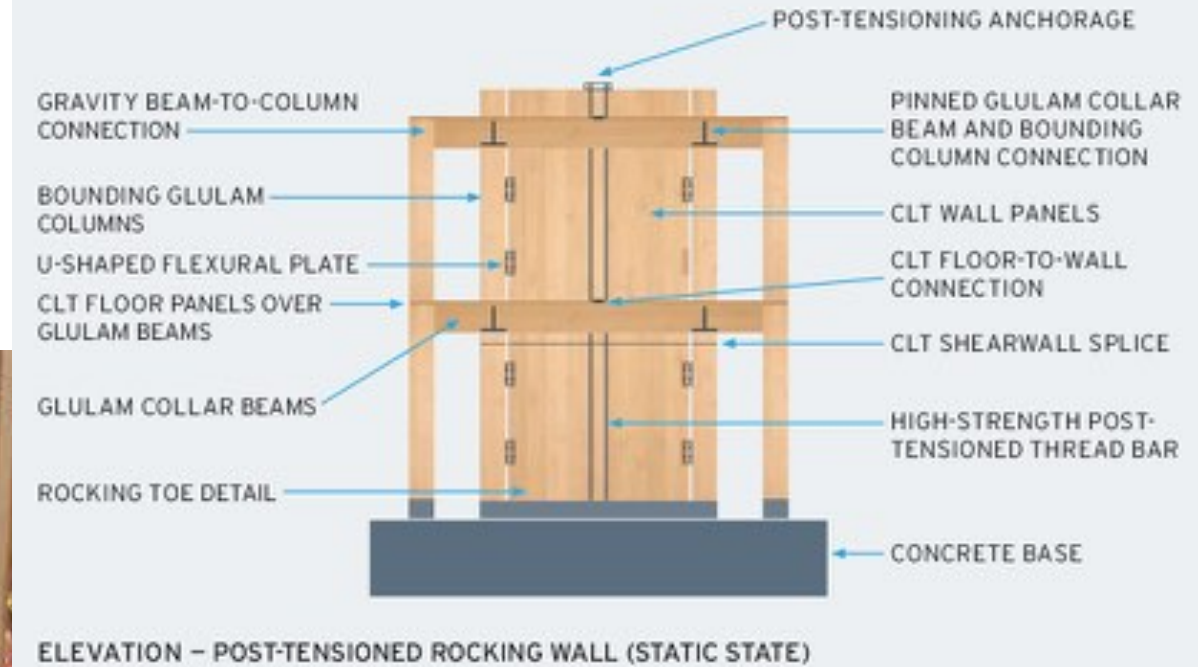


Image: KPFF

Mass Timber Rocking Shearwalls

A construction worker wearing a black hard hat, a high-visibility green long-sleeved shirt, and an orange safety vest is working on a tall, light-colored wood structure. The worker is positioned on a red ladder or scaffolding, reaching up to adjust or secure a vertical wooden beam. The structure is composed of horizontal wooden planks and vertical beams, with metal bracing and scaffolding visible in the background. The sky is clear and blue.

CONNECTIONS IN TALL WOOD

Photo: Structurlam

Connection Fire Protection

In Construction Types IV-A, IV-B & IV-C, building elements are required to be FRR as specified in IBC Tables 601 and 602. Connections between these building elements must be able to maintain FRR no less than that required of the connected members.

16.3 Wood Connections

Wood connections, including connectors, fasteners, and portions of wood members included in the connection design, shall be protected from fire exposure for the required fire resistance time. Protection shall be provided by wood, fire-rated gypsum board, other approved materials, or a combination thereof.

Source: NDS

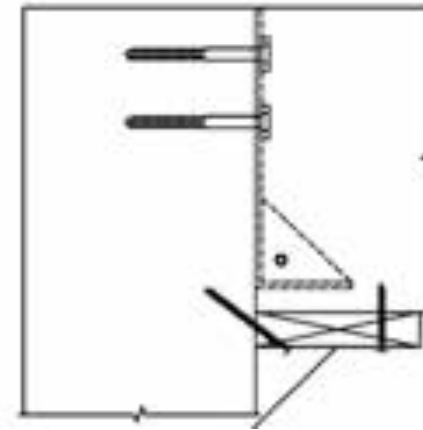


Photo: MyTiCon

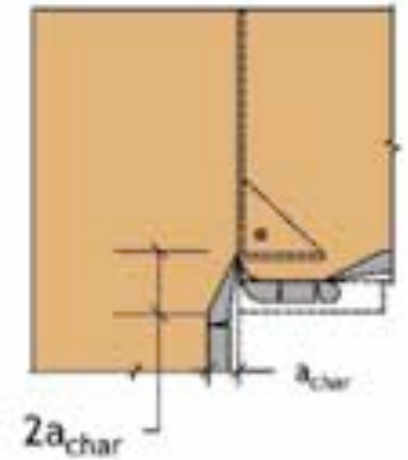
Fire Resistance of Connections

2304.10.1 Connection fire resistance rating. Fire resistance ratings in Type IV-A, IV-B, or IV-C construction shall be determined by one of the following:

1. Testing in accordance with Section 703.2 where the connection is part of the fire resistance test.
2. Engineering analysis that demonstrates that the temperature rise at any portion of the connection is limited to an average temperature rise of 250° F (139° C), and a maximum temperature rise of 325° F (181° C), for a time corresponding to the required fire resistance rating of the structural element being connected. For the purposes of this analysis, the connection includes connectors, fasteners, and portions of wood members included in the structural design of the connection.



Source: AWC's TR 10



Connection Fire Protection

Many ways to demonstrate connection fire protection: calculations, prescriptive NC, test results, others as approved by AHJ



Photo: John Stamets



Photo: Josh Partee



Photo: Christian Columbres

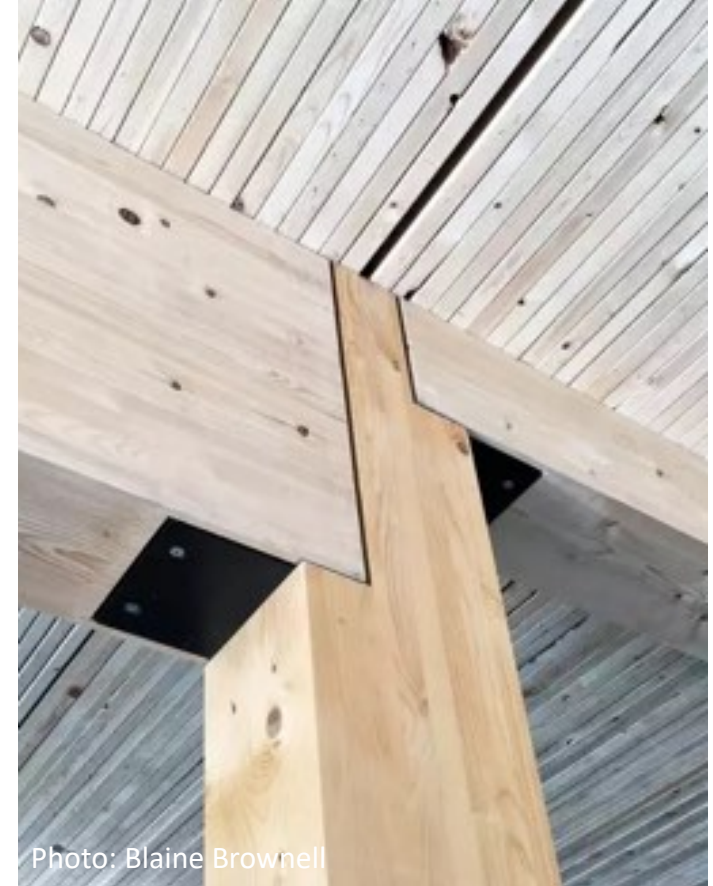


Photo: Blaine Brownell

Connection Fire Protection

**2017 Glulam Beam to Column Connection
Fire Tests under standard ASTM E119
time-temperature exposure**



Connection Fire Protection

Fire Test Results

Test	Beam	Connector	Applied Load	FRR
1	8.75" x 18" (222mm x 457mm)	1 x Ricon S VS 290x80	3,905lbs (17.4kN)	1hr
2	10.75" x 24" (273mm x 610mm)	Staggered double Ricon S VS 200x80	16,620lbs (73.9kN)	1.5hrs
3	10.75" x 24" (273mm x 610mm)	1 x Megant 430	16,620lbs (73.9kN)	1.5hrs

Connection Fire Protection

Softwood Lumber Board Glulam Connection Fire Test Summary Report

Issue | June 5, 2017

Full Report Available at:

<https://www.thinkwood.com/wp-content/uploads/2018/01/reThink-Wood-Arup-SLB-Connection-Fire-Testing-Summary-web.pdf>

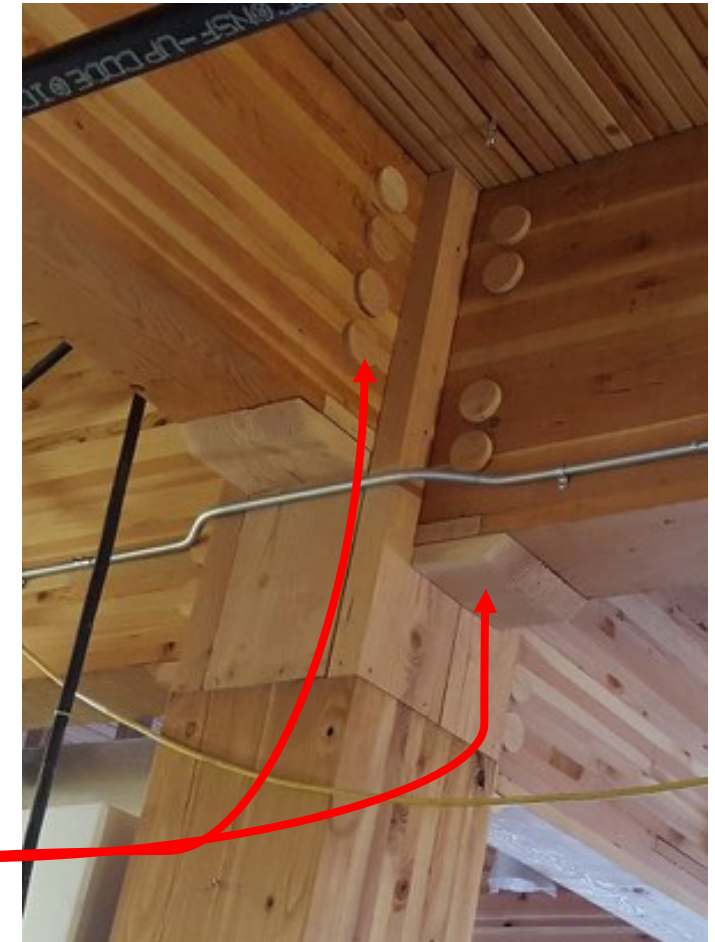


Tall Mass Timber Inspections

Wood Connection Coverings for Fire-Resistance

110.3.5 Type IV-A, IV-B, and IV-C connection protection inspection. In buildings of Type IV-A, IV-B, and IV-C Construction, where connection fire resistance ratings are provided by wood cover calculated to meet the requirements of Section 2304.10.1, inspection of the wood cover shall be made after the cover is installed, but before any other coverings or finishes are installed.

Inspection of Wood Coverings



Tall Mass Timber Special Inspections

TABLE 1705.5.3
REQUIRED SPECIAL INSPECTIONS OF MASS TIMBER CONSTRUCTION

<u>Type</u>	<u>Continuous Special Inspection</u>	<u>Periodic Special Inspection</u>
<u>1. Inspection of anchorage and connections of mass timber construction to timber deep foundation systems.</u>		X
<u>2. Inspect erection of mass timber construction</u>		X
<u>3. Inspection of connections where installation methods are required to meet design loads</u>		
<u>3.1. Threaded fasteners</u>		
<u>3.1.1. Verify use of proper installation equipment.</u>		X
<u>3.1.2. Verify use of pre-drilled holes where required.</u>		X
<u>3.1.3. Inspect screws, including diameter, length, head type, spacing, installation angle, and depth.</u>		X
<u>3.2. Adhesive anchors installed in horizontal or upwardly inclined orientation to resist sustained tension loads</u>	X	
<u>3.3. Adhesive anchors not defined in 3.2.</u>		X
<u>3.4. Bolted connections</u>		X
<u>3.5. Concealed connections</u>		X



PENETRATIONS IN TALL WOOD

Photo: Alex Schreyer

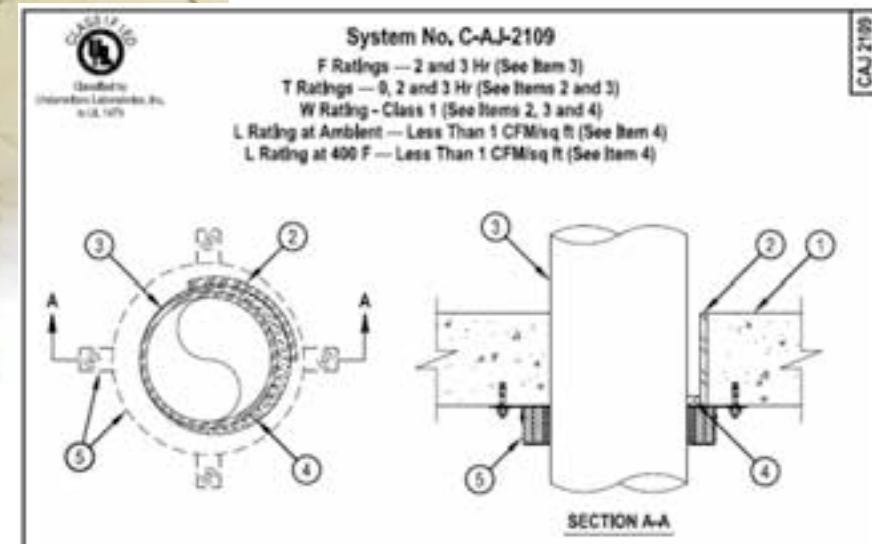
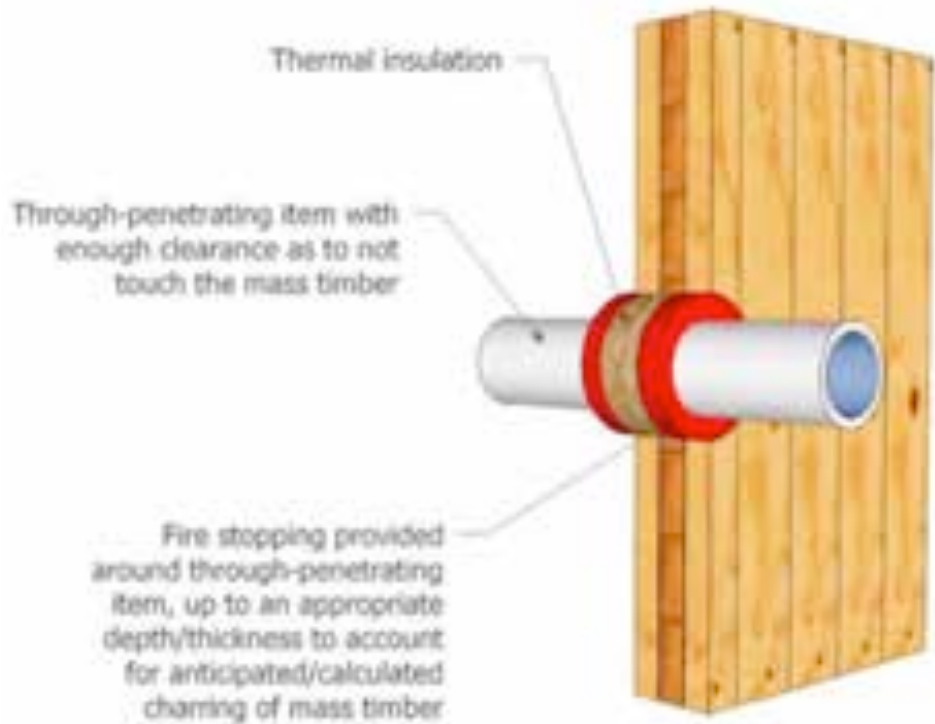
Penetration Fire Protection

Although not a new code requirement or specific to tall wood, more testing & information is becoming available on firestopping of penetrations through MT assemblies



Penetration Fire Protection

Most firestopping systems include combination of fire safing (eg. noncombustible materials such as mineral wool insulation) plus fire caulk



Penetration Fire Protection

Firestop systems tests on Mass Timber
Contact WoodWorks for information

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CHEMISTRY AND CHEMICAL ENGINEERING DIVISION

FIRE TECHNOLOGY DEPARTMENT
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FAX (210) 553-3377



FIRE RESISTANCE PERFORMANCE EVALUATION
OF A PENETRATION FIRESTOP SYSTEM TESTED
IN ACCORDANCE WITH ASTM E814-13A,
STANDARD TEST METHOD FOR FIRE TESTS OF
PENETRATION FIRESTOP SYSTEMS

FINAL REPORT
Consisting of 18 Pages

SwRI® Project No. 01.21428.01.001a
Test Date: September 30, 2015
Report Date: October 22, 2015

Prepared for:

American Wood Council
222 Catocin Circle SE
Leesburg, VA 20175

FIRE PERFORMANCE OF FIRESTOPS, PENETRATIONS, AND FIRE DOORS IN MASS TIMBER ASSEMBLIES

Lindsay Ranger¹, Christian Dagenais¹, Conroy Lum¹, Tony Thomas¹

ABSTRACT: Integrity and continuity must be maintained for fire separations required to provide fire resistance. Firestop systems are used to prevent passage of hot gases or increased temperature on the unexposed side. Vulnerable locations, where penetrations are introduced into mass timber systems, are susceptible to fire spread. Service and closure penetrations through mass timber fire separation have been investigated. Many of the fire stop systems were able to achieve 1-1/2 hr fire resistance in accordance with CAN/ULC-S115, which would be required for 2-hr fire resistance rated assemblies, such as tall wood buildings. Construction details are outlined which ensure adequate fire performance of these penetrations.

KEYWORDS: Firestop, through-penetrations, fire rated door, mass timber, cross-laminated timber, buildings, fire resistance

1 INTRODUCTION

Many tall wood buildings using mass timber are planned or are currently being designed for construction around the world. A few have been built in Canada, including an 18 storey cross-laminated timber (CLT) and glulam building in British Columbia. The prescriptive requirements in the National Building Code of Canada (NBCC) [1] do not (yet) permit the construction of wood buildings taller than six stories, however an alternative

construction, as well as in several alternative building designs.

Although the general fire performance of mass timber is well documented, there are still several areas that warrant further investigation to ensure safety levels are met and a number of design details are available for designers to use. Generating generic assemblies will reduce the need for testing completed on an individual construction



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FIRESTOPPING TEST WITNESS REPORT

for

NORDIC STRUCTURES

Penetration Fire Protection

Inventory of Fire Tested Penetrations in MT Assemblies



Table 3: North American Fire Tests of Penetrations and Fire Stops in CLT Assemblies

CLT Panel	Exposed Side Protection	Penetrating Item	Penetration Considered as Offset in Study	Firestopping System Description	F Rating	T Rating	Noted Test Protocol	Source	Testing Lab
3-ply (78mm x 87")	None	1.2" diameter data cable bunch	Continued	3.3 in diameter hole. Mineral wool was installed in the 1 in. annular space around the data cable to a total depth of approximately 2 - 3.64 in. The remaining 1 in. annular space from the top of the mineral wool to the top of the floor assembly was filled with HBI FS-One Max caulking.	1 hour	0.3 hour	CANULC E113	28	Intertek March 30, 2018
3-ply (78mm x 87")	None	2" copper pipe	Continued	4.375 in diameter hole. Pipe wrap was installed around the copper pipe to a total depth of approximately 2 - 3.64 in. The remaining 1 in. annular space starting at the top of the mineral wool to the top of the floor assembly was filled with HBI FS-One Max caulking.	1 hour	NA	CANULC E113	28	Intertek March 30, 2018
3-ply (78mm x 87")	None	2.3" sch40 40 pipe	Continued	4.92 in diameter hole. Pipe wrap was installed around the schedule 40 pipe to a total depth of approximately 2 - 3.64 in. The remaining 1 in. annular space starting at the top of the pipe wrap to the top of the floor assembly was filled with HBI FS-One Max caulking.	1 hour	NA	CANULC E113	28	Intertek March 30, 2018
3-ply (78mm x 87")	None	6" cast iron pipe	Continued	6.31 in diameter hole. Mineral wool was installed in the 1 in. annular space around the cast iron pipe to a total depth of approximately 2 - 3.64 in. The remaining 1 in. annular space starting at the top of the pipe wrap to the top of the floor assembly was filled with HBI FS-One Max caulking.	1 hour	NA	CANULC E113	28	Intertek March 30, 2018
3-ply (78mm x 87")	None	HBI-6 in drop in device System No.: F-B-2049	Continued	8.01" diameter hole. Mineral wool was installed in the 1 - 1.9 in. annular space around the drop-in device to a total depth of approximately 1 - 7.64 in and the remaining 1 in. annular space from the top of the mineral wool to the top edge of the 8 - 1.94 in. hole in the CLT was filled with HBI FS-One Max caulking.	1 hour	0.71 hour	CANULC E113	28	Intertek March 30, 2018
5-ply CL2 (131 mm x 116")	None	1.2" diameter data cable bunch	Continued	3.3" diameter hole. Mineral wool was installed in the 1 in. annular space around the data cable to a total depth of approximately 4 - 3.32 in. The remaining 1 in. annular space from the top of the mineral wool to the top of the floor assembly was filled with HBI FS-One Max caulking.	2 hours	1.3 hours	CANULC E113	28	Intertek March 30, 2018
5-ply CL2 (131 mm x 116")	None	2" copper pipe	Continued	4.375 in diameter hole. Pipe wrap was installed around the copper pipe to a total depth of approximately 4 - 3.32 in. The remaining 1 in. annular space starting at the top of the mineral wool to the top of the floor assembly was filled with HBI FS-One Max caulking.	2 hours	NA	CANULC E113	28	Intertek March 30, 2018
5-ply CL2 (131 mm x 116")	None	2.3" sch40 40 pipe	Continued	4.92 in diameter hole. Pipe wrap was installed around the schedule 40 pipe to a total depth of approximately 4 - 3.32 in. The remaining 1 in. annular space starting at the top of the pipe wrap to the top of the floor assembly was filled with HBI FS-One Max caulking.	2 hours	0.3 hour	CANULC E113	28	Intertek March 30, 2018
5-ply CL2 (131 mm x 116")	None	6" cast iron pipe	Continued	6.31 in diameter hole. Mineral wool was installed in the 1 in. annular space around the cast iron pipe to a total depth of approximately 4 - 3.32 in. The remaining 1 in. annular space starting at the top of the pipe wrap to the top of the floor assembly was filled with HBI FS-One Max caulking.	2 hours	NA	CANULC E113	28	Intertek March 30, 2018
5-ply CL2 (131 mm x 116")	None	HBI-6 in drop in device System No.: F-B-2049	Continued	8.01" diameter hole. Mineral wool was installed in the 1 - 1.9 in. annular space around the drop-in device to a total depth of approximately 1 - 7.64 in and the remaining 1 in. annular space from the top of the mineral wool to the top edge of the 8 - 1.94 in. hole in the CLT was filled with HBI FS-One Max caulking.	2 hours	1.3 hours	CANULC E113	28	Intertek March 30, 2018
3-ply (178mm x 87")	None	1" nominal PVC pipe	Continued	8.21 in diameter with a 3/4 in plywood sublayer flush with the top of the slab reducing the opening to 2.24 in. Two wraps of HBI CP-635-E-WES-1, 3/4" Firestop wrap was applied at two locations with a 50 gauge steel plate which extended from the top of the slab to 1 in below the slab. The first location was with the bottom of the wrap wrap flush with the bottom of the steel sleeve and the second was with the bottom of the wrap wrap 7 in. from the bottom of the slab. The void between the steel sleeve and the CLT and between the steel sleeve and pipe at the top was filled with Resol full mineral wool having a 3/4 in deep void at the top of the assembly. HBI FS-One Max Intumescent Firestop Sealant was applied to a depth of 3/4 in on the top of the assembly between the plywood and steel sleeve as well as the steel sleeve and pipe.	2 hours	2 hours	ASTM E814	14	QAI Laboratories March 3, 2017

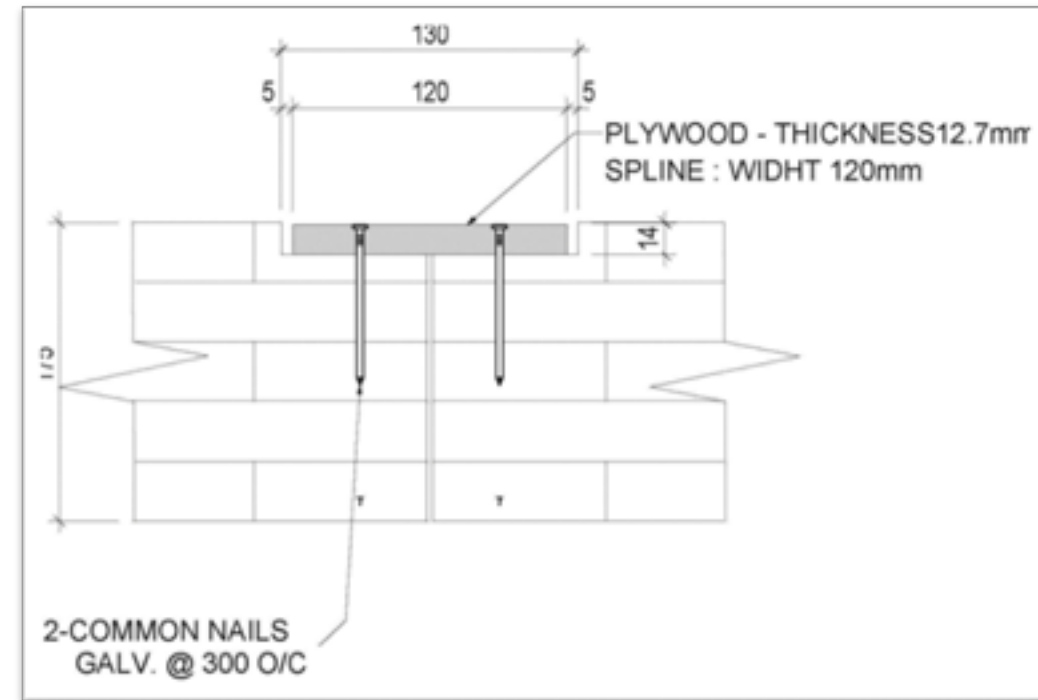
SEALANTS AT MT PANEL EDGES



Sealants at MT Panel Edges

703.9 Sealing of adjacent mass timber elements. In buildings of Type IVA, IVB, and IVC construction, sealant or adhesive shall be provided to resist the passage of air in the following locations:

1. At abutting edges and intersections of mass timber building elements required to be fire resistance-rated
2. At abutting intersections of mass timber building elements and building elements of other materials where both are required to be fire resistance-rated.



Sealants at MT Panel Edges

Sealants shall meet the requirements of ASTM C920 (elastomeric joint sealants). Adhesives shall meet the requirements of ASTM D3498 (gap filling construction adhesives, i.e. not fire caulk).

Exception: Sealants or adhesives need not be provided where they are not a required component of a fire resistance- rated assembly.



Photo: NRCAN



Photo: Charles Judd



Photo: ARUP

Sealants at MT Panel Edges

Several MT fire tested assemblies have successfully been completed w/o adhesives/sealants at abutting panel edges

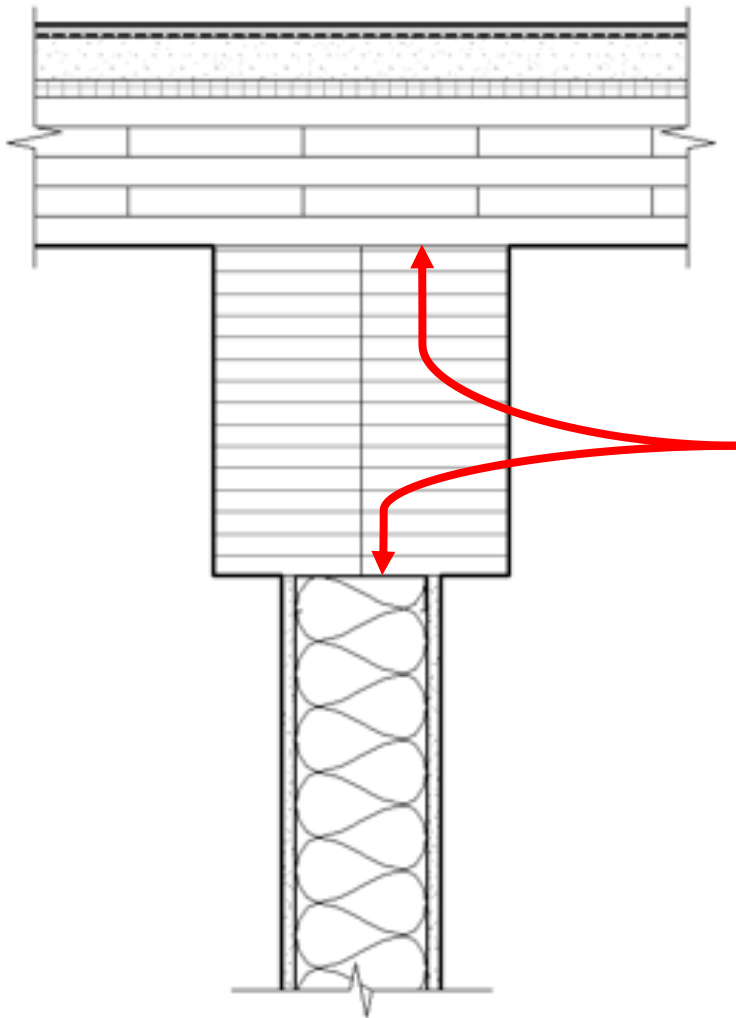
2021 IBC will require periodic special inspections of adhesive/sealant installation (when required to be installed)



Joints & Intersecting Elements

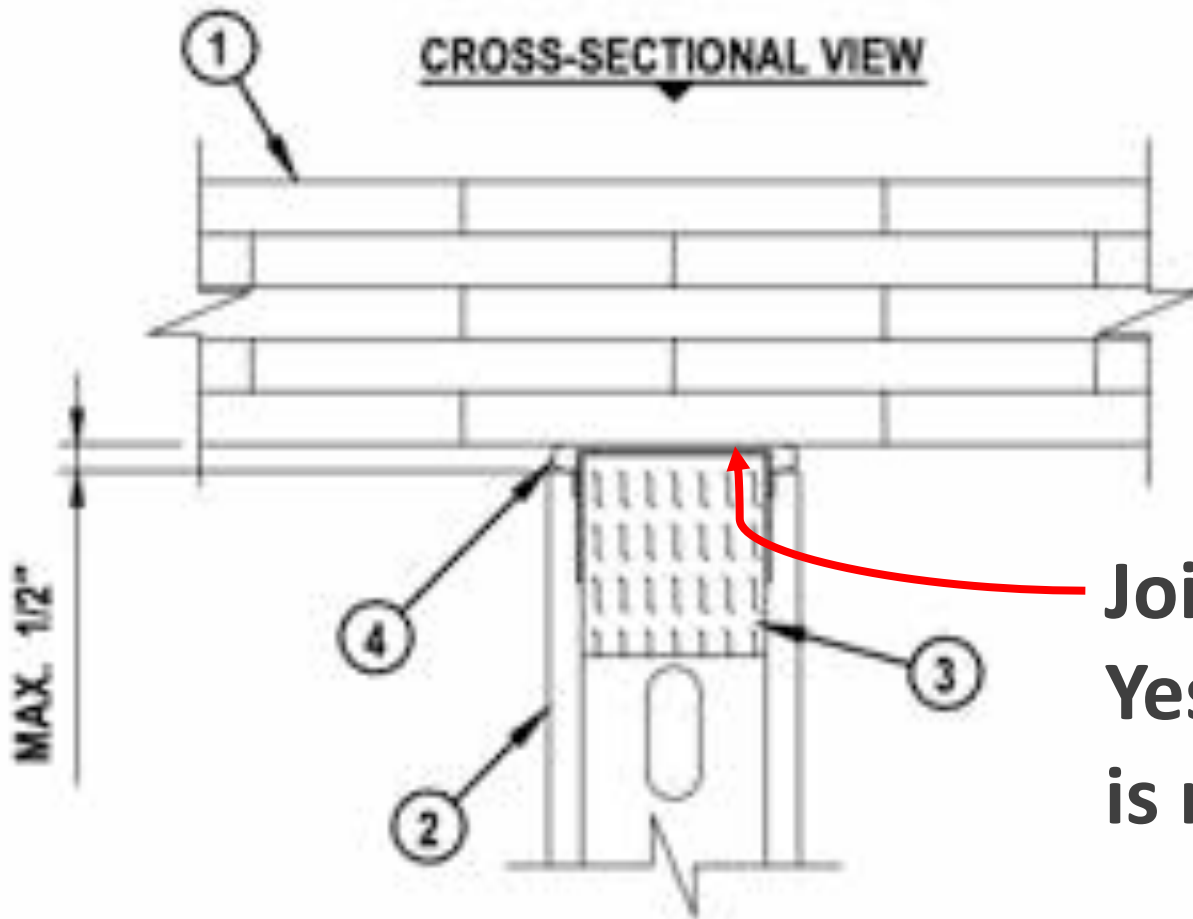
SECTION 202 DEFINITIONS

Joint. *The opening in or between adjacent assemblies that is created due to building tolerances, or is designed to allow independent movement of the building in any plane caused by thermal, seismic, wind or any other loading.*

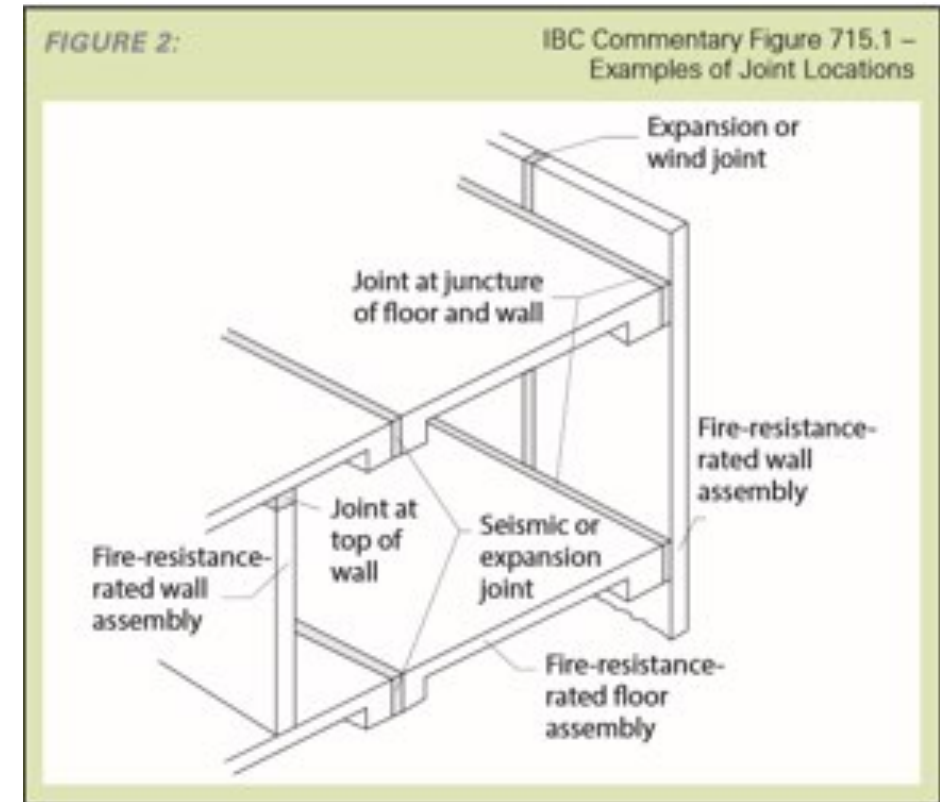


Joint?
**No (if wall
is bearing)**

Joints & Intersecting Elements



Joint?
Yes (if wall
is non-brng)



Source: International Building Code

Fire Safety During Construction

New code provisions in International Fire Code (IFC) address construction fire safety of tall wood buildings

3308.4 Fire safety requirements for buildings of Types IV-A, IV-B, and IV-C construction. Buildings of Types IV-A, IV-B, and IV-C construction designed to be greater than six stories above grade plane shall meet the following requirements during construction unless otherwise approved by the fire code official.

1. Standpipes shall be provided in accordance with Section 3313.
2. A water supply for fire department operations, as approved by the fire chief.



Photo: Structurlam

Fire Safety During Construction

IFC 3313 Standpipe Requirements

SECTION 3313 STANDPIPES

3313.1 Where required.

In buildings required to have standpipes by Section 905.3.1, not less than one standpipe shall be provided for use during construction. Such standpipes shall be installed prior to construction exceeding 40 feet (12 192 mm) in height above the lowest level of fire department vehicle access. Such standpipe shall be provided with fire department hose connections at accessible locations adjacent to usable stairways. Such standpipes shall be extended as construction progresses to within one floor of the highest point of construction having secured decking or flooring.

3313.2 Buildings being demolished.

Where a building is being demolished and a standpipe is existing within such a building, such standpipe shall be maintained in an operable condition so as to be available for use by the fire department. Such standpipe shall be demolished with the building but shall not be demolished more than one floor below the floor being demolished.

3313.3 Detailed requirements.

Standpipes shall be installed in accordance with the provisions of Section 905.

Exception: Standpipes shall be either temporary or permanent in nature, and with or without a water supply, provided that such standpipes comply with the requirements of Section 905 as to capacity, outlets and materials.

Fire Safety During Construction

IFC 3308.4 Cont'd

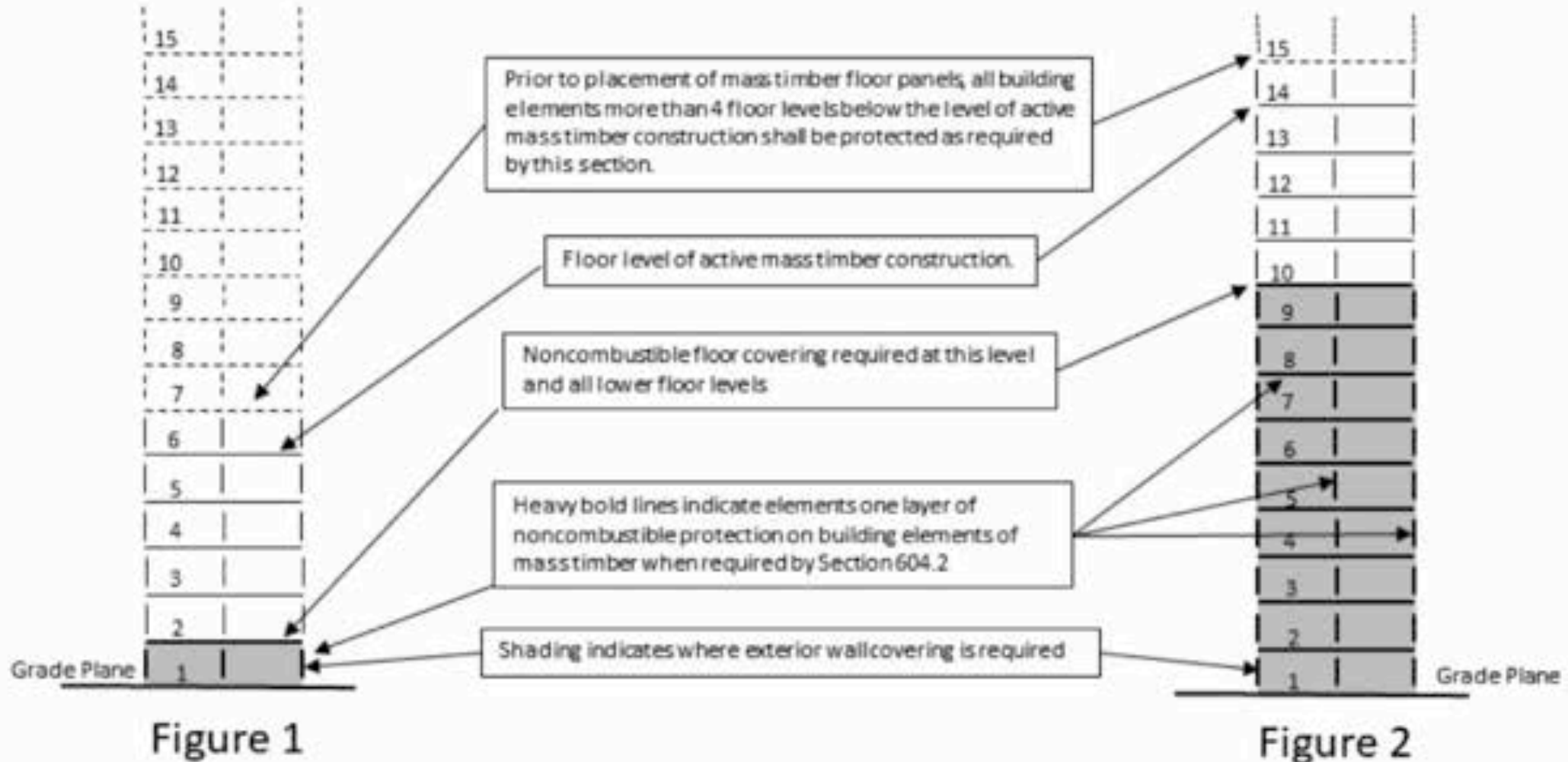
3. Where building construction exceeds six stories above grade plane, at least one layer of noncombustible protection where required by Section 602.4 of the International Building Code shall be installed on all building elements more than 4 floor levels, including mezzanines, below active mass timber construction before erecting additional floor levels.
4. Where building construction exceeds six stories above grade plane required exterior wall coverings shall be installed on all floor levels more than 4 floor levels, including mezzanines, below active mass timber construction before erecting additional floor level.

Exception: Shafts and vertical exit enclosures



Photo: Urban One

Fire Safety During Construction



**Examples of Protection During Construction
For Mass Timber Buildings Greater Than
6 Stories Above Grade Plane**

QUESTIONS?

This concludes The American
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Continuing Education
Systems Course

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